

July 12, 2022

Site Planning
Civil Engineering
Landscape Architecture
Land Surveying
Transportation Engineering

Environmental Studies
Entitlements
Construction Services
3D Visualization
Laser Scanning

Mr. Joseph Cermele, P.E., CFM Kellard Sessions Consulting, PC 500 Main Street Armonk, New York 10504

RE: IMC Project 20044

4 Tripp Lane Gross Land Coverage Compliance Analysis

4 Tripp Lane

Town of North Castle, New York

#### Response to Town Consultant's Comments

Mr. Cermele:

This letter has been prepared to address comments in your October 9<sup>th</sup>, 2020, memorandum to the North Castle Planning Board and the Town's Planning Department staff report dated, October 7, 2020.

In response to the comments in the above noted correspondence, we are pleased to submit one (1) copy of the following documents for your review:

To assist in your review of the revised documents, we are pleased to provide the following, which restates the comments from the above referenced memorandums, followed by our responses:

#### Kellard Sessions Memorandum, dated October 9th, 2020:

#### Comment No. 1

The applicant has provided a Gross Land Coverage Plan to demonstrate compliance with the maximum permitted gross land coverage for the zoning district. The plan indicates the removal of an existing sport court and a portion of the existing drive, both completed without permits, to reduce the land coverage, as necessary, to comply. We note, however, that the plan appears to require the addition of two areas of existing coverage, currently not accounted for; (1) the northernmost portion of the Boulder wall along the eastern property line appears to exceed 4 feet in height, and (2) the plan makes reference to a concrete patio north of the shed building. Although not shown on the plan, based on review of available Westchester County aerial mapping, the patio appears to exist. The plan shall be revised to include these additional coverage areas and the calculations adjusted accordingly so a determination can be made as to whether the total allowable coverage has been exceeded.

All portions (greater than 4' high) of the boulder wall have now been included in the coverage calculations. After a site visit by JMC on March 22, 2021, it was confirmed that the above referenced concrete patio area north of the shed building had previously been removed by the owner. A picture of this area has been included on the updated Gross Land Coverage drawing. In addition, the existing sport court and a portion of the existing driveway will be removed to comply with the Gross Land Coverage requirements.

#### Comment No. 2

The applicant will need to demonstrate to the Planning Board the levels of disturbances associated with the tree removal, filling and grading, construction of additional structures, walks, walls, patios, etc. This office will require an engineered site plan and comparative plan analysis using available historical Westchester County aerial mapping and GIS topography. This plan shall be used as the baseline to establish the various disturbances and the associated mitigation that will be required.

#### Response No. 2

An engineered site plan depicting the current conditions of the site has been prepared along with a pre-existing conditions plan depicting what the Site had looked like before the owner performed the improvements.

#### Comment No. 3

The applicant shall provide floor plans and elevations for the proposed additions to the existing residence, the pool cabana and the shed. The plans shall clarify whether any services or utilities including water, sewer and electric are provided at the cabana and I or the shed.

#### Response No. 3

Floor plans and elevations have been provided for the improvements to the residence along with the Cabana. The Shed was prefabricated therefore no specification sheets, floor plans, elevations were provided to the client. A picture of the shed is now included on the Gross Land Coverage Calculation drawing. No utilities serve the Cabana or the Shed.

#### Comment No. 4

The applicant will be required to provide confirmation from the Westchester County Health Department that the improvements and expansions to the residence and cabana do not require upgrades or modifications to the on-site wastewater treatment system.

#### Response No. 4

The applicant has begun discussions with the WCDOH and all approvals will be provided to the Town as soon as they are received by the applicant.

#### Comment No. 5

The plan shall illustrate and dimension all minimum required yard setbacks.

#### Response No. 5

JMC Drawing C-110 now illustrates and dimensions all yard setbacks and all conform to Town code.

#### Comment No. 6

As part of an ongoing application with the adjacent property to the east, it was discovered that a locally regulated wetland exists at the rear of the site. The applicant will be required to investigate this wetland system to identify the boundary and associated 100-foot wetland buffer. Based on review of available Westchester County aerial mapping, it appears that this system is potentially connected to or continues through the subject property (prior to placement of fill) to a system on the west side of the property. The wetland boundary shall be field located and established with sequentially number flags for confirmation by the Town Wetland Consultant. Prior disturbances are likely to have occurred within the regulated buffer. If so, a local Wetland Permit will be required, and the applicant will be required to prepare a wetland mitigation plan in accordance with Chapter 340, Wetlands and Watercourse Protection of the Town Code. The plan will require referral to the Conservation Board for recommendation of approval. Please notify this office once the wetland boundary has been established in the field.

#### Response No. 6

Survey information was obtained from the Town of North Castle's Planning Board website that included the extents of the town regulated wetland located on the adjacent property. This was the only information available as there is no historical information on this town regulated wetland. This wetland was delineated on April 18, 2022, by Ecological Solutions, LLC. The wetland buffer and the approximate amount of previous disturbance within this buffer are now shown on JMC Drawing C-110.

#### Comment No. 7

The Wetland Mitigation Plan, if necessary, shall illustrate and quantifying the previous disturbance areas to the wetland and/or wetland buffer. The plan shall include a summary table that quantifies the total wetland and wetland buffer area on site, total disturbance areas within each, and total pervious and impervious cover pre and post development. Mitigation shall be provided at a ratio of 2:1 minimum.

#### Response No. 7

The only new impervious surfaces within the 100' wetland buffer are the new retaining walls that total approximately 300 SF of impervious area. The approximate amount of disturbance within the wetland buffer is now labeled on JMC Drawing C-110. There was no disturbance to the wetland itself according to the wetland information delineated by Ecological Solutions on April 18, 2022. The applicant awaits determination by the Town on whether a mitigation plan will be necessary based on new information included with this submission.

#### Comment No. 8

The applicant has cleared a significant number of trees on the property. The quantity, size and species are not known. As required by Chapter 308, Trees of the Town Code, the applicant will be required to provide a tree restoration plan to mitigate the unapproved removal of existing vegetation. The Planning Board will need to determine whether the restoration plan is ultimately appropriate for the level of disturbance.

#### Response No. 8

JMC Drawing C-130 has been added to the Site Plan set that delineates the areas of tree removal and proposes a solution for the mitigation of these trees that were removed. The applicant awaits the Town's review and determination on whether the 255 trees that were planted are sufficient for the mitigation of the 171 trees removed.

#### Comment No. 9

The applicant imported an unknown quantity of fill to regrade the rear yard. The baseline plan noted in Comment #2 above will be used as the basis for determination of the approximate quantity of fill imported to the site. The applicant shall prepare a cut/fill calculation and will be required to demonstrate compliance with Chapter 161, Filling and Grading of the Town Code, specifically as a relates to the soil source, import quantity and compliance with 6 NYCRR part 360. At a minimum, the applicant will be required to provide certification that the soil meets the Unrestricted Soil Use Group for residential sites. The applicant will be required to complete soil sampling and testing in accordance with New York State Department of Environmental Conservation (NYSDEC) protocol and provide a soils analysis report certified by a NYS Certified Laboratory and Soils Scientist or Engineer to demonstrate that the material imported to the site is suitable.

#### Response No. 9

JMC Drawing C-410 has been added to the Site Plan set that delineates and identifies the cut and fill areas along with the total amounts of each. The client has begun conversations with a soil consultant, William Canavan of HESNY, about the soils testing on Site. All information from this testing will be provided to the Town upon receipt.

#### Comment No. 10

The property is served by an on-site wastewater treatment system. The plan shall illustrate the location of the existing septic field and tanks based on available Westchester County Department of Health (WCHD) as-builts and record data. It is assumed that the imported fill material and regrading activities that occurred at the rear of the property was also placed above the existing septic field, potentially compromising its function. The applicant will be required to provide a determination, confirmed by the WCHD, that the septic system continues to operate as intended. Any upgrades or modifications that may become necessary will need to be illustrated on the plan and approved by the Westchester County Health Department.

The applicant has begun discussions with the WCDOH and all approvals will be provided to the Town as soon as they are received by the applicant. No bedrooms were added as part of the improvements to the residence.

#### Comment No. 11

The applicant has developed several improvements and altered the land cover characteristics for the site which has resulted in an increase in impervious surface and an associated increase in stormwater runoff. As required by Chapter 267, Stormwater Management of the Town Code, the applicant shall prepare a Stormwater Pollution Prevention Plan, inclusive of stormwater mitigation and attenuation measures, to mitigate stormwater runoff through the 100-year, 24-hour storm event. For the purpose of the analysis, the baseline map noted above shall be used to establish pre-developed conditions and a comparative analysis to the current site conditions shall be prepared.

#### Response No. 11

A stormwater report, prepared by JMC, has been prepared per town requirements and has been included with this submission.

#### Comment No. 12

The plan shall clearly illustrate the location of any existing drainage systems, conveyance systems and connections. Any connections that may exist, to this storm system located in Tripp Lane, will require approval by the Town Highway Department.

#### Response No. 12

All pertinent information is now depicted on the updated Site Plans. To the best of our knowledge, there has been no connection into the storm system located in Tripp Lane.

#### Comment No. 13

As part of the stormwater mitigation system design, the applicant will be required to perform deep and soil percolation testing in the vicinity of any proposed stormwater mitigation practices. The soil testing shall be witnessed by the Town Engineer. Please contact this office to schedule the required soil testing.

#### Response No. 13

The applicant will coordinate the soils testing with your office. The plans will be updated per information from this soils testing and all information will be included in the Stormwater Report.

#### Comment No. 14

The applicant will be required to provide certification for the proper construction and stability of all retaining walls greater than or equal to 4 feet in height. Details of their construction shall be provided on the plan.

The applicant has hired a licensed professional engineer to analyze the installed walls. He has provided a retaining wall plan, a narrative and calculations verifying the stability of these walls and all information has been include with this submission.

#### Comment No. 15

The plan shall clearly illustrate and identify the various fences located throughout the site, indicating their height and material. Fence details shall be provided on the plan.

#### Response No. 15

JMC Drawing C-901 has been updated to include pictures and details of all fencing on Site.

#### Comment No. 16

Driveway piers and a gate has been installed at the front property line. The Town requires that gates be set back a minimum of 20 feet from the right of way to permit adequate area for a vehicle to pull off the road as well as to account for potential future road widening. The piers and gate shall be relocated accordingly, and appropriate details of their construction included on the plans.

#### Response No. 16

It is the applicant's intent to ask for a waiver for this requirement and the applicant is prepared to update the pier locations in the event of the proposed widening of Tripp Lane.

#### Comment No. 17

The driveway curb cut is greater than 18 feet in width which is the maximum permitted by the Town Highway Department. The plan shall be revised to demonstrate compliance and include all details necessary for work and restoration within the Town Right of Way.

#### Response No. 17

It is the applicant's intent to ask for a waiver for this requirement.

#### Town of North Castle Planning Department Staff Report, dated October 7, 2020:

#### **Procedural Comments**

#### Comment No. 1

The Proposed Action would be classified as a Type II Action pursuant to the State Environmental Quality Review Act (SEQRA).

So noted.

#### Comment No. 2

A neighbor notification meeting regarding the proposed amendment will need to be scheduled.

#### Response No. 2

So noted.

#### Comment No. 3

Pursuant to Section 12-18.A of the Town Code, all site development plans submitted to the Planning Board are required to be referred to the Architectural Review Board (ARB) for review and comment.

#### Response No. 3

So noted.

#### **General Comments**

#### Comment No. 1

The Applicant has only addressed one aspect of the various violations on the site (gross land coverage) and has not substantively responded to the notices of violations.

#### Response No. 1

All violations with corresponding responses are outlined below:

#### Code Violation 127-4A – Building Permit

A building permit will be filed for all work performed and to be performed as soon as all items are addressed to the satisfaction of the Town's Engineer.

#### Code Violation 127-5A – Construction Inspections

It was understood by the applicant, per Comment #14 above that it was the applicant's responsibility to inspect the walls that were installed and information from these inspections has been include with this submission. If the remaining items need to be inspected by the Town, the applicant would like to schedule those inspections as soon as possible and all certifying documentation will be provided to the Town.

Code Violation 127-7A — Certificates of Occupancy/Certificates of Compliance As soon as the inspections mentioned above have been completed to the satisfaction of the Town, the applicant will file for all Certificates of Occupancy and Certificates of Compliance.

#### Code Violation 355-74A – Building Permits

A building permit will be filed for all work performed and to be performed as soon as all items are addressed to the satisfaction of the Town's Engineer

#### Code Violation 355-75A – Certificates of Occupancy

As soon as the inspections mentioned above have been completed to the satisfaction of the Town, the applicant will file for all Certificates of Occupancy and Certificates of Compliance.

#### Code Violation 355-4B - Structure

It was understood by the applicant, per Comment #14 above that it was the applicant's responsibility to inspect the walls that were installed and information from these inspections has been include with this submission. If the remaining items need to be inspected by the Town, the applicant would like to schedule those inspections as soon as possible and all certifying documentation will be provided to the Town.

#### 2017 NYS Uniform Code Supplement – 108.3 – Building Permit Violation

A building permit will be filed for all work performed and to be performed as soon as all items are addressed to the satisfaction of the Town's Engineer. A tree removal permit will be filed if deemed necessary by the Planning Board.

2017 NYS Uniform Code Supplement – 108.5 – Construction Inspection Violation It was understood by the applicant, per Comment #14 above that it was the applicant's responsibility to inspect the walls that were installed and information from these inspections has been include with this submission. If the remaining items need to be inspected by the Town, the applicant would like to schedule those inspections as soon as possible and all certifying documentation will be provided to the Town. As soon as the inspections mentioned above have been completed to the satisfaction of the Town, the applicant will file for all Certificates of Occupancy and Certificates of Compliance.

#### Code Violation 157-16A - Tree Removal

A revised tree removal plan has been included in this submission set and if deemed necessary, a tree removal permit will be filed with the Town.

#### Code Violation 157-16B - Tree Removal

A revised tree removal plan has been included in this submission set and if deemed necessary, a tree removal permit will be filed with the Town.

#### Code Violation 161-1 - Fill and Grading

JMC Drawing C-410 has been added to the Site Plan set that delineates and identifies the cut and fill areas along with the total amounts of each. The client has begun conversations with the Town's soil consultant, William Canavan of HESNY, about the soils testing on Site. All information from this testing will be provided to the Town upon receipt.

#### Code Violation 161-1E – Filling and Grading

All required fees will be paid upon review and approval of the attached drawings.

Code Violation 161-B(4) – Filling and Grading (SWPPP)

A stormwater report, prepared by JMC has been include in this submission.

Code Violation 340-4 – Wetland Activities Subject to Regulation

Survey information was obtained from the Town of North Castle's Planning Board website that included the extents of the town regulated wetland located on the adjacent property. This was the only information available as there is no historical information on this town regulated wetland. This wetland was delineated on April 18, 2022, by Ecological Solutions, LLC. The wetland buffer and the approximate amount of previous disturbance within this buffer are now shown on JMC Drawing C-110.

Code Violation 267-5A – Stormwater Pollution Prevention Plans A stormwater report, prepared by JMC has been include in this submission.

Code Violation 340-5A - General Procedures (Permit Required)

Survey information was obtained from the Town of North Castle's Planning Board website that included the extents of the town regulated wetland located on the adjacent property. This was the only information available as there is no historical information on this town regulated wetland. This wetland was delineated on April 18, 2022, by Ecological Solutions, LLC. The wetland buffer and the approximate amount of previous disturbance within this buffer are now shown on JMC Drawing C-110.

#### Comment No. 2

The site plan should depict the location of the 3/4 acre of trees removed without a permit Pursuant to Section 308-15.A(11) of the Town Code, the Applicant should prepare an extensive tree replanting plan of the disturbed area. The plan should aim to revegetate the site to the maximum extent practicable.

See site prior to tree removal on the right.

#### Response No. 2

JMC Drawing C-130 has been added to the Site Plan set that delineates the areas of tree removal and proposes a solution for the mitigation of these trees that were removed. The applicant awaits the Town's review and determination on whether the 255 trees that were planted are sufficient for the mitigation of the 171 trees removed.

#### Comment No. 3

The site plan should be revised to depict the location of the proposed (legalization) fence. In addition, a fence detail should be submitted for review.

#### Response No. 3

JMC Drawing C-110 has been updated to label all installed fencing.

#### Comment No. 4

The site plan should be revised to label the proposed (legalization) driveway entry piers. In addition, details of the driveway piers should be submitted for review.

#### Response No. 4

The piers are now labeled on JMC Drawing C-IIO and Detail #14 has been added to the Site Plan set.

#### Comment No. 5

The proposed (legalization) driveway gates are located on the property line. Driveway gates should be located a minimum of 20 feet from the front property line to permit adequate vehicular pull off from the right-of-way should Tripp Lane ever be expanded to the edge of the right-of-way. A detail for the gates should be submitted to the Planning Board for review.

#### Response No. 5

It is the applicant's intent to ask for a waiver for this requirement and the applicant is prepared to update the pier locations in the event of the proposed widening of Tripp Lane.

#### Comment No. 6

The site plan should be revised to include a zoning conformance table.

#### Response No. 6

JMC Drawing C-000 now shows a Table of Land Use.

#### Comment No. 7

The Applicant should submit floor plans and elevations for the proposed (legalization) cabana.

#### Response No. 7

Floor plans and elevations have been provided for the improvements to the residence along with the Cabana.

#### Comment No. 8

The Applicant should submit floor plans and elevations for the proposed (legalization) shed.

#### Response No. 8

Floor plans and elevations have been provided for the improvements to the residence along with the Cabana. The Shed was prefabricated therefore no specification sheets, floor plans, elevations were provided to the client. A picture of the shed is now included on the Gross Land Coverage Calculation drawing.

#### Comment No. 9

The Applicant should submit floor plans and elevations for the proposed (legalization) rear house addition.

#### Response No. 9

Floor plans and elevations have been provided for the improvements to the residence along with the Cabana.

#### Comment No. 10

The site plan should depict the location and height of all proposed (legalization) retaining walls.

#### Response No. 10

JMC Drawing C-110 has been updated to include labels on all retaining walls.

#### Comment No. 11

The site should depict the location of where fill was placed on the site.

#### Response No. 11

JMC Drawing C-110 has been updated to show the approximate limit of fill area.

#### Comment No. 12

The Applicant should submit a gross floor area calculations worksheet and backup data for review.

#### Response No. 12

The applicant has provided a gross floor area calculation worksheet and backup data for the Town's review.

We trust that the above, along with the enclosed documents and drawings, address your comments. We look forward to your continued review throughout the approval process and discussing this matter with you further. Should you have any questions or require additional information regarding the information provided above, please do not hesitate to contact our office at 914-273-5225.

Sincerely,

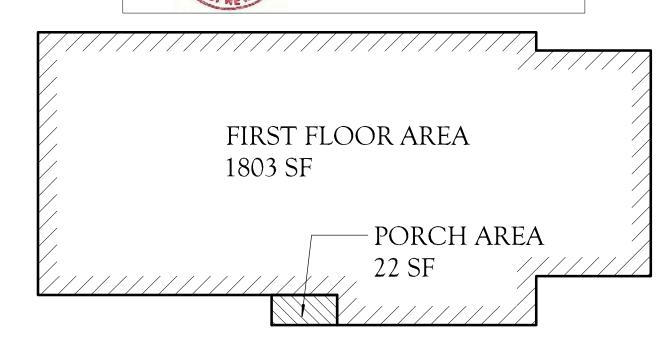
JMC Planning Engineering Landscape Architecture & Land Surveying, PLLC

Rick Bohlander, PE Project Manager

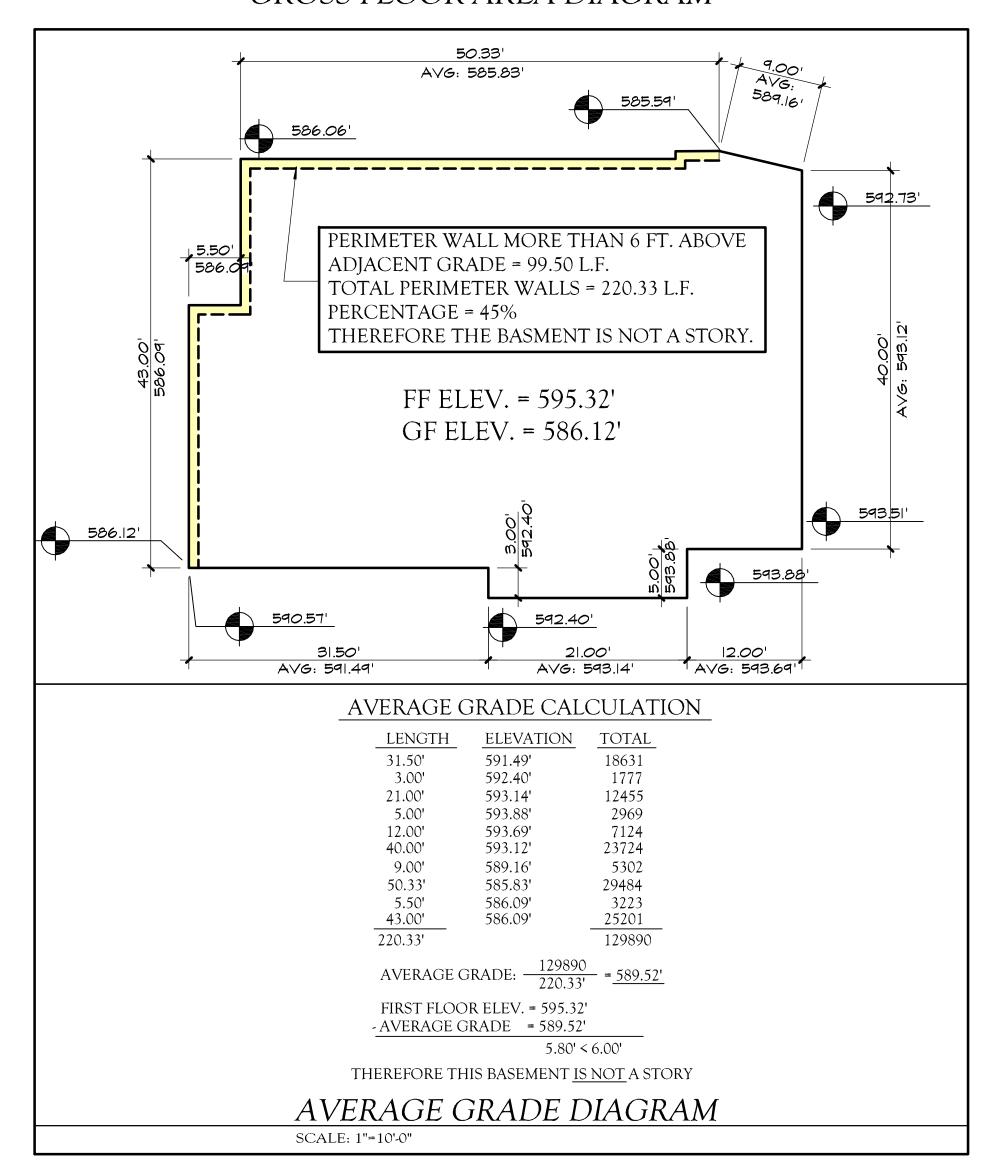
CC: Mr. Adam Kaufman

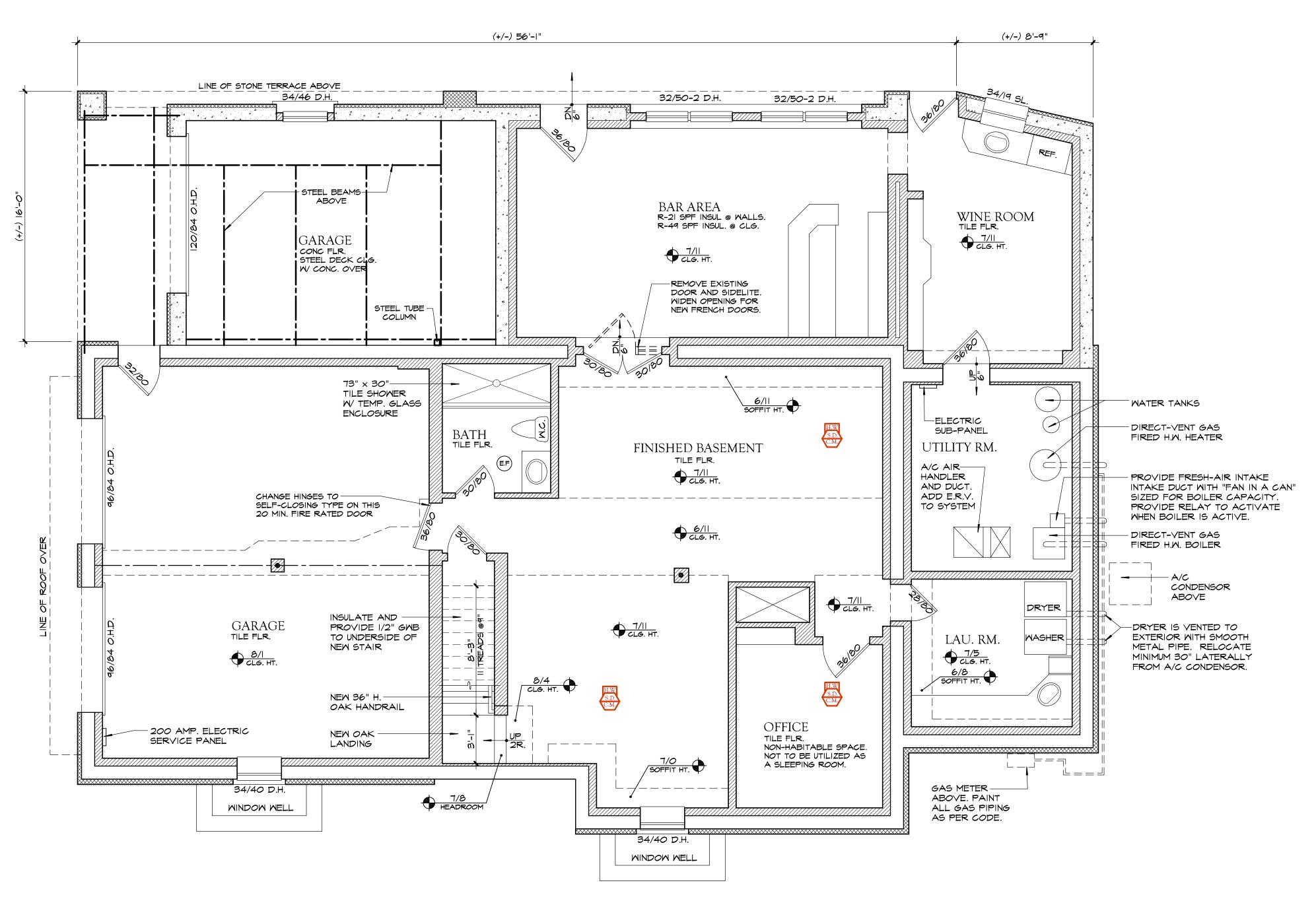
Ms. Valerie Desimone

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# GROSS FLOOR AREA DIAGRAM





AS-BUILT BASEMENT FLOOR PLAN

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The Certificate of Occupancy Pros Avenue, Suite 203, Pleasantville, New York

Legalizations to the

Pereira Residence

4 Tripp Lane, Armonk, New York

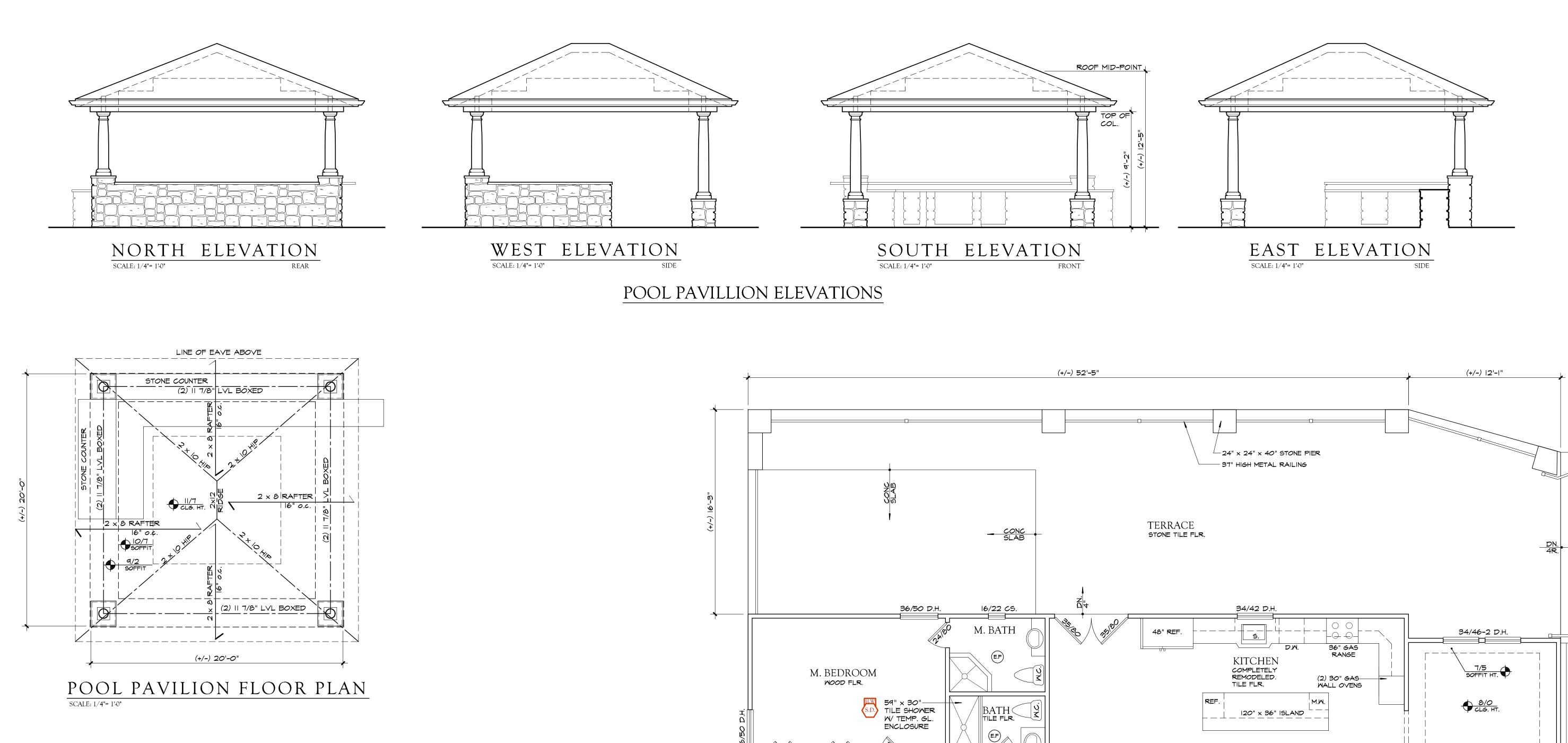
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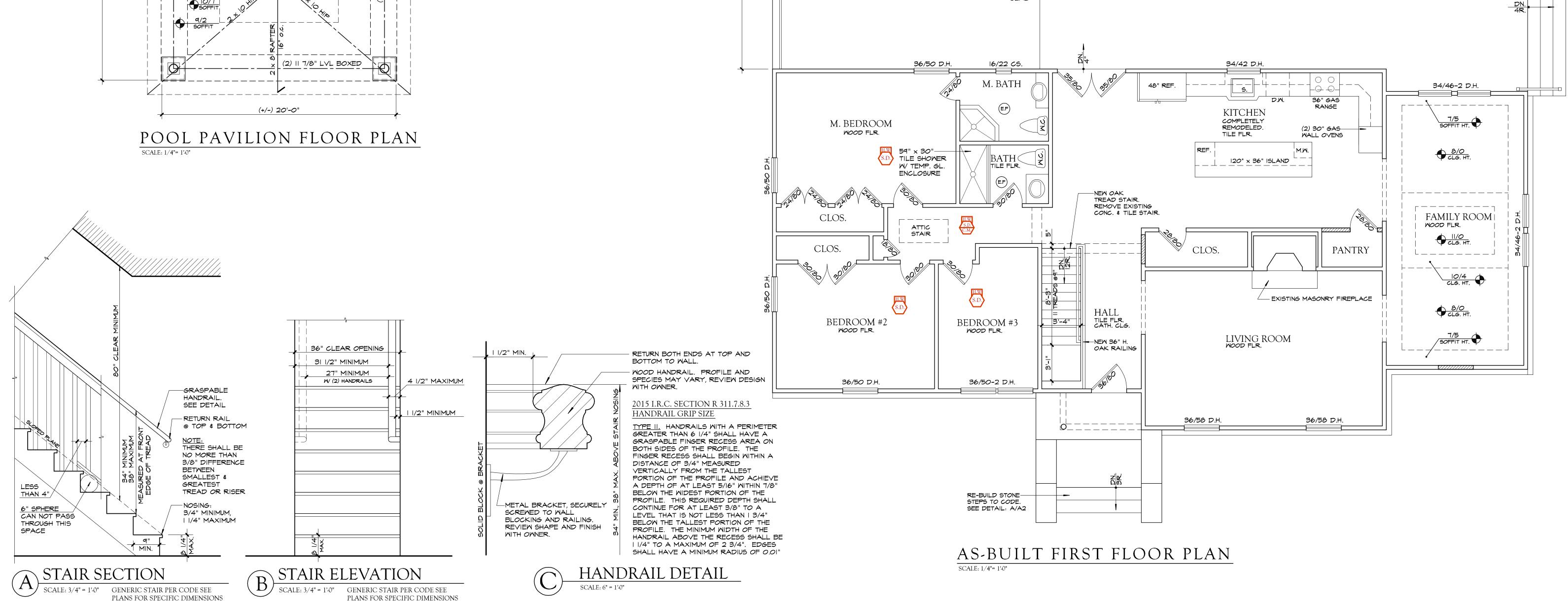
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A1

Pereira





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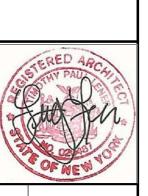
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Revisions

Date: 09/16/20

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Sheet No.

A2

Pereira



REAR VIEW FROM DRIVEWAY

NORTH ELEVATION

SCALE: 1/4"= 1'-0"

REAR

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Date: 09/16/20

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# SITE DEVELOPMENT PLAN APPROVAL DRAWINGS

# PEREIRA RESIDENCE

# 4 TRIPP LANE TAX MAP SECTION 108.02 | BLOCK 1 | LOT 10 WESTCHESTER COUNTY NORTH CASTLE, NY

Applicant / Owner:
MR. & MRS. PEREIRA
4 TRIPP LANE
TOWN OF NORTH CASTLE, NY
APPLICANT PHONE: (914) 391-6979

## **Architect:**

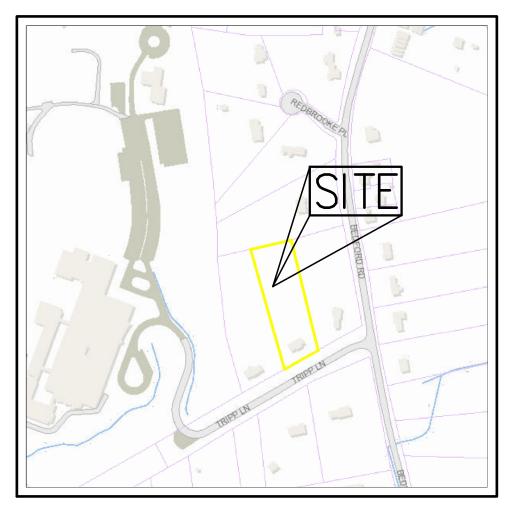
GET MY C.O. 57 WHEELER AVENUE, SUITE 203 PLEASANTVILLE, NY 10570 (914) 727-0980

## Surveyor:

SUMMIT LAND SURVEYING P.C. 21 DRAKE LANE WHITE PLAINS, NY 10607 (914) 629-7758



Site Planner, Civil Engineer
and Landscape Architect:
120 BEDFORD ROAD
ARMONK, NY 10504
(914) 273-5225







### GENERAL CONSTRUCTION NOTES APPLY TO ALL WORK HEREIN

1. PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL CALL 811 "DIG SAFELY" (1-800-962-7962) TO HAVE UNDERGROUND UTILITIES LOCATED. EXPLORATORY EXCAVATIONS SHALL COMPLY WITH CODE 753 REQUIREMENTS. NO WORK SHALL COMMENCE UNTIL ALL THE OPERATORS HAVE NOTIFIED THE CONTRACTOR THAT THEIR UTILITIES HAVE BEEN LOCATED. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PRESERVATION OF ALL PUBLIC AND PRIVATE UNDERGROUND AND SURFACE UTILITIES AND STRUCTURES AT OR ADJACENT TO THE SITE OF CONSTRUCTION, INSOFAR AS THEY MAY BE ENDANGERED BY THE CONTRACTOR'S OPERATIONS. THIS SHALL HOLD TRUE WHETHER OR NOT THEY ARE SHOWN ON THE CONTRACT DRAWINGS. IF THEY ARE SHOWN ON THE DRAWINGS, THEIR LOCATIONS ARE NOT GUARANTEED EVEN THOUGH THE INFORMATION WAS OBTAINED FROM THE BEST AVAILABLE SOURCES, AND IN ANY EVENT, OTHER UTILITIES ON THESE PLANS MAY BE ENCOUNTERED IN THE FIELD. THE CONTRACTOR SHALL, AT HIS OWN EXPENSE, IMMEDIATELY REPAIR OR REPLACE ANY STRUCTURES OR UTILITIES THAT HE DAMAGES, AND SHALL CONSTANTLY PROCEED WITH CAUTION TO PREVENT UNDUE INTERRUPTION OF UTILITY SERVICE.

2. CONTRACTOR SHALL HAND DIG TEST PITS TO VERIFY THE LOCATION OF ALL EXISTING UNDERGROUND UTILITIES PRIOR TO THE START OF CONSTRUCTION. CONTRACTOR SHALL VERIFY EXISTING UTILITIES DEPTHS AND ADVISE OF ANY CONFLICTS WITH PROPOSED UTILITIES. IF CONFLICTS ARE PRESENT. THE OWNER'S FIELD REPRESENTATIVE, JMC, PLLC AND THE APPLICABLE MUNICIPALITY OR AGENCY SHALL BE NOTIFIED IN WRITING. THE EXISTING/PROPOSED UTILITIES RELOCATION SHALL BE DESIGNED BY JMC, PLLC.

- 3. CONTRACTOR IS RESPONSIBLE FOR OBTAINING ANY AND ALL LOCAL PERMITS REQUIRED.
- 4. ALL WORK SHALL BE DONE IN STRICT COMPLIANCE WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES, STANDARDS, ORDINANCES, ROLES, AND REGULATIONS. ALL CONSTRUCTION WORK SHALL BE PERFORMED IN ACCORDANCE WITH ALL SAFETY CODES. APPLICABLE SAFETY CODES MEAN THE LATEST EDITION INCLUDING ANY AND ALL AMENDMENTS, REVISIONS, AND ADDITIONS THERETO, TO THE FEDERAL DEPARTMENT OF LABOR, OCCUPATIONAL SAFETY AND HEALTH STANDARDS (OSHA); AND APPLICABLE SAFETY, HEALTH REGULATIONS AND BUILDING CODES FOR CONSTRUCTION IN THE STATE OF NEW YORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR GUARDING AND PROTECTING ALL OPEN EXCAVATIONS IN ACCORDANCE WITH THE PROVISION OF SECTION 107–05 (SAFETY AND HEALTH REQUIREMENTS) OF THE NYSDOT STANDARD SPECIFICATIONS. IF THE CONTRACTOR PERFORMS ANY HAZARDOUS CONSTRUCTION PRACTICES, ALL OPERATIONS IN THE AFFECTED AREA SHALL BE DISCONTINUED AND IMMEDIATE ACTION SHALL BE TAKEN TO CORRECT THE SITUATION TO THE SATISFACTION OF THE APPROVAL AUTHORITY HAVING JURISDICTION.
- 5. CONTRACTOR SHALL MAINTAIN ACCESS TO ALL PROPERTIES AFFECTED BY THE SCOPE OF WORK SHOWN HEREON AT ALL TIMES TO THE SATISFACTION OF THE OWNERS REPRESENTATIVE. RAMPING CONSTRUCTION TO PROVIDE ACCESS MAY BE CONSTRUCTED WITH SUBBASE MATERIAL EXCEPT THAT TEMPORARY ASPHALT CONCRETE SHALL BE PLACED AS DIRECTED BY THE ENGINEER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING SAFE PEDESTRIAN ACCESS AT ALL TIMES.
- 6. CONTRACTOR SHALL MAINTAIN THE INTEGRITY OF EXISTING PAVEMENT TO REMAIN.

# JMC Drawing List:

C-000 COVER SHEET

C-100 PRE-EXISTING CONDITIONS MAP

C-110 EXISTING CONDITIONS MAP AND DEMOLITION PLAN

C-130 TREE MITIGATION PLAN

C-200 SITE PLAN

C-310 GROSS LAND COVERAGE PLAN

C-410 CUT AND FILL PLAN

C-900 CONSTRUCTION DETAILS

C-901 CONSTRUCTION DETAILS

TABLE OF LAND USE				
TOWN OF NORTH CASTLE, ZONE "R-2A." - "ONE FA				
DESCRIPTION	N	REQUIRED	PROVIDED	
MINIMUM LOT AREA	(ACRES / S.F.)	2	±2.06/±89,820	
MINIMUM LOT FRONTAGE	(FEET)	150	±183.6	
MINIMUM LOT WIDTH	(FEET)	150	±175	
MINIMUM LOT DEPTH	(FEET)	150	±513.3	
MINIMUM YARDS				
FRONT	(FEET)	50	±55.1	
SIDE	(FEET)	30	±35.2	
REAR	(FEET)	50	±402.2	

(PERCENT)

# AREA MAP SCALE: N.T.S.

SUBSURFACE UTILITY LOCATIONS ARE BASED ON A COMPILATION OF FIELD EVIDENCE, AVAILABLE RECORD PLANS AND/OR UTILITY MARK-OUTS. THE LOCATION OR COMPLETENESS OF UNDERGROUND INFORMATION CANNOT BE GUARANTEED. VERIFY THE ACTUAL LOCATION OF ALL UTILITIES PRIOR TO EXCAVATION OR CONSTRUCTION.



Know what's **below. Call** before you dig.

MAXIMUM BUILDING HEIGHT

MAXIMUM BUILDING COVERAGE

MINIMUM DWELLING UNIT SIZE (§355-70)

ANY ALTERATION OF PLANS,
SPECIFICATIONS, PLATS AND
REPORTS BEARING THE SEAL
OF A LICENSED PROFESSIONAL
ENGINEER OR LICENSED LAND
SURVEYOR IS A VIOLATION OF
SECTION 7209 OF THE NEW
YORK STATE EDUCATION LAW,
EXCEPT AS PROVIDED FOR BY
SECTION 7209, SUBSECTION 2.

No. Revision Date By

1. REVISED PER TOWN ENGINEER'S COMMENTS 07/12/2022 RB

Previous Editions Obsolete



JMC Planning, Engineering, Landscape
Architecture & Land Surveying, PLLC

JMC Site Development Consultants, LLC

John Meyer Consulting, Inc.

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voice 914.273.5225 • fax 914.273.2102
www.jmcpllc.com

Scale: NOT TO SCALE

Date: 03/01/2021

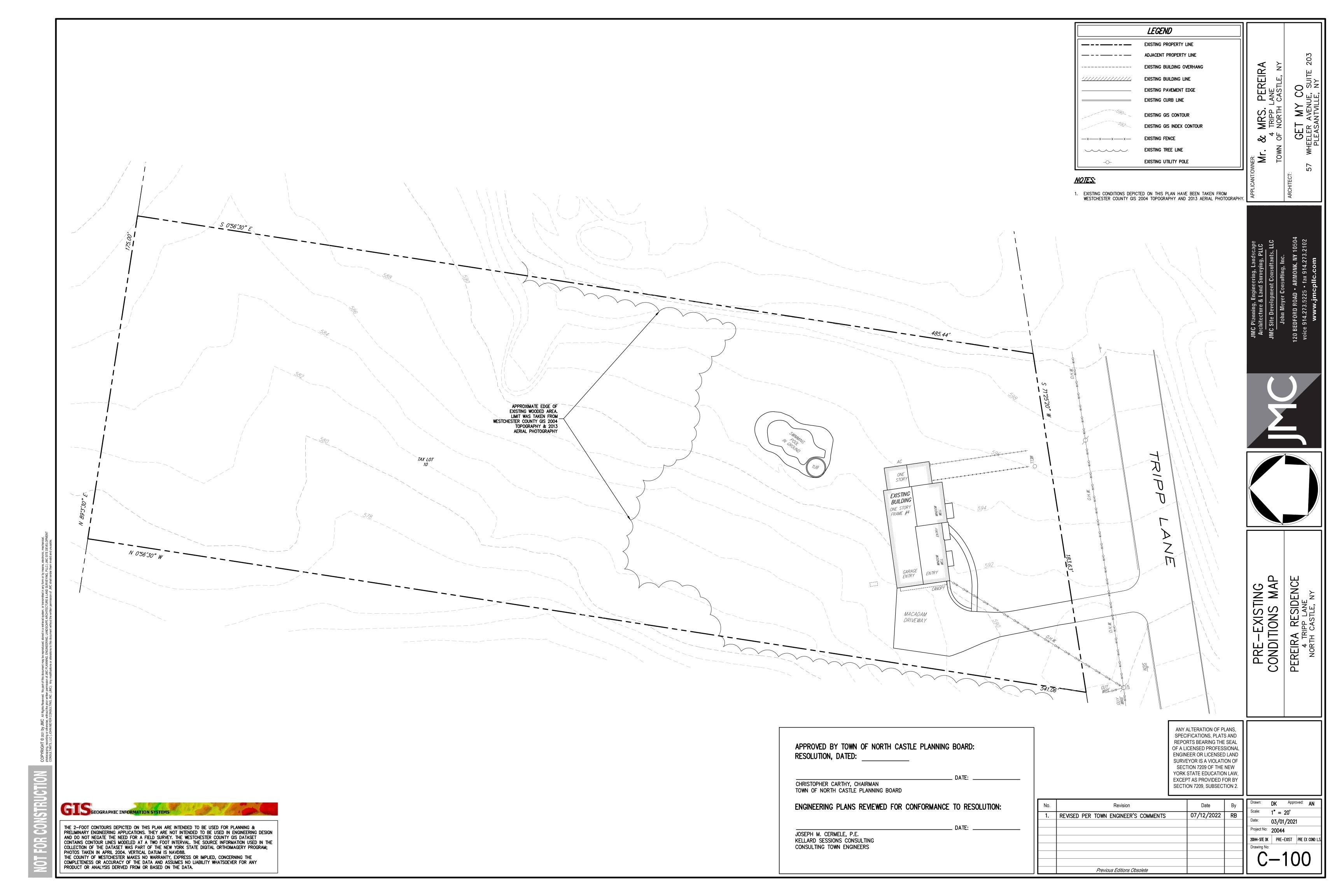
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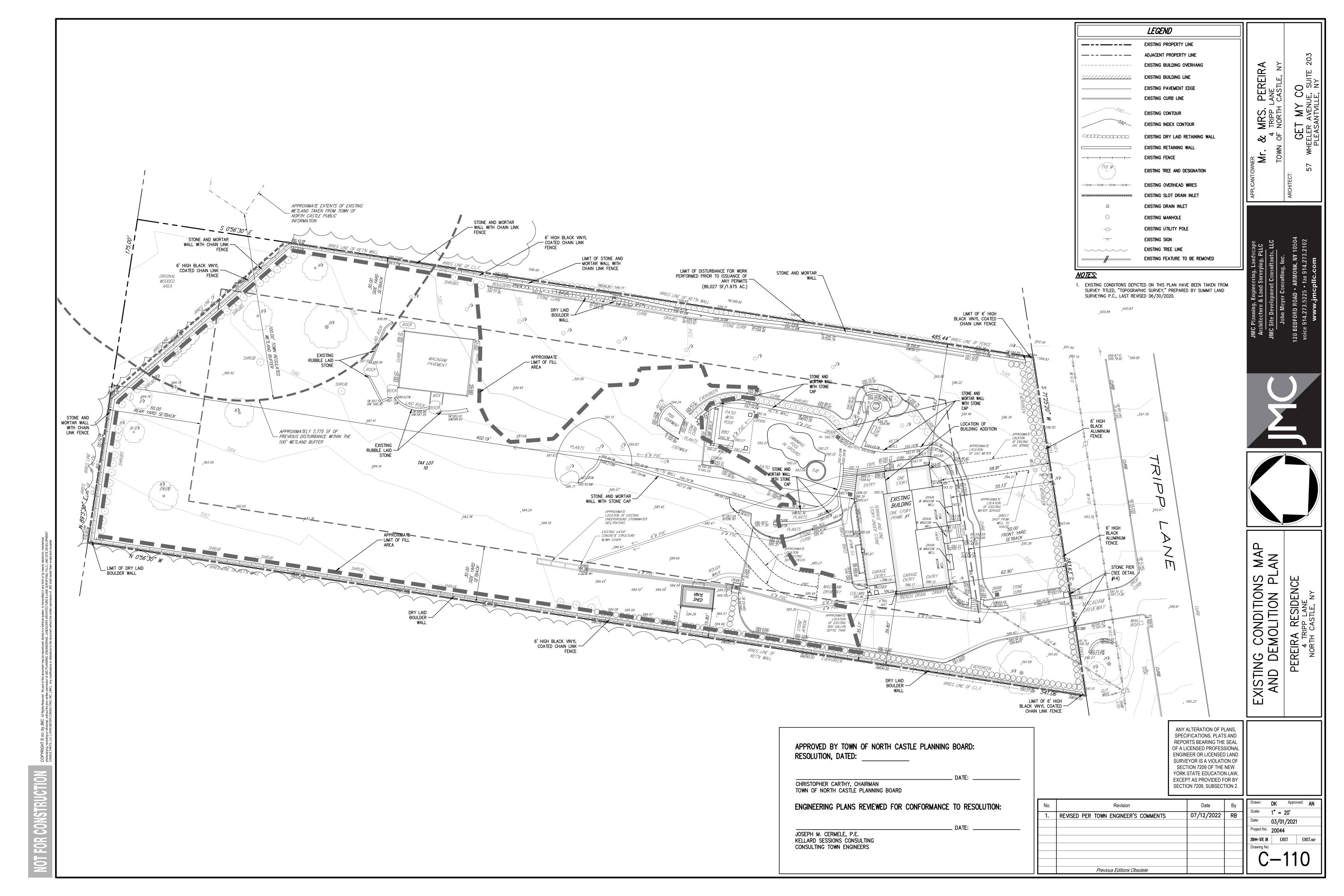
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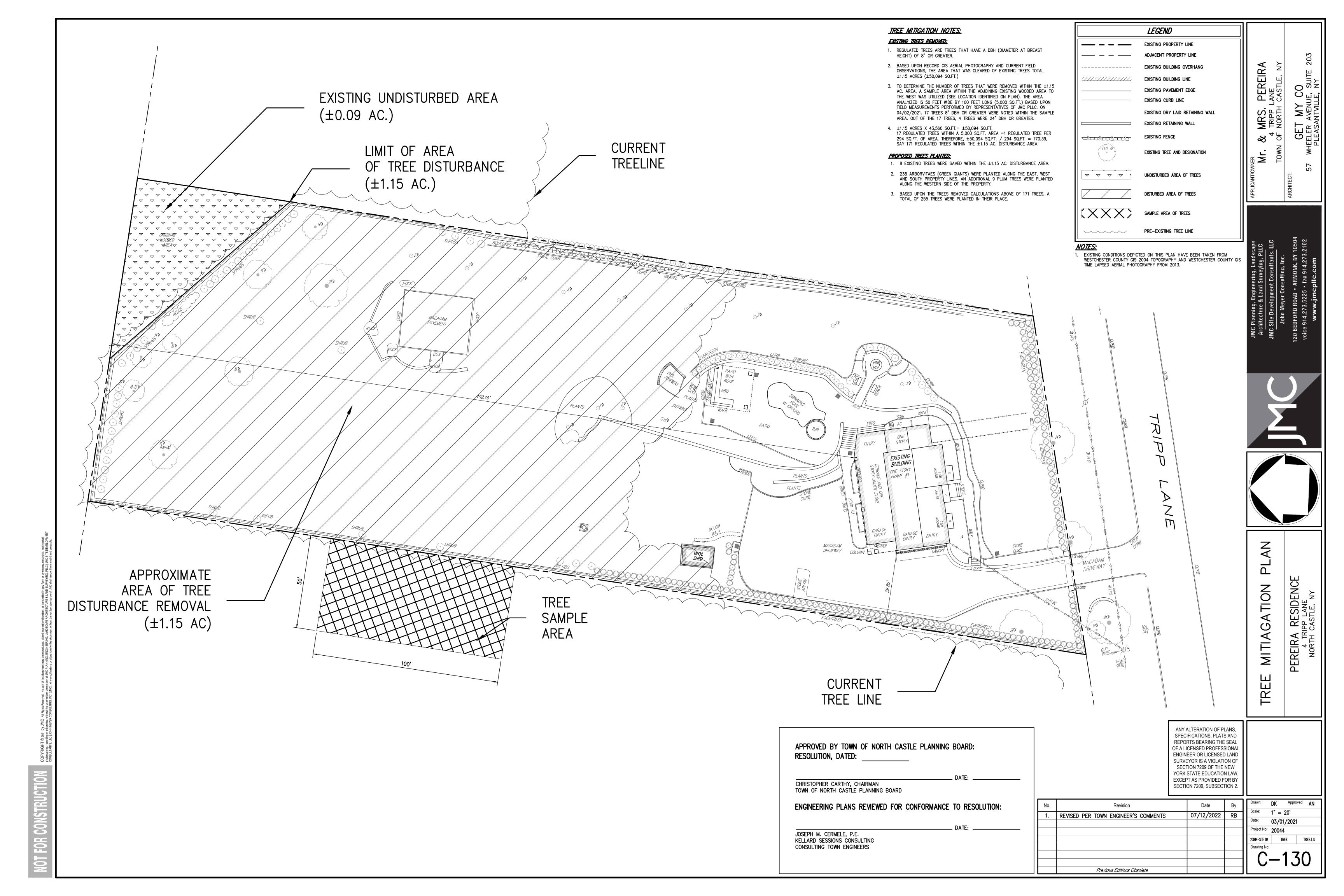
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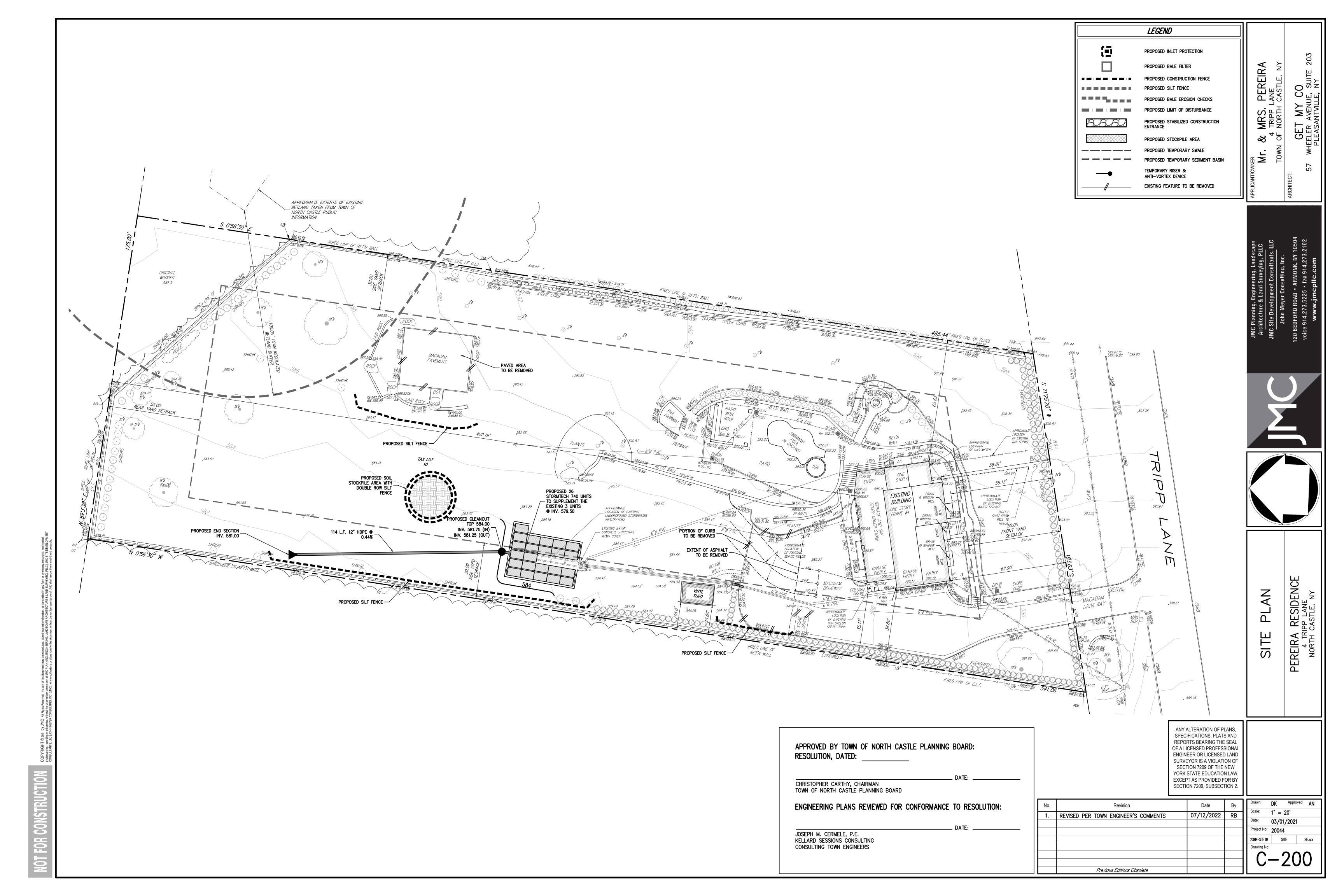
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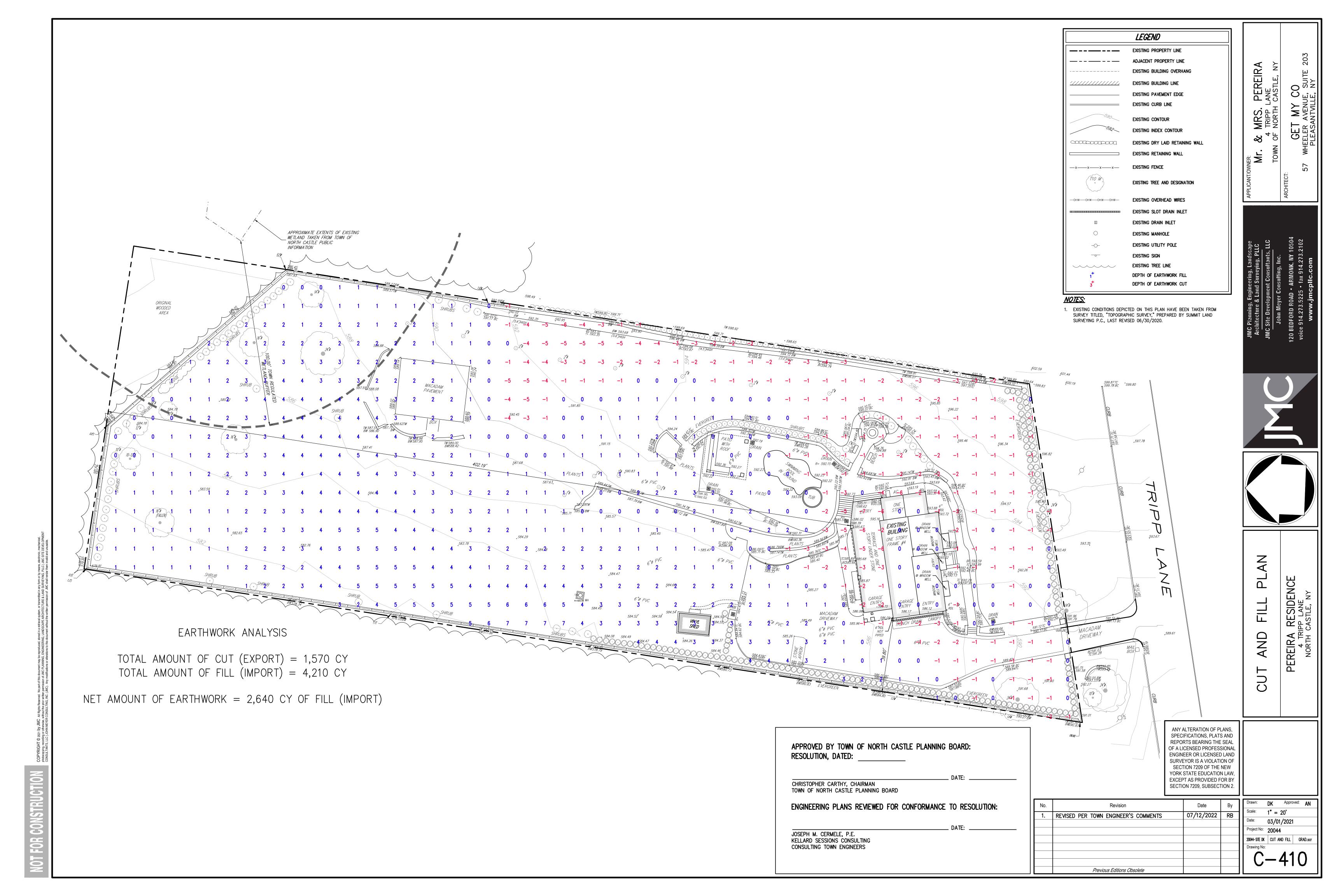
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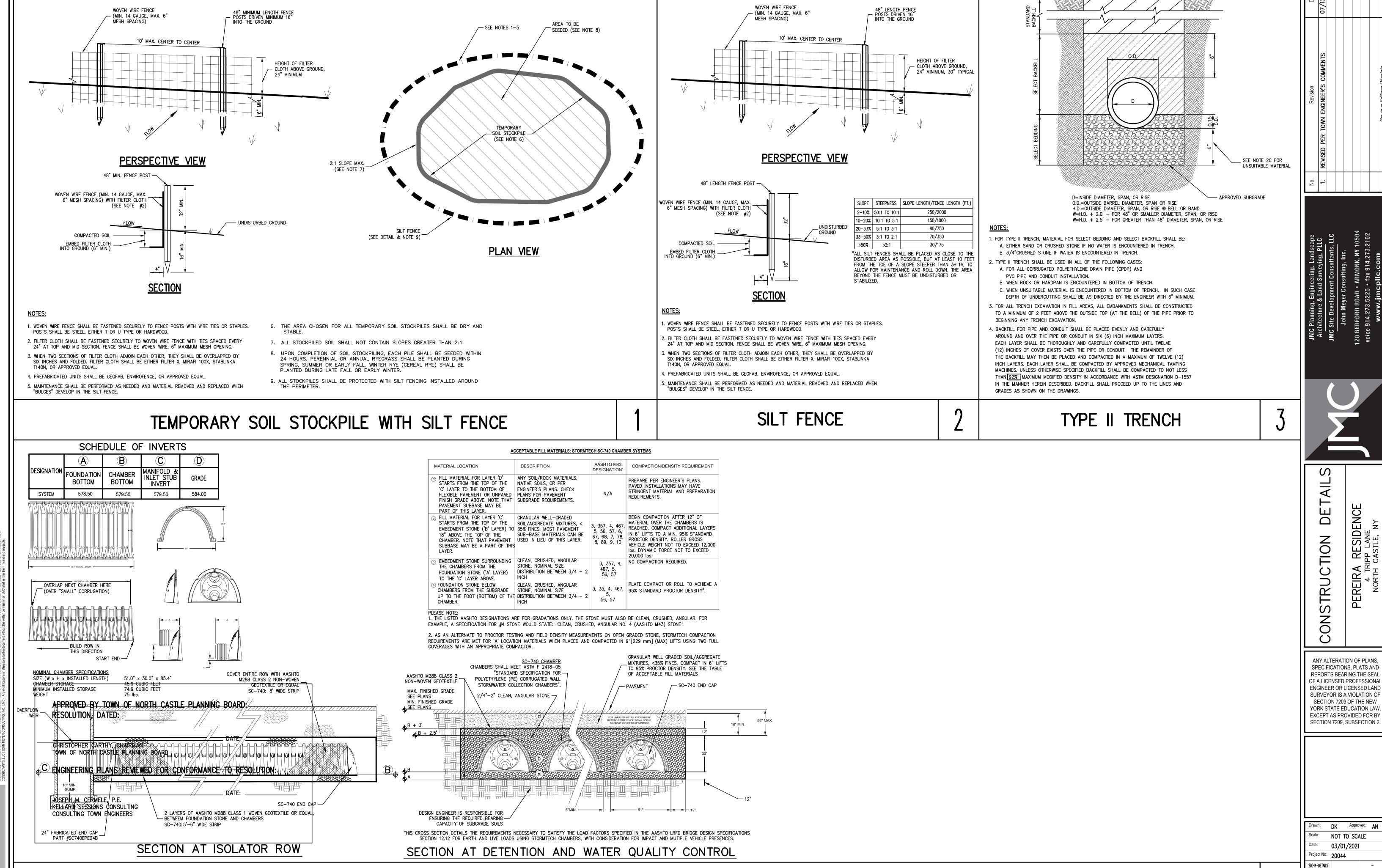












STORMTECH CHAMBERS SC-740

A-2 WHEN STEPS ARE REQUIRED, STEPS SHALL COMPLY WITH THE SAME REQUIREMENTS OF ASTM STANDARD C-478, ARTICLE 13 ENTITLED "MANHOLE STEPS & LADDERS".

A-3 FOR MASONRY STRUCTURES, THE FIRST COURSE OF MASONRY SHALL BE SET IN THE CONCRETE FOUNDATION BEFORE THE CONCRETE HAS SET. CONCRETE FOUNDATION SHALL BE CLASS "A"(4000 psi) CONCRETE, TWELVE (12) INCHES THICK AND SHALL EXTEND SIX (6) INCHES BEYOND THE OUTSIDE FACE THE STRUCTURE.

A-4 IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO FURNISH AND CONSTRUCT THE PROPER SIZE STRUCTURE INCLUDING THE NECESSARY OPENINGS TO ACCOMMODATE THE WORK AS SHOWN ON THE PLANS OR ORDERED BY THE ENGINEER, AT NO ADDITIONAL COST TO THE OWNER.

A-5 ALL NECESSARY PATCHING FOR DRAIN STRUCTURES SHALL BE ACCOMPLISHED WITH NON-SHRINKING CEMENT MORTAR GROUT, APPROVED EQUAL TO SIKA-SET AS MANUFACTURED BY THE SIKA CHEMICAL

A-6 FOUNDATIONS FOR PRECAST CONCRETE STRUCTURES SHALL BE SET ON A COMPACTED LAYER OF APPROVED CRUSHED STONE HAVING A MINIMUM COMPACTED THICKNESS OF EIGHT (8) INCHES.

A-7 ALL PIPES SHALL BE CUT FLUSH WITH THE INSIDE WALL OF THE STRUCTURE.

PROVIDE REINFORCED CONCRETE TOP SLAB FOR OVERSIZED DRAIN INLETS WITH PROPER SIZE OPENING TO ACCOMMODATE INSTALLATION OF FRAME & GRATE.

A-9 FOR MASONRY STRUCTURES GREATER THAN TEN (10) FEET IN DEPTH, THICKNESS OF MASONRY WALLS SHALL BE INCREASED TO TWELVE (12) INCHES.

A-10 FOR ALL STRUCTURES GREATER THAN 10 FEET IN DEPTH, STRUCTURES SHALL PROVIDE MINIMUM INSIDE DIMENSIONS OF 4 FEET X 4 FEET.

## NOTES PERTAINING TO MANHOLES

B-1 PRECAST CONCRETE MANHOLES SHALL COMPLY WITH ASTM STANDARD C-478. MANHOLE JOINTS SHALL COMPLY WITH ASTM STANDARD C-443.

B-2 FOR PRECAST CONCRETE MANHOLES FIVE (5) FEET OR LESS IN HEIGHT, TOP CONE SECTION SHALL BE REPLACED WITH PRECAST REINFORCED CONCRETE SLAB (6" MIN. THICKNESS) WITH OPENING OF SUFFICIENT SIZE TO ACCOMMODATE MANHOLE CASTING.

B-3 FOR MANHOLES 10 FEET OR MORE IN DEPTH, MANHOLE DIAMETER SHALL BE FIVE (5) FEET.

B-4 TERMINAL MANHOLE FLOORS SHALL BE SLOPED TOWARD OUTFALL PIPE.

B-5 INVERT CHANNELS FOR PRECAST CONCRETE MANHOLES SHALL BE CONSTRUCTED OF CONCRETE.

B-6 NOTES A-1, A-2, A-4, A-5, A-6 & A-7 UNDER "NOTES PERTAINING TO DRAIN INLETS" ABOVE SHALL

# NOTES PERTAINING TO PRECAST CONCRETE STRUCTURES FOR STORM DRAINS, SANITARY SEWERS AND WATER LINES

C-1 ALL PRECAST CONCRETE STRUCTURES SHALL BE DESIGNED TO ACCOMMODATE AN H-20 DESIGN LOAD.

C-2 STEPS SHALL BE LOCATED WITHIN STRUCTURE TO AVOID PLACEMENT OVER PIPES WHEN PRACTICABLE

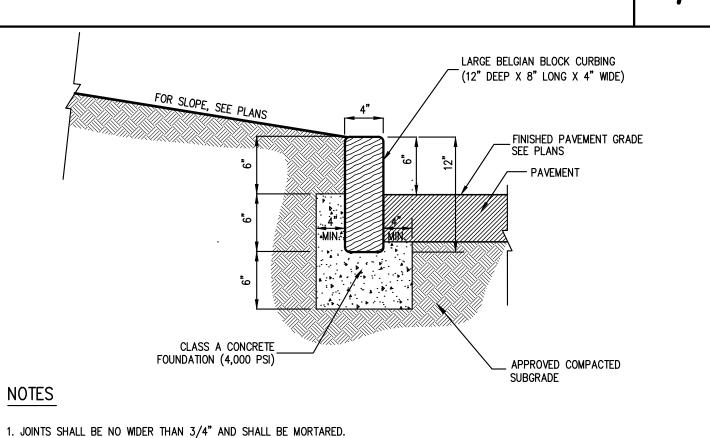
<u>PLAN</u> FRAME & GRATE: CAMPBELL FOUNDRY Co. FINISHED GRADE — No. 2815 OR APPROVED EQUAL STEPS AT 12" O.C. CAST 2'-0" SEE NOTE A-10 IRON OR POLYPROPYLENE -BRICK FOR ADJUSTMENT OR COATED STEEL PRECAST CONCRETE RINGS (SEE DRAINAGE NOTE A-2) (12" MAX.) FOR SIZE AND INVERT, SEE PLAN OR PROFILE 6" SOLID CONC. BLOCK OR PRECAST CONCRETE REINFORCEMENT AS REQUIRED FOR PRECAST CONCRETE SEE DRAINAGE NOTE A-3 FOR CONCRETE FOUNDATION FOR CONCRETE BLOCK STRUCTURES APPROVED COMPACTED CRUSHED STONE FOUNDATION COURSE SECTION A-A APPROVED SUBGRADE

SEE NOTE A-10

1. SEE NOTES PERTAINING TO DRAIN INLETS UNDER UTILITY NOTES ON THIS DRAWING.

LAWN OR LANDSCAPING (SEE PLANS) DRIVEWAY WIDTH APPROVED COMPACTED — SUBGRADE 2" TOP COURSE MATERIAL: ASPHALT CONCRETE, TYPE 6F NOTES: MIX/ITEM: NYSDOT ITEM 403.1701 THICKNESSES INDICATED REFER TO COMPACTED MEASURES. . MATERIAL AND MIX/ITEM NUMBERS REFER TO: 6" BASE/SUBBASE COURSE NEW YORK STATE MATERIAL: SUBBASE, TYPE 4 DEPARTMENT OF TRANSPORTATION MIX/ITEM: NYSDOT ITEM 304.05 STANDARD SPECIFICATIONS

SITE DRIVEWAY



\_\_CONTINUOUS TOP RAIL TWISTED AND BARBED TOP OF WALL GALVANIZED HIGH CARBON STEEL COIL SPRING TENSION WIRE TIES 12" O.C.

POST SETTING 6'-1" CENTER TO CENTER

CLEAR BETWEEN PICKETS

CHAIN LINK FENCE

ANY ALTERATION OF PLANS SPECIFICATIONS, PLATS AND REPORTS BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER OR LICENSED LAND SURVEYOR IS A VIOLATION OF SECTION 7209 OF THE NEW YORK STATE EDUCATION LAW, EXCEPT AS PROVIDED FOR BY SECTION 7209, SUBSECTION 2.

UTILITY NOTES

LAWN INLET (TYPE LI)

STONE CURB (BELGIAN BLOCK)

JOINTS SHALL BE FULLY FILLED WITH 1:2 CEMENT MORTAR, NEATLY

POINTED AND CLEANED OF EXCESS MORTAR.

SKIRT SECTION

**TYPICAL** 

CROSS-SECTION "

CONNECTOR SECTION

- REINFORCED EDGE

BLACK ALUMINUM FENCE

INTERMEDIATE POST-

SPECIFICATIONS:

END POSTS: 4"x4"

1"x1"

3/4" x 1 1/2"

POSTS, RAILS : & PICKETS

INTERMEDIATE POSTS:

RAILS:

COLOR:

PICKETS:

PIPE DIM. **ALTERNATE CONNECTION** 

2'-10" X 3'-1" 6'-0" HT. @ CENTER 5'-0" HT. @ CONNECTION TO PIER



DRY LAID BOULDER WALL

STEPS (SEE UTILITY NOTES

A-1, A-2 AND C-2)

STONE AND MORTAR WALL



HOLES ON 12" CENTERS MAX. **ELEVATION** 1. Toe plate to be punched to match holes in skirt Lip. 3/8" galv bolts to be furnished. Length of toe plate is W+10" for 12" to 30" dia. Pipe and W+22" for 36" to 60" dia. Pipe. 2. Skirt section for 12" to 30" dia. Pipe to be made in one piece. SKIRT SECTION OF 36" TO 54" DIA. PIPE MAY BE MADE FROM TWO SHEETS JOINED BY RIVETING OR BOLTING ON CENTER LINE, 60" MAY BE CONSTRUCTED IN 3 PIECES. CONNECTOR SECTION, CORNER PLATE AND TOE PLATE TO BE SAME SHEET THICKNESS AS SKIRT 5. END—SECTIONS AND FITTINGS ARE TO BE GALVANIZED STEEL OR ALUMINIUM ALLOY FOR USE WITH LIKE PIPE. 6. WHERE FLARED END—SECTIONS ARE TO BE USED WITH BITUMINOUS COATED AND PAVED METAL PIPE,

JOSEPH M. CERMELE, P.E. KELLARD SESSIONS CONSULTING CONSULTING TOWN ENGINEERS

ENGINEERING PLANS REVIEWED FOR CONFORMANCE TO RESOLUTION:

APPROVED BY TOWN OF NORTH CASTLE PLANNING BOARD:

RESOLUTION, DATED:

CHRISTOPHER CARTHY, CHAIRMAN

TOWN OF NORTH CASTLE PLANNING BOARD

GATE AND STONE PIER

STONE AND MORTAR WALL

SHED (WITH PATIO REMOVED) END SECTION

NOT TO SCALE 03/01/2021



#### **TOWN OF NORTH CASTLE**

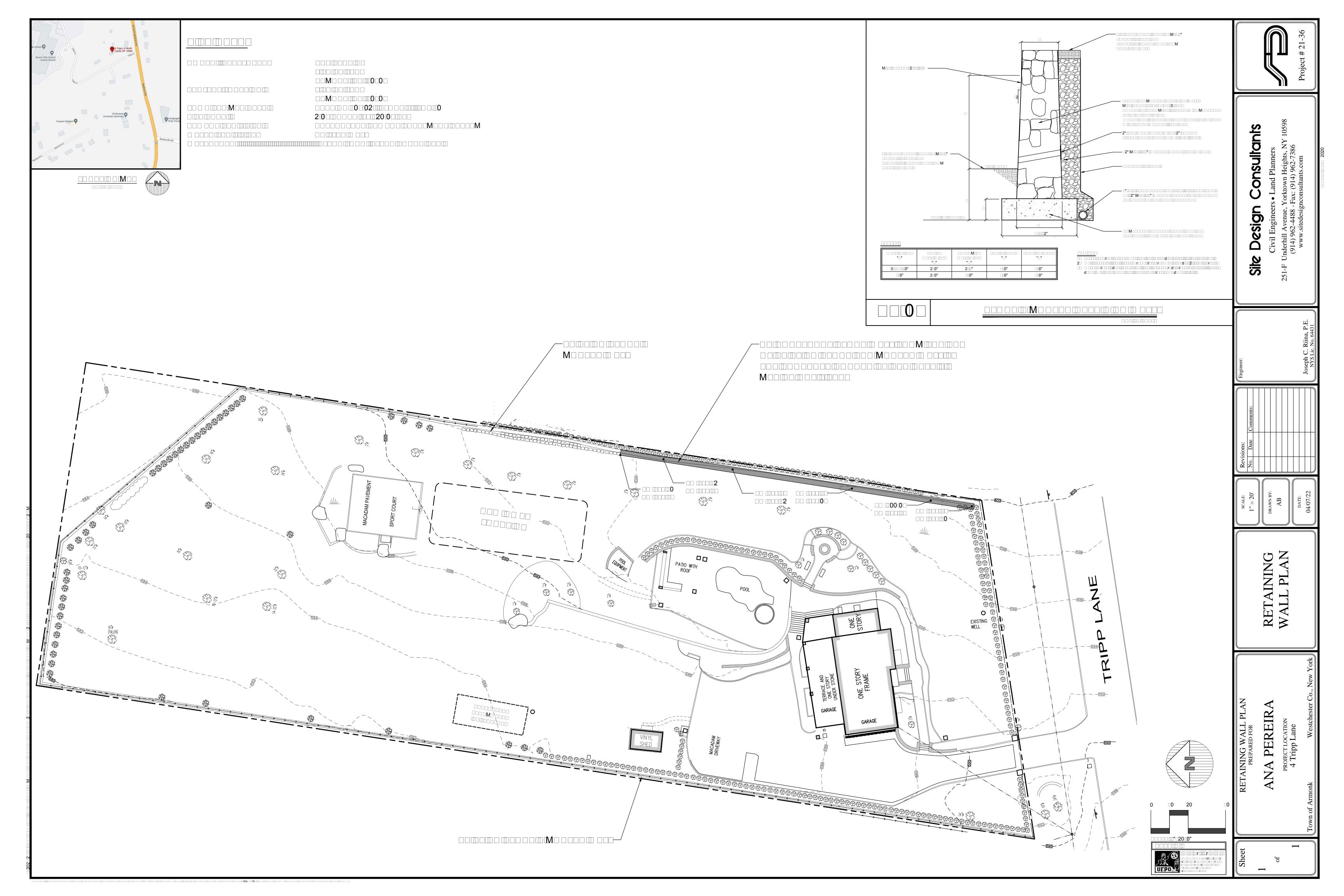
#### WESTCHESTER COUNTY 17 Bedford Road Armonk, New York 10504-1898

#### PLANNING DEPARTMENT Adam R. Kaufman, AICP Director of Planning

Telephone: (914) 273-3542 Fax: (914) 273-3554 www.northcastleny.com

#### FLOOR AREA CALCULATIONS WORKSHEET

Applica	ntion Name or Identifying Title:	Pereira residence	Date: 9-16-20
Tax Ma	p Designation or Proposed Lot No.:	108.02-1-10	
Floor A			
1.	Total Lot Area (Net Lot Area for Lo	ots Created After 12/13/06):	89820
2.	Maximum permitted floor area (pe	r Section 213-22.2B):	10230
3.	Amount of floor area contained wit $1803$ existing + $0$		1803
4.	Amount of floor area contained wit $\underline{0}$ existing $+\underline{0}$	hin second floor: _ proposed =	
5.	Amount of floor area contained wit $\underline{0}$ existing $+\underline{0}$	hin garage: _ proposed = NOT A STORY	0
6.	Amount of floor area contained wit 22 existing + 0	hin porches capable of being enclosed: _ proposed =	22
7.	Amount of floor area contained wit 0 existing +	hin basement (if applicable – see definition): _ proposed = NOT A STORY	0
8.	Amount of floor area contained wit 0 existing + 0	hin attic (if applicable – see definition): _ proposed =	0
9.	Amount of floor area contained wit 0 existing + 0	hin all accessory buildings: _ proposed =	0
10.	Proposed <b>floor area:</b> Total of Lines	s 3 - 9 =	1825: OK
and the		our proposal <b>complies</b> with the Town's maxing Project Review Committee for review. If Linguist regulations.	
	STERED ARCA		9-16-20
Signatu	re ing	g Worksheet	Date



# Site Design Consultants

Civil Engineers • Land Planners

April 18, 2022

Robert Melillo, Building Inspector Town of North Castle 17 Bedford Road Armonk, NY 10504

Re: Pereira – 4 Trip Lane, Armonk

Dear Mr. Melillo:

We have been retained by the Pereira Family regarding retaining walls which have been constructed on their property without filing for the required permits to your department, specifically, the stone and mortar walls along the east and west property lines. The walls along the east property line are only partially being considered as part of the existing walls to remain. An additional length of dry stacked stone wall along the east property line is to be removed and reconstructed as per the enclosed plan.

As stated, the existing walls to remain were constructed by the homeowner without filing the proper construction plans and permits. Hence, the construction of the walls were not supervised or inspected by a town official or licensed design professional. We, therefore, cannot attest to the construction. However, we did inspect the walls in their current state. We specifically were looking for any signs of movement such as collapse, settlement, bowing out, or leaning of the wall. We found none of these conditions. The wall appears to be sound and stable. We, therefore, believe the walls at this point in time appear to be structurally sound.

The dry stacked portion of the east wall is to be disassembled and rebuilt. This portion is about 190 lf. We have prepared a design and plan with the necessary detail to reconstruct this wall as a continuation of the stone and mortar wall. The wall has a maximum height of 5 feet. The plan and supporting calculations are enclosed for your review as follows:

- Two copies of the Plan titled "Retaining Wall Plan prepared for Ana Pereira" dated 4/7/22, Sheet 1 of 1; and
- Two copies of the Structural Wall Calculations.

If you have any question or comments, please contact us. Thank you



J. Cermele, P.E., Consulting TE

A. Nestor, P.E.



#### Proposed Retaining Wall Design Prepared for Pereira Residence 4 Tripp Lane Armonk, NY

#### Prepared By Site Design Consultants

251 F Underhill Avenue Yorktown Heights, NY 10598 April 18, 2022

Exposed Wall Height 5'

Design Parameters	v	
Top width, B	2.00	ft
Bottom width, C1	2.00	ft
Bottom width, C2	1.00	ft
Total Bottom width, C	3.00	ft
Footing depth, D	1.00	ft
Footing width, E1	0.75	ft
Footing width, E2	3.00	ft
Footing width, E3	0.50	ft
Total Footing width, E	4.25	ft
Exposed wall height, H	5.00	ft
Burried height, J	2.00	ft
Wall height (design), H'	8.00	ft
Gamma (H'/3)	2.67	ft
Unit weight of wall	170	pcf
Footing Material	Gravel	
Unit weight of footing	125	pcf
Back Angle, β	27	degrees
Unit weight of soil	110	pcf
Friction angle of soil, φ	32	degrees
Surcharge load	0	psf

#### Pressure Calculations

Ka = 0.472681

Pa = 1663.836 Pah = 1482.489 Pav = 755.366

Pa surcharge = 0.000 Pah surcharge = 0.000

Pav surcharge = 0.000

		ь
	0	β
H'	Н	
<u> </u>	J	
		<b>←</b>
		C1 C2
2 <	E1	C E2 E3
	,	E

Resisting I	<b>Moment</b>			
		Weight	Arm	Moment
Wall	Part 1	2380.00	1.75	4165.00
	Part 2	595.00	3.08	1834.58
Footing		531.25	2.13	1128.91
Pav		755.37	4.25	3210.30
Sum		4261.62		10338.79



Proposed Retaining	Wall Desi 4 Tripp La			ira Residence
	erhill Avenue		Consultants Heights, NY 10	598
Overturning Moment	0	Arm	Moment	
Pah Pah surcharge <b>Total overturning Moment</b>	1482.49 0.00	2.67 4.00 <b>3953.30</b>	3953.30 0.00	
FS overturning				
$M_{resisting}/M_{overturning} =$	2.615229	> 1.50	ок	444
Resisting Forces f = tan (φ) =			÷	
F <sub>resisting</sub> = Sum Weight * f =	2662.953			
F <sub>resisting</sub> / Pah =	1.796272	> 1.50	ок	
Eccentricity			4	
$\bar{x} = \Sigma M_{toe} / \Sigma W$		* 2		
<del>x</del> =	1.50	CW mor	ment is +	Bowles pg 455
e =	B/2- x		*	-
e =	0.63	<=L/6	ОК	N.A.
Allowable Bearing Forces			1	
' q <sub>allow</sub> =	6000	psf		
q <sub>actual</sub> =	P/A*(1+	6e/L)		
q actual =	115.6656	MIN		
q actual =	1889.801	MAX		i i
FS Bearing			¥:	
q allow / q actual =	3.174938	> 2.0	ок	

#### Proposed Retaining Wall Design Prepared for Pereira Residence 4 Tripp Lane Armonk, NY

#### Prepared By Site Design Consultants

251 F Underhill Avenue Yorktown Heights, NY 10598 April 18, 2022

Exposed Wall Height 5'

Design Parameters		
Top width, B	2.00	ft
Bottom width, C1	2.00	ft
Bottom width, C2	1.00	ft
Total Bottom width, C	3.00	ft
Footing depth, D	1.00	ft
Footing width, E1	0.75	ft
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Footing width, E3	0.50	ft
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Footing Material	Gravel	
Unit weight of footing	125	pcf
Back Angle, β	27	degrees
Unit weight of soil	110	pcf
Friction angle of soil, φ	32	degrees
Surcharge load	0	psf

#### **Pressure Calculations**

Ka = 0.472681

Pa = 1663.836 Pah = 1482.489

Pav = 755.366

Pa surcharge = 0.000

Pah surcharge = 0.000

Pav surcharge = 0.000

н	Н			
	J			
6		C1	C2	<b>+</b>
•	E1	4	C E2	▶ <b>∢</b> E3 ▶
	•	E		
oment 165.00				

Resisting N	/loment			
		Weight	Arm	Moment
Wall	Part 1	2380.00	1.75	4165.00
	Part 2	595.00	3.08	1834.58
Footing		531.25	2.13	1128.91
Pav		755.37	4.25	3210.30
Sum		4261.62		10338.79

Proposed Retaining	Wall Desi 4 Tripp La			a Residence
Prepar	ed By <b>Site</b> erhill Avenue	Design C	onsultants Heights, NY 105	98
Overturning Moment				
Pah Pah surcharge <b>Total overturning Moment</b>	1482.49 0.00	Arm 2.67 4.00 <b>3953.30</b>	Moment 3953.30 0.00	
FS overturning				
$M_{resisting}/M_{overturning} =$	2.615229	> 1.50	ок	
Resisting Forces  f = tan (φ) =  F <sub>resisting</sub> = Sum Weight * f =				
FS Sliding			The state of	<u> </u>
F <sub>resisting</sub> / Pah =	1.796272	> 1.50	ок	
Eccentricity				
$\overline{x} = \sum M_{\text{toe}} / \sum W$	1.50	CW mor	nent is +	Bowles pg 455
e =	B/2- x		3	·
e =	0.63	<=L/6	ок	N.A.
Allowable Bearing Forces				
q <sub>allow</sub> =	6000	psf	5	
q <sub>actual</sub> =	P/A*(1+	6 <mark>e/L</mark> )		
q actual =	115.6656	MIN		
q actual =	1889.801	MAX		
FS Bearing				
q allow / q actual =	3.174938	> 2.0	ОК	5.67.5



Site Planning
Civil Engineering
Landscape Architecture
Land Surveying
Transportation Engineering

Environmental Studies Entitlements Construction Services 3D Visualization Laser Scanning

#### STORMWATER POLLUTION PREVENTION PLAN

JMC Project 20044
Residential Zoning Compliance Analysis
4 Tripp Lane
Town of North Castle, New York
July 12, 2022

#### I. INTRODUCTION

This report has been prepared to study the stormwater management aspects of the previous improvements performed by the client prior to the Town's approval and subsequent proposed drainage improvements located at the above address.

The previous improvements included the expansion of the residence, the installation of a pool patio, the installation of a separate patio area located in the backyard, the installation of a basketball court in the backyard and driveway improvements. These previous improvements have increased the square footage of impervious surfaces which will now require stormwater runoff mitigation. These improvements also increased the coverage numbers of the Site over the permitted limit. The applicant is proposing to remove approximately 2,750 square feet of impervious area (the basketball court and a large portion of the driveway) to comply with this requirement.

A hydrologic analysis of the overall site and its sub-drainage areas studied herein was prepared using the USDA Soil Conservation Service TR-55 "Urban Hydrology for Small Watersheds" methodology for the following rainfall event shown in Table 1:

#### <u>Table I</u> <u>TR-55 24 Hour Rainfall Depths</u>

Rainfall depths shown in the table above for the Town of North Castle in Westchester County are taken from the Extreme Precipitation Tables from the Northeast Regional Climate Center 24-hour rainfall frequency data from Cornell University's precip.net.

As detailed below, the previous improvements have caused a net increase in the overall impervious surfaces which will be mitigated by the installation of an additional 23-Stormtech 740 units to supplement the previously installed 3 units. This system will reduce the peak rate of runoff and runoff volume associated with the previous improvements when compared to the pre-existing conditions for the 100-year storm event.

JMC Planning Engineering Landscape Architecture & Land Surveying, PLLC | JMC Site Development Consultants, LLC

#### II. EXISTING CONDITIONS

Under pre-existing conditions, the Site, in general drains from north to south towards the adjacent lot and eventually towards Byram Hills High School. Three areas were identified as areas where stormwater runoff exits the project site, all located along the southern property line. To simplify the stormwater study, one single design line was used instead of three separate design points, and peak rates of runoff and runoff volumes were reduced at this design line, which incorporates all runoff from the project site.

Existing Drainage Area I (EDA-I) is approximately 2.062 acres and includes the entire project site. Stormwater from this drainage area drains from north to south towards the adjacent lot and eventually towards Byram Hills High School. All runoff leaves the project site along the southern property line which will be designated as Design Line #I, as shown on drawing DA-I. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 73 and 9.66 minutes, respectively. Refer to Drawing DA-I in Appendix C.

#### III. PROPOSED CONDITIONS

As mentioned above, the previous improvements included the expansion of the residence, the installation of a pool patio, the installation of a separate patio area located in the backyard, the installation of a basketball court in the backyard and driveway improvements. These previous improvements have increased the square footage of impervious surfaces which will now require stormwater runoff mitigation. These improvements also increased the coverage numbers of the Site over the permitted limit. The applicant is proposing to remove approximately 2,750 square feet of impervious area (the basketball court and a large portion of the driveway) to comply with this requirement. The previous improvements have caused a net increase in the overall impervious surfaces which will be mitigated by the installation of an additional 23-Stormtech 740 units to supplement the previously installed 3 units. This system will reduce the peak rate of runoff and runoff volume associated with the previous improvements when compared to the pre-existing conditions for the 100-year storm event.

<u>Proposed Drainage Area I (PDA-I)</u> is approximately 1.399 acres, is in the western portion of the site and includes much of the project site. Stormwater from this drainage area drains from north to south towards the adjacent lot and eventually towards Byram Hills High School. All runoff leaves the project site along the southern property line which is designated as Design Line #I, as shown on drawing DA-2. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 74 and 9.18 minutes, respectively. Refer to Drawing DA-2 in Appendix C.

Proposed Drainage Area IA (PDA-IA) is approximately 0.136 acres and is located in the central portion of the project site. This area includes the pool and improved pool patio area. Stormwater from this drainage area is collected in several inlets dispersed throughout the patio area and under current conditions is being daylighted in the backyard but under proposed conditions will be conveyed to the improved underground infiltration system that will consist of 26-Stormtech 740 units. This system will outlet in the backyard near where the previous outlet had been located. Runoff then drains towards the adjacent lot and eventually towards Byram Hills High School. All runoff leaves the project site along the southern property line which will be designated as Design Line #1, as shown on drawing DA-2. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 88 and 5.00 minutes, respectively. Refer to Drawing DA-2 in Appendix C.

Proposed Drainage Area 1B (PDA-1B) is approximately 0.527 acres and is located in the eastern portion of the project site. This area includes the residence, driveway, shed, walkways and landscaped areas. Stormwater from this drainage area is collected in several inlets dispersed throughout this drainage area and under current conditions is being conveyed to the existing underground infiltration system in the backyard. Under proposed conditions runoff from this area will continue to be conveyed to this underground infiltration system that will now consist of 26-Stormtech 740 units. This system will outlet in the backyard near where the previous outlet had been located. Runoff then drains towards the adjacent lot and eventually towards Byram Hills High School. All runoff leaves the project site along the southern property line which will be designated as Design Line #1, as shown on drawing DA-2. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 84 and 8.94 minutes, respectively. Refer to Drawing DA-2 in Appendix C.

The numbers included in the tables below were obtained from calculations included in Appendix A & B of this report.

<u>Table 2</u>
<u>Percent Reduction in Peak Rate of Runoff (Existing vs. Proposed Conditions)</u>
(Cubic Feet per Second)

Storm Recurrence Frequency (Years)	Existing Peak Runoff Rate (cfs) Design Line I	Proposed Peak Runoff Rate (cfs) Design Line I	Percent Reduction (%)
100-year	11.26	11.18	0.7

Table 3
Percent Reduction in Runoff Volume (Existing vs. Proposed Conditions)
(Cubic Feet)

Storm Recurrence Frequency (Years)	Existing Runoff Volume (cf) Design Line I	Proposed Runoff Volume (cf) Design Line I	Percent Reduction (%)
100-year	43,587	34,502	20.8

#### IV. CONCLUSION

Based on the foregoing, it is our professional opinion that the previous improvements will not have an adverse drainage impact to the site, adjacent properties, or downstream areas with the installation of an additional 23-Stormtech 740 units.

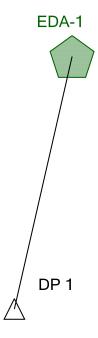
Respectfully Submitted

JMC

Rick Bohlander, PE Senior Designer II

P:\2020\20044\DRAINAGE\REPORTS\2022-07-11\_rb\Storm Report 07-12-2022.doc

# APPENDIX A EXISTING HYDROLOGIC CALCULATIONS



# **Table of Contents**

	Master Network Summary	1
Armonk	Time-Depth Curve, 100 years (4 Tripp Street - Synthetic Curve, 100 yrs)	2
EDA-1	Time of Concentration Calculations, 100 years (4 Tripp Street - Synthetic Curve, 100 yrs)	4
EDA-1	Runoff CN-Area, 100 years (4 Tripp Street - Synthetic Curve, 100 yrs)	6

Subsection: Master Network Summary

# **Catchments Summary**

Label	Scenario	Return Event (years)	Hydrograph Volume (ft³)	Time to Peak (hours)	Peak Flow (ft³/s)
EDA-1	4 Tripp Street - Synthetic Curve, 100 yrs	100	43,587.000	12.150	11.26

# **Node Summary**

Label	Scenario	Return Event (years)	Hydrograph Volume (ft³)	Time to Peak (hours)	Peak Flow (ft³/s)
DP 1	4 Tripp Street - Synthetic Curve, 100 yrs	100	43,587.000	12.150	11.26

Subsection: Time-Depth Curve Return Event: 100 years Storm Event: 100 Year Label: Armonk

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Time-Depth Curve: 100 Year	
Label	100 Year
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	100 years

#### **CUMULATIVE RAINFALL (in) Output Time Increment = 0.100 hours** Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.1	0.1	0.1	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.2	0.2	0.2
2.000	0.2	0.2	0.2	0.2	0.2
2.500	0.2	0.2	0.2	0.3	0.3
3.000	0.3	0.3	0.3	0.3	0.3
3.500	0.3	0.3	0.4	0.4	0.4
4.000	0.4	0.4	0.4	0.4	0.4
4.500	0.5	0.5	0.5	0.5	0.5
5.000	0.5	0.5	0.5	0.6	0.6
5.500	0.6	0.6	0.6	0.6	0.6
6.000	0.7	0.7	0.7	0.7	0.7
6.500	0.7	0.8	0.8	0.8	0.8
7.000	0.8	0.8	0.9	0.9	0.9
7.500	0.9	0.9	1.0	1.0	1.0
8.000	1.0	1.1	1.1	1.1	1.1
8.500	1.2	1.2	1.2	1.3	1.3
9.000	1.3	1.4	1.4	1.4	1.5
9.500	1.5	1.6	1.6	1.6	1.7
10.000	1.7	1.8	1.8	1.9	1.9
10.500	2.0	2.0	2.1	2.2	2.2
11.000	2.3	2.4	2.4	2.5	2.6
11.500	2.7	2.9	3.1	3.4	3.8
12.000	4.6	5.3	5.7	6.0	6.3
12.500	6.4	6.5	6.6	6.7	6.8
13.000	6.8	6.9	7.0	7.0	7.1
13.500	7.2	7.2	7.3	7.3	7.4
14.000	7.4	7.4	7.5	7.5	7.6
14.500	7.6	7.7	7.7	7.7	7.8
15.000	7.8	7.8	7.9	7.9	7.9
15.500	8.0	8.0	8.0	8.0	8.1
16.000	8.1	8.1	8.1	8.2	8.2
16.500	8.2	8.2	8.2	8.3	8.3

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Subsection: Time-Depth Curve Return Event: 100 years Label: Armonk Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# CUMULATIVE RAINFALL (in) Output Time Increment = 0.100 hours Time on left represents time for first value in each row.

Time	Depth	Depth	Depth	Depth	Depth			
(hours)	(in)	(in)	(in)	(in)	(in)			
17.000	8.3	8.3	8.3	8.4	8.4			
17.500	8.4	8.4	8.4	8.4	8.5			
18.000	8.5	8.5	8.5	8.5	8.5			
18.500	8.5	8.6	8.6	8.6	8.6			
19.000	8.6	8.6	8.6	8.7	8.7			
19.500	8.7	8.7	8.7	8.7	8.7			
20.000	8.7	8.7	8.8	8.8	8.8			
20.500	8.8	8.8	8.8	8.8	8.8			
21.000	8.9	8.9	8.9	8.9	8.9			
21.500	8.9	8.9	8.9	8.9	8.9			
22.000	9.0	9.0	9.0	9.0	9.0			
22.500	9.0	9.0	9.0	9.0	9.0			
23.000	9.0	9.1	9.1	9.1	9.1			
23.500	9.1	9.1	9.1	9.1	9.1			
24.000	9.1	(N/A)	(N/A)	(N/A)	(N/A)			

Subsection: Time of Concentration Calculations

Label: EDA-1

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

#### Time of Concentration Results

Time or concentration results						
Segment #1: TR-55 Sheet Flow						
Hydraulic Length	60.00 ft					
Manning's n	0.400					
Slope	0.067 ft/ft					
2 Year 24 Hour Depth	3.4 in					
Average Velocity	0.12 ft/s					
Segment Time of Concentration	0.142 hours					
Segment #2: TR-55 Shallow Cond	centrated Flow					
Hydraulic Length	200.00 ft					
Is Paved?	False					
Slope	0.035 ft/ft					
Average Velocity	3.02 ft/s					
Segment Time of Concentration	0.018 hours					
Time of Concentration (Composite	e)					
Time of Concentration (Composite)	0.161 hours					

Return Event: 100 years Storm Event: 100 Year

Subsection: Time of Concentration Calculations Return Event: 100 years

Label: EDA-1 Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

#### ==== SCS Channel Flow

Tc = R = Qa / Wp

V = (1.49 \* (R\*\*(2/3)) \* (Sf\*\*-0.5)) / n

(Lf / V) / 3600

Where: R= Hydraulic radius

Aq= Flow area, square feet Wp= Wetted perimeter, feet

V= Velocity, ft/sec Sf= Slope, ft/ft n= Manning's n

Tc= Time of concentration, hours

Lf= Flow length, feet

#### ==== SCS TR-55 Shallow Concentration Flow

Tc = Unpaved surface:

V = 16.1345 \* (Sf\*\*0.5)

Paved Surface:

V = 20.3282 \* (Sf\*\*0.5)

(Lf / V) / 3600

Where: V= Velocity, ft/sec

Sf= Slope, ft/ft

Tc= Time of concentration, hours

Lf= Flow length, feet

Subsection: Runoff CN-Area Return Event: 100 years Label: EDA-1 Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Soil/Surface Description	CN	Area (ft²)	C (%)	UC (%)	Adjusted CN
Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil C	74.000	31,144.000	0.0	0.0	74.000
Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil C	98.000	5,160.000	0.0	0.0	98.000
Woods - good - Soil C	70.000	53,516.000	0.0	0.0	70.000
COMPOSITE AREA & WEIGHTED CN>	(N/A)	89,820.000	(N/A)	(N/A)	72.996

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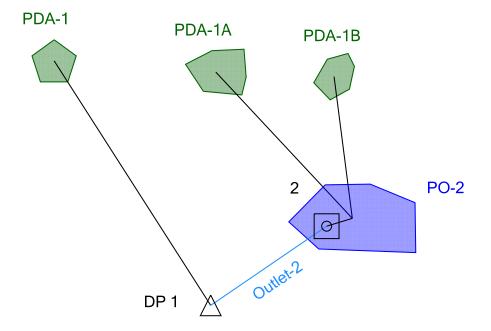
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Master Network Summary...1

# APPENDIX B PROPOSED HYDROLOGIC CALCULATIONS

# Scenario: 4 Tripp Street - Synthetic Curve, 1 yrs



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Subsection: Master Network Summary

# **Catchments Summary**

Label	Scenario	Return Event (years)	Hydrograph Volume (ft³)	Time to Peak (hours)	Peak Flow (ft³/s)
PDA-1	4 Tripp Street - Synthetic Curve, 100 yrs	100	30,194.000	12.150	7.79
PDA-1A	4 Tripp Street - Synthetic Curve, 100 yrs	100	3,788.000	12.100	0.99
PDA-1B	4 Tripp Street - Synthetic Curve, 100 yrs	100	13,756.000	12.100	3.45

#### **Node Summary**

Label	Scenario	Return Event (years)	Hydrograph Volume (ft³)	Time to Peak (hours)	Peak Flow (ft³/s)
DP 1	4 Tripp Street - Synthetic Curve, 100 yrs	100	34,502.000	12.150	11.18

# **Pond Summary**

Label	Scenario	Return Event (years)	Hydrograph Volume (ft³)	Time to Peak (hours)	Peak Flow (ft³/s)	Maximum Water Surface Elevation (ft)	Maximum Pond Storage (ft³)
PO-2 (IN)	4 Tripp Street - Synthetic Curve, 100 yrs	100	17,544.000	12.100	4.44	(N/A)	(N/A)
PO-2 (OUT)	4 Tripp Street - Synthetic Curve, 100 yrs	100	4,308.000	12.150	3.39	583.83	2,495.000

Subsection: Time-Depth Curve Return Event: 100 years
Label: Armonk Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Time-Depth Curve: 100 Year	
Label	100 Year
Start Time	0.000 hours
Increment	0.100 hours
End Time	24.000 hours
Return Event	100 years

# CUMULATIVE RAINFALL (in) Output Time Increment = 0.100 hours Time on left represents time for first value in each row.

Time (hours)	Depth (in)	Depth (in)	Depth (in)	Depth (in)	Depth (in)
0.000	0.0	0.0	0.0	0.0	0.0
0.500	0.0	0.1	0.1	0.1	0.1
1.000	0.1	0.1	0.1	0.1	0.1
1.500	0.1	0.1	0.2	0.2	0.2
2.000	0.2	0.2	0.2	0.2	0.2
2.500	0.2	0.2	0.2	0.3	0.3
3.000	0.3	0.3	0.3	0.3	0.3
3.500	0.3	0.3	0.4	0.4	0.4
4.000	0.4	0.4	0.4	0.4	0.4
4.500	0.5	0.5	0.5	0.5	0.5
5.000	0.5	0.5	0.5	0.6	0.6
5.500	0.6	0.6	0.6	0.6	0.6
6.000	0.7	0.7	0.7	0.7	0.7
6.500	0.7	0.8	0.8	0.8	0.8
7.000	0.8	0.8	0.9	0.9	0.9
7.500	0.9	0.9	1.0	1.0	1.0
8.000	1.0	1.1	1.1	1.1	1.1
8.500	1.2	1.2	1.2	1.3	1.3
9.000	1.3	1.4	1.4	1.4	1.5
9.500	1.5	1.6	1.6	1.6	1.7
10.000	1.7	1.8	1.8	1.9	1.9
10.500	2.0	2.0	2.1	2.2	2.2
11.000	2.3	2.4	2.4	2.5	2.6
11.500	2.7	2.9	3.1	3.4	3.8
12.000	4.6	5.3	5.7	6.0	6.3
12.500	6.4	6.5	6.6	6.7	6.8
13.000	6.8	6.9	7.0	7.0	7.1
13.500	7.2	7.2	7.3	7.3	7.4
14.000	7.4	7.4	7.5	7.5	7.6
14.500	7.6	7.7	7.7	7.7	7.8
15.000	7.8	7.8	7.9	7.9	7.9
15.500	8.0	8.0	8.0	8.0	8.1
16.000	8.1	8.1	8.1	8.2	8.2
16.500	8.2	8.2	8.2	8.3	8.3

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Subsection: Time-Depth Curve Return Event: 100 years Label: Armonk Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# CUMULATIVE RAINFALL (in) Output Time Increment = 0.100 hours Time on left represents time for first value in each row.

The contract of the contract o					
Time	Depth	Depth	Depth	Depth	Depth
(hours)	(in)	(in)	(in)	(in)	(in)
17.000	8.3	8.3	8.3	8.4	8.4
17.500	8.4	8.4	8.4	8.4	8.5
18.000	8.5	8.5	8.5	8.5	8.5
18.500	8.5	8.6	8.6	8.6	8.6
19.000	8.6	8.6	8.6	8.7	8.7
19.500	8.7	8.7	8.7	8.7	8.7
20.000	8.7	8.7	8.8	8.8	8.8
20.500	8.8	8.8	8.8	8.8	8.8
21.000	8.9	8.9	8.9	8.9	8.9
21.500	8.9	8.9	8.9	8.9	8.9
22.000	9.0	9.0	9.0	9.0	9.0
22.500	9.0	9.0	9.0	9.0	9.0
23.000	9.0	9.1	9.1	9.1	9.1
23.500	9.1	9.1	9.1	9.1	9.1
24.000	9.1	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time of Concentration Calculations

Label: PDA-1

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

#### Time of Concentration Results

Time or concentration results			
Segment #1: TR-55 Sheet Flow			
Hydraulic Length	100.00 ft		
Manning's n	0.240		
Slope	0.060 ft/ft		
2 Year 24 Hour Depth	3.4 in		
Average Velocity	0.19 ft/s		
Segment Time of Concentration	0.149 hours		
Segment #2: TR-55 Shallow Concentrated Flow			
Hydraulic Length 82.00 ft			
Is Paved?	False		
Slope	0.110 ft/ft		
Average Velocity	5.35 ft/s		
Segment Time of Concentration	0.004 hours		
Time of Concentration (Composite	e)		
Time of Concentration (Composite)	0.153 hours		

Return Event: 100 years

Subsection: Time of Concentration Calculations Return Event: 100 years

Label: PDA-1 Storm Event: 100 Year Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

==== SCS Channel Flow

Tc = R = Qa / Wp

V = (1.49 \* (R\*\*(2/3)) \* (Sf\*\*-0.5)) / n

(Lf / V) / 3600

Where: R= Hydraulic radius

Aq= Flow area, square feet Wp= Wetted perimeter, feet

V= Velocity, ft/sec Sf= Slope, ft/ft n= Manning's n

Tc= Time of concentration, hours

Lf= Flow length, feet

==== SCS TR-55 Shallow Concentration Flow

Tc = Unpaved surface:

V = 16.1345 \* (Sf\*\*0.5)

Paved Surface:

V = 20.3282 \* (Sf\*\*0.5)

(Lf / V) / 3600

Where: V= Velocity, ft/sec

Sf= Slope, ft/ft

Tc= Time of concentration, hours

Lf= Flow length, feet

Subsection: Time of Concentration Calculations

Label: PDA-1B

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

#### Time of Concentration Results

Time of Concentration Results	
Segment #1: TR-55 Sheet Flow	
Hydraulic Length	100.00 ft
Manning's n	0.240
Slope	0.070 ft/ft
2 Year 24 Hour Depth	3.4 in
Average Velocity	0.20 ft/s
Segment Time of Concentration	0.140 hours
Segment #2: TR-55 Shallow Conc	entrated Flow
Hydraulic Length	24.00 ft
Is Paved?	False
Slope	0.042 ft/ft
Average Velocity	3.31 ft/s
Segment Time of Concentration	0.002 hours
Segment #3: TR-55 Channel Flow	
Flow Area	0.2 ft <sup>2</sup>
Hydraulic Length	233.00 ft
Manning's n	0.012
Slope	0.030 ft/ft
Wetted Perimeter	0.79 ft
Average Velocity	8.53 ft/s
Segment Time of Concentration	0.008 hours
Time of Concentration (Composite)	
Time of Concentration (Composite)	0.149 hours

Return Event: 100 years

Subsection: Time of Concentration Calculations Return Event: 100 years

Label: PDA-1B Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

#### ==== SCS Channel Flow

Tc = R = Qa / Wp

V = (1.49 \* (R\*\*(2/3)) \* (Sf\*\*-0.5)) / n

(Lf / V) / 3600

Where: R= Hydraulic radius

Aq= Flow area, square feet Wp= Wetted perimeter, feet

V= Velocity, ft/sec Sf= Slope, ft/ft n= Manning's n

Tc= Time of concentration, hours

Lf= Flow length, feet

#### ==== SCS TR-55 Shallow Concentration Flow

Tc = Unpaved surface:

V = 16.1345 \* (Sf\*\*0.5)

Paved Surface:

V = 20.3282 \* (Sf\*\*0.5)

(Lf / V) / 3600

Where: V= Velocity, ft/sec

Sf= Slope, ft/ft

Tc= Time of concentration, hours

Lf= Flow length, feet

#### ==== SCS TR-55 Sheet Flow

 $Tc = \frac{(0.007 * ((n * Lf)**0.8)) / ((P**0.5) * (Sf**0.4))}{((P**0.5) * (Sf**0.4))}$ 

Where: Tc= Time of concentration, hours

n= Manning's n Lf= Flow length, feet

P= 2yr, 24hr Rain depth, inches

Sf= Slope, %

Subsection: Runoff CN-Area Return Event: 100 years Label: PDA-1 Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Soil/Surface Description	CN	Area (ft²)	C (%)	UC (%)	Adjusted CN
Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil C	74.000	54,360.000	0.0	0.0	74.000
Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil C	98.000	1,529.000	0.0	0.0	98.000
Woods - good - Soil C	70.000	5,034.000	0.0	0.0	70.000
COMPOSITE AREA & WEIGHTED CN>	(N/A)	60,923.000	(N/A)	(N/A)	74.272

Subsection: Runoff CN-Area Return Event: 100 years Label: PDA-1A Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Soil/Surface Description	CN	Area (ft²)	C (%)	UC (%)	Adjusted CN
Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil C	74.000	2,401.000	0.0	0.0	74.000
Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil C	98.000	3,521.000	0.0	0.0	98.000
COMPOSITE AREA & WEIGHTED CN>	(N/A)	5,922.000	(N/A)	(N/A)	88.270

Subsection: Runoff CN-Area Return Event: 100 years
Label: PDA-1B Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Soil/Surface Description	CN	Area (ft²)	C (%)	UC (%)	Adjusted CN
Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil C	74.000	10,987.000	0.0	0.0	74.000
Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil C	98.000	9,908.000	0.0	0.0	98.000
Woods - good - Soil C	70.000	2,080.000	0.0	0.0	70.000
COMPOSITE AREA & WEIGHTED CN>	(N/A)	22,975.000	(N/A)	(N/A)	83.988

Subsection: Unit Hydrograph Summary

Label: PDA-1

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

	<u>,                                      </u>
Storm Event	100 Year
Return Event	100 years
Duration	35.000 hours
Depth	9.1 in
Time of Concentration (Composite)	0.153 hours
Area (User Defined)	60,923.000 ft <sup>2</sup>
Computational Time Increment	0.020 hours
Time to Peak (Computed)	12.133 hours
Flow (Peak, Computed)	7.94 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	12.150 hours
Flow (Peak Interpolated Output)	7.79 ft³/s
Drainage Area	
	74.000
SCS CN (Composite) Area (User Defined)	60,923.000 ft <sup>2</sup>
Maximum Retention (Pervious)	3.5 in
Maximum Retention (Pervious, 20 percent)	0.7 in
(* 6. 116.16)	
Cumulative Runoff	
Cumulative Runoff Depth (Pervious)	5.9 in
Runoff Volume (Pervious)	30,195.545 ft <sup>3</sup>
Hydrograph Volume (Area und	der Hydrograph curve)
Volume	30,194.000 ft <sup>3</sup>
CCC Unit Hydrograph Dozers	toro
SCS Unit Hydrograph Parame	:1615
Time of Concentration (Composite)	0.153 hours
Computational Time Increment	0.020 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Return Event: 100 years

Subsection: Unit Hydrograph Summary

Label: PDA-1

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

SCS Unit Hydrograph Parameters	
Unit peak, qp	10.36 ft <sup>3</sup> /s
Unit peak time, Tp	0.102 hours
Unit receding limb, Tr	0.408 hours
Total unit time, Tb	0.510 hours

Return Event: 100 years

Subsection: Unit Hydrograph Summary

Label: PDA-1A

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Storm Event	100 Year
Return Event	100 years
Duration	35.000 hours
Depth	9.1 in
Time of Concentration (Composite)	0.083 hours
Area (User Defined)	5,922.000 ft <sup>2</sup>
Computational Time Increment	0.011 hours
Time to Peak (Computed)	12.095 hours
Flow (Peak, Computed)	0.99 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	12.100 hours
Flow (Peak Interpolated Output)	0.99 ft³/s
Drainage Area	
SCS CN (Composite)	88.000
Area (User Defined)	5,922.000 ft <sup>2</sup>
Maximum Retention (Pervious)	1.4 in
Maximum Retention (Pervious, 20 percent)	0.3 in
Cumulative Runoff	
Cumulative Runoff Depth (Pervious)	7.7 in
Runoff Volume (Pervious)	3,787.893 ft³
Hydrograph Volume (Area unde	er Hydrograph curve)
Volume	3,788.000 ft <sup>3</sup>
SCS Unit Hydrograph Paramete	ers
Time of Concentration (Composite)	0.083 hours
Computational Time Increment	0.011 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670

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Subsection: Unit Hydrograph Summary

Label: PDA-1A

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

SCS Unit Hydrograph Parameters	3
Unit peak, qp	1.85 ft <sup>3</sup> /s
Unit peak time, Tp	0.056 hours
Unit receding limb, Tr	0.222 hours
Total unit time, Tb	0.278 hours

Return Event: 100 years

Subsection: Unit Hydrograph Summary

Label: PDA-1B

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

	7
Storm Event	100 Year
Return Event	100 years
Duration	35.000 hours
Depth	9.1 in
Time of Concentration (Composite)	0.149 hours
Area (User Defined)	22,975.000 ft <sup>2</sup>
Computational Time Increment	0.020 hours
Time to Peak (Computed)	12.131 hours
Flow (Peak, Computed)	3.49 ft <sup>3</sup> /s
Output Increment	0.050 hours
Time to Flow (Peak Interpolated Output)	12.100 hours
Flow (Peak Interpolated Output)	3.45 ft³/s
Drainage Area	
SCS CN (Composite)	84.000
Area (User Defined)	22,975.000 ft <sup>2</sup>
Maximum Retention (Pervious)	1.9 in
Maximum Retention (Pervious, 20 percent)	0.4 in
Cumulative Runoff	
Cumulative Runoff Depth (Pervious)	7.2 in
Runoff Volume (Pervious)	13,755.961 ft³
Hydrograph Volume (Area und	ler Hydrograph curve)
Volume	13,756.000 ft <sup>3</sup>
SCS Unit Hydrograph Parame	ters
Time of Concentration (Composite)	0.149 hours
Computational Time Increment	0.020 hours
Unit Hydrograph Shape Factor	483.432
K Factor	0.749
Receding/Rising, Tr/Tp	1.670
3, 3, 1 F	-

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Subsection: Unit Hydrograph Summary

Label: PDA-1B

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

SCS Unit Hydrograph Parameters					
Unit peak, qp	4.00 ft <sup>3</sup> /s				
Unit peak time, Tp	0.100 hours				
Unit receding limb, Tr	0.398 hours				
Total unit time, Tb	0.498 hours				

Return Event: 100 years

Subsection: Time vs. Elevation Return Event: 100 years Label: PO-2 (IN) Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Elevation (ft)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
0.000	579.50	579.50	579.50	579.50	579.50
0.250	579.50	579.50	579.50	579.50	579.50
0.500	579.50	579.50	579.50	579.50	579.50
0.750	579.50	579.50	579.50	579.50	579.50
1.000	579.50	579.50	579.50	579.50	579.50
1.250	579.50	579.50	579.50	579.50	579.50
1.500	579.50	579.50	579.50	579.50	579.50
1.750	579.50	579.50	579.50	579.50	579.50
2.000	579.50	579.50	579.50	579.50	579.50
2.250	579.50	579.50	579.50	579.50	579.50
2.500	579.50	579.50	579.50	579.50	579.50
2.750	579.50	579.50	579.50	579.50	579.50
3.000	579.50	579.50	579.50	579.50	579.50
3.250	579.50	579.50	579.50	579.50	579.50
3.500	579.50	579.50	579.50	579.50	579.50
3.750	579.50	579.50	579.50	579.50	579.50
4.000	579.50	579.50	579.50	579.50	579.50
4.250	579.50	579.50	579.50	579.50	579.50
4.500	579.51	579.51	579.51	579.51	579.51
4.750	579.51	579.51	579.51	579.51	579.51
5.000	579.51	579.51	579.51	579.51	579.51
5.250	579.51	579.51	579.51	579.51	579.51
5.500	579.51	579.52	579.52	579.52	579.52
5.750	579.52	579.52	579.52	579.52	579.52
6.000	579.52	579.52	579.52	579.52	579.52
6.250	579.52	579.52	579.52	579.53	579.53
6.500	579.53	579.53	579.53	579.53	579.53
6.750	579.53	579.53	579.53	579.53	579.54
7.000	579.54	579.54	579.54	579.54	579.54
7.250	579.54	579.54	579.54	579.54	579.55
7.500	579.55	579.55	579.55	579.55	579.55
7.750	579.55	579.55	579.56	579.56	579.56
8.000	579.56	579.56	579.56	579.56	579.56
8.250	579.57	579.57	579.57	579.57	579.57
8.500 8.750	579.58 579.59	579.58 579.59	579.58 579.59	579.58 579.60	579.59 579.60
9.000	579.59 579.60	579.59 579.60	579.59 579.61	579.60 579.61	579.60 579.61
				579.61 579.62	579.61 579.63
9.250 9.500	579.61 579.63	579.62 579.63	579.62 579.63	579.62 579.64	5/9.63 579.64
9.500	579.63 579.64	579.63 579.65	579.63 579.65	579.64 579.65	579.64 579.66
9.750	5/9.64	5/9.65	5/9.65	5/9.05	5/9.66

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Subsection: Time vs. Elevation Return Event: 100 years Label: PO-2 (IN) Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Elevation (ft)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
10.000	579.66	579.66	579.66	579.67	579.67
10.250	579.68	579.68	579.69	579.69	579.70
10.500	579.70	579.71	579.72	579.72	579.73
10.750	579.73	579.74	579.74	579.75	579.76
11.000	579.76	579.77	579.78	579.79	579.80
11.250	579.81	579.83	579.85	579.87	579.89
11.500	579.91	579.94	579.98	580.06	580.21
11.750	580.46	580.65	580.88	581.16	581.55
12.000	582.16	582.93	583.56	583.83	583.78
12.250	583.54	583.28	583.07	582.92	582.81
12.500	582.71	582.63	582.55	582.49	582.45
12.750	582.40	582.36	582.32	582.28	582.24
13.000	582.21	582.17	582.13	582.09	582.04
13.250	581.99	581.94	581.90	581.84	581.79
13.500	581.74	581.68	581.63	581.57	581.51
13.750	581.45	581.39	581.33	581.26	581.20
14.000	581.13	581.06	580.99	580.93	580.86
14.250	580.79	580.72	580.65	580.57	580.50
14.500	580.36	580.21	580.06	579.93	579.84
14.750	579.78	579.75	579.73	579.72	579.71
15.000	579.70	579.70	579.69	579.69	579.69
15.250	579.68	579.68	579.68	579.67	579.67
15.500	579.67	579.67	579.66	579.66	579.66
15.750	579.65	579.65	579.65	579.65	579.64
16.000	579.64	579.64	579.64	579.63	579.63
16.250	579.63	579.63	579.63	579.62	579.62
16.500	579.62	579.62	579.62	579.62	579.62
16.750	579.62	579.61	579.61	579.61	579.61
17.000	579.61	579.61	579.61	579.61	579.60
17.250	579.60	579.60	579.60	579.60	579.60
17.500	579.60	579.60	579.59	579.59	579.59
17.750	579.59	579.59	579.59	579.59	579.59
18.000	579.58	579.58	579.58	579.58	579.58
18.250	579.58	579.58	579.58	579.58	579.58
18.500	579.58	579.58	579.58	579.58	579.58
18.750	579.58	579.58	579.57	579.57	579.57
19.000	579.57	579.57	579.57	579.57	579.57
19.250	579.57	579.57	579.57	579.57	579.57
19.500	579.57	579.57	579.57	579.57	579.57
19.750	579.57	579.57	579.57	579.57	579.57
20.000	579.57	579.57	579.57	579.57	579.56

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Subsection: Time vs. Elevation Return Event: 100 years Label: PO-2 (IN) Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Elevation (ft)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
20.250	579.56	579.56	579.56	579.56	579.56
20.500	579.56	579.56	579.56	579.56	579.56
20.750	579.56	579.56	579.56	579.56	579.56
21.000	579.56	579.56	579.56	579.56	579.56
21.250	579.56	579.56	579.56	579.56	579.56
21.500	579.56	579.56	579.56	579.56	579.56
21.750	579.56	579.56	579.56	579.56	579.56
22.000	579.55	579.55	579.55	579.55	579.55
22.250	579.55	579.55	579.55	579.55	579.55
22.500	579.55	579.55	579.55	579.55	579.55
22.750	579.55	579.55	579.55	579.55	579.55
23.000	579.55	579.55	579.55	579.55	579.55
23.250	579.55	579.55	579.55	579.55	579.55
23.500	579.55	579.55	579.55	579.55	579.55
23.750	579.54	579.54	579.54	579.54	579.54
24.000	579.54	579.54	579.54	579.53	579.52
24.250	579.51	579.51	579.50	579.50	579.50
24.500	579.50	579.50	579.50	579.50	579.50
24.750	579.50	579.50	579.50	579.50	579.50
25.000	579.50	579.50	579.50	579.50	579.50
25.250	579.50	579.50	579.50	579.50	579.50
25.500	579.50	579.50	579.50	579.50	579.50
25.750	579.50	579.50	579.50	579.50	579.50
26.000	579.50	579.50	579.50	579.50	579.50
26.250	579.50	579.50	579.50	579.50	579.50
26.500	579.50	579.50	579.50	579.50	579.50
26.750	579.50	579.50	579.50	579.50	579.50
27.000	579.50	579.50	579.50	579.50	579.50
27.250	579.50	579.50	579.50	579.50	579.50
27.500	579.50	579.50	579.50	579.50	579.50
27.750	579.50	579.50	579.50	579.50	579.50
28.000	579.50	579.50	579.50	579.50	579.50
28.250	579.50	579.50	579.50	579.50	579.50
28.500	579.50	579.50	579.50	579.50	579.50
28.750	579.50	579.50	579.50	579.50	579.50
29.000	579.50	579.50	579.50	579.50	579.50
29.250	579.50	579.50	579.50	579.50	579.50
29.500	579.50	579.50	579.50	579.50	579.50
29.750	579.50	579.50	579.50	579.50	579.50
30.000	579.50	579.50	579.50	579.50	579.50
30.250	579.50	579.50	579.50	579.50	579.50

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Subsection: Time vs. Elevation Return Event: 100 years Label: PO-2 (IN) Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Elevation (ft)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)	Elevation (ft)
30.500	579.50	579.50	579.50	579.50	579.50
30.750	579.50	579.50	579.50	579.50	579.50
31.000	579.50	579.50	579.50	579.50	579.50
31.250	579.50	579.50	579.50	579.50	579.50
31.500	579.50	579.50	579.50	579.50	579.50
31.750	579.50	579.50	579.50	579.50	579.50
32.000	579.50	579.50	579.50	579.50	579.50
32.250	579.50	579.50	579.50	579.50	579.50
32.500	579.50	579.50	579.50	579.50	579.50
32.750	579.50	579.50	579.50	579.50	579.50
33.000	579.50	579.50	579.50	579.50	579.50
33.250	579.50	579.50	579.50	579.50	579.50
33.500	579.50	579.50	579.50	579.50	579.50
33.750	579.50	579.50	579.50	579.50	579.50
34.000	579.50	579.50	579.50	579.50	579.50
34.250	579.50	579.50	579.50	579.50	579.50
34.500	579.50	579.50	579.50	579.50	579.50
34.750	579.50	579.50	579.50	579.50	579.50
35.000	579.50	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Time vs. Volume Return Event: 100 years Label: PO-2 Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Volume (ft³)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Volume (ft³)	Volume (ft³)	Volume (ft³)	Volume (ft³)	Volume (ft³)
0.000	0.000	0.000	0.000	0.000	0.000
0.250	0.000	0.000	0.000	0.000	0.000
0.500	0.000	0.000	0.000	0.000	0.000
0.750	0.000	0.000	0.000	0.000	0.000
1.000	0.000	0.000	0.000	0.000	0.000
1.250	0.000	0.000	0.000	0.000	0.000
1.500	0.000	0.000	0.000	0.000	0.000
1.750	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.000	0.000	0.000	0.000
2.250	0.000	0.000	0.000	0.000	0.000
2.500	0.000	0.000	0.000	0.000	0.000
2.750	0.000	0.000	0.000	0.000	0.000
3.000	0.000	0.000	0.000	0.000	0.000
3.250	0.000	0.000	0.000	0.000	0.000
3.500	0.000	0.000	0.000	0.000	0.000
3.750	1.000	1.000	1.000	1.000	1.000
4.000	1.000	1.000	1.000	1.000	1.000
4.250	1.000	2.000	2.000	2.000	2.000
4.500	2.000	2.000	3.000	3.000	3.000
4.750	3.000	3.000	4.000	4.000	4.000
5.000	4.000	4.000	5.000	5.000	5.000
5.250	5.000	5.000	6.000	6.000	6.000
5.500	6.000	6.000	7.000	7.000	7.000
5.750	7.000	7.000	8.000	8.000	8.000
6.000	8.000	8.000	9.000	9.000	9.000
6.250	9.000	10.000	10.000	10.000	11.000
6.500	11.000	11.000	12.000	12.000	13.000
6.750	13.000	13.000	14.000	14.000	14.000
7.000	15.000	15.000	16.000	16.000	17.000
7.250 7.500	17.000 19.000	17.000 20.000	18.000	18.000	19.000 21.000
7.750	22.000	22.000	20.000 23.000	21.000 23.000	24.000
8.000	24.000	25.000	25.000	26.000	26.000
8.250	27.000	28.000	29.000	30.000	31.000
8.500	32.000	33.000	33.000	34.000	35.000
8.750	36.000	37.000	38.000	39.000	41.000
9.000	42.000	43.000	44.000	45.000	46.000
9.250	47.000	48.000	49.000	50.000	52.000
9.500	53.000	54.000	55.000	56.000	58.000
9.750	59.000	60.000	61.000	63.000	64.000
1 5.750	] 55.000	00.000	01.000	05.000	01.000

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Subsection: Time vs. Volume

Return Event: 100 years

Label: PO-2

Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Volume (ft³)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Volume (ft³)	Volume (ft³)	Volume (ft³)	Volume (ft³)	Volume (ft³)
10.000	65.000	66.000	68.000	69.000	71.000
10.250	73.000	75.000	77.000	79.000	81.000
10.500	84.000	86.000	88.000	91.000	93.000
10.750	96.000	98.000	100.000	103.000	105.000
11.000	108.000	111.000	114.000	118.000	123.000
11.250	129.000	136.000	144.000	152.000	160.000
11.500	169.000	180.000	198.000	231.000	293.000
11.750	393.000	534.000	718.000	946.000	1,247.000
12.000	1,680.000	2,119.000	2,386.000	2,495.000	2,477.000
12.250	2,379.000	2,272.000	2,185.000	2,117.000	2,061.000
12.500	2,012.000	1,968.000	1,931.000	1,901.000	1,872.000
12.750	1,842.000	1,813.000	1,786.000	1,760.000	1,736.000
13.000	1,714.000	1,691.000	1,665.000	1,636.000	1,604.000
13.250	1,571.000	1,537.000	1,501.000	1,464.000	1,425.000
13.500	1,386.000	1,345.000	1,303.000	1,259.000	1,215.000
13.750	1,169.000	1,122.000	1,074.000	1,024.000	973.000
14.000	921.000	868.000	814.000	758.000	702.000
14.250	646.000	588.000	530.000	472.000	413.000
14.500	353.000	293.000	232.000	177.000	140.000
14.750	117.000	103.000	95.000	89.000	86.000
15.000	83.000	81.000	79.000	78.000	76.000
15.250	75.000	74.000	73.000	72.000	70.000
15.500	69.000	68.000	67.000	66.000	65.000
15.750	63.000	62.000	61.000	60.000	59.000
16.000	58.000	57.000	55.000	54.000	54.000
16.250	53.000	52.000	52.000	51.000	50.000
16.500	50.000	49.000	49.000	48.000	48.000
16.750	47.000	47.000	46.000	46.000	45.000
17.000	45.000	44.000	44.000	43.000	43.000
17.250	42.000	42.000	41.000	41.000	40.000
17.500	40.000	39.000	39.000	38.000	38.000
17.750	37.000	37.000	36.000	36.000	35.000
18.000	35.000	34.000	34.000	33.000	33.000
18.250	33.000	32.000	32.000	32.000	32.000
18.500	32.000	32.000	31.000	31.000	31.000
18.750	31.000	31.000	31.000	31.000	30.000
19.000	30.000	30.000	30.000	30.000	30.000
19.250	29.000	29.000	29.000	29.000	29.000
19.500	29.000	29.000	28.000	28.000	28.000
19.750	28.000	28.000	28.000	28.000	27.000
20.000	27.000	27.000	27.000	27.000	27.000
·	·	Bentley Sy	stems. Inc. Haestad	Methods Solution	ŗ

Bentley Systems, Inc. Haestad Methods Solution Center

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Subsection: Time vs. Volume

Return Event: 100 years

Label: PO-2

Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Volume (ft³)

# Output Time increment = 0.050 hours Time on left represents time for first value in each row.

20.250 20.500	(ft³) 27.000 26.000 25.000	(ft³) 26.000 26.000	(ft³) 26.000	(ft³) 26.000	(ft³) 26.000
20.500		26,000		20.000	26.000
	25 000	20.000	26.000	26.000	25.000
20.750	23.000	25.000	25.000	25.000	25.000
21.000	25.000	25.000	25.000	24.000	24.000
21.250	24.000	24.000	24.000	24.000	24.000
21.500	24.000	23.000	23.000	23.000	23.000
21.750	23.000	23.000	23.000	23.000	23.000
22.000	22.000	22.000	22.000	22.000	22.000
22.250	22.000	22.000	22.000	22.000	21.000
22.500	21.000	21.000	21.000	21.000	21.000
22.750	21.000	21.000	21.000	20.000	20.000
23.000	20.000	20.000	20.000	20.000	20.000
23.250	20.000	19.000	19.000	19.000	19.000
23.500	19.000	19.000	19.000	19.000	19.000
23.750	18.000	18.000	18.000	18.000	18.000
24.000	18.000	17.000	15.000	11.000	8.000
24.250	5.000	3.000	2.000	1.000	1.000
24.500	0.000	0.000	0.000	0.000	0.000
24.750	0.000	0.000	0.000	0.000	0.000
25.000	0.000	0.000	0.000	0.000	0.000
25.250	0.000	0.000	0.000	0.000	0.000
25.500	0.000	0.000	0.000	0.000	0.000
25.750	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.000	0.000	0.000	0.000
26.250	0.000	0.000	0.000	0.000	0.000
26.500	0.000	0.000	0.000	0.000	0.000
26.750	0.000	0.000	0.000	0.000	0.000
27.000	0.000	0.000	0.000	0.000	0.000
27.250	0.000	0.000	0.000	0.000	0.000
27.500	0.000	0.000	0.000	0.000	0.000
27.750	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.000	0.000	0.000	0.000
28.250	0.000	0.000	0.000	0.000	0.000
28.500	0.000	0.000	0.000	0.000	0.000
28.750	0.000	0.000	0.000	0.000	0.000
29.000	0.000	0.000	0.000	0.000	0.000
29.250	0.000	0.000	0.000	0.000	0.000
29.500	0.000	0.000	0.000	0.000	0.000
29.750	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.000	0.000	0.000	0.000
30.250	0.000	0.000	0.000	0.000	0.000

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27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 PondPack CONNECT Edition [10.02.00.01] Page 23 of 28

Subsection: Time vs. Volume Return Event: 100 years Label: PO-2 Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Time vs. Volume (ft³)

#### Output Time increment = 0.050 hours Time on left represents time for first value in each row.

Time (hours)	Volume (ft³)	Volume (ft³)	Volume (ft³)	Volume (ft³)	Volume (ft³)
30.500	0.000	0.000	0.000	0.000	0.000
30.750	0.000	0.000	0.000	0.000	0.000
31.000	0.000	0.000	0.000	0.000	0.000
31.250	0.000	0.000	0.000	0.000	0.000
31.500	0.000	0.000	0.000	0.000	0.000
31.750	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.000	0.000	0.000	0.000
32.250	0.000	0.000	0.000	0.000	0.000
32.500	0.000	0.000	0.000	0.000	0.000
32.750	0.000	0.000	0.000	0.000	0.000
33.000	0.000	0.000	0.000	0.000	0.000
33.250	0.000	0.000	0.000	0.000	0.000
33.500	0.000	0.000	0.000	0.000	0.000
33.750	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.000	0.000	0.000	0.000
34.250	0.000	0.000	0.000	0.000	0.000
34.500	0.000	0.000	0.000	0.000	0.000
34.750	0.000	0.000	0.000	0.000	0.000
35.000	0.000	(N/A)	(N/A)	(N/A)	(N/A)

Subsection: Storage Chamber System

Return Event: 100 years Label: PO-2 Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Storage Chamber	_	_	
ID	130	Notes	Created on 02/10/2010. Please check with the manufacturer for the latest data.
Label	SC-740 Chamber		
Storage Chamber			
Effective Length	7.12 ft	Manufacturer	StormTech
Section Length Varies?	False	Default Spacing	0.50 ft

# **Depth-Incremental Volume Per Unit Length** Curve

Depth (ft)	Incremental Volume Per Unit Length (ft³/ft)
0.08	0.31
0.17	0.31
0.25	0.31
0.33	0.30
0.42	0.30
0.50	0.30
0.58	0.29
0.67	0.29
0.75	0.28
0.83	0.28
0.92	0.27
1.00	0.27
1.08	0.26
1.17	0.25
1.25	0.25
1.33	0.24
1.42	0.23
1.50	0.22
1.58	0.21
1.67	0.20
1.75	0.19
1.83	0.18
1.92	0.17
2.00	0.15
2.08	0.13
2.17	0.11
2.25	0.09

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Subsection: Storage Chamber System

Label: PO-2

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

Depth-Incremental Volume Per Unit Length
Curve

Depth (ft)	Incremental Volume Per Unit Length (ft³/ft)
2.33	0.04
2.42	0.02
2.50	0.01

Storage Chamber			
Storage Chamber Type	Incremental Volume Per Unit Length	Maximum Width	4.2
Storage Chamber (Pond)			
Chamber System Invert	579.50 ft		
Chamber System Rows	13		
Chambers per Row	2		
Chamber System Fill Void Space	40.0 %		
Chamber System Row Spacing	6.0 in		
Chamber System Side Fill	12.0 in		
Chamber System Fill Cover Depth	12.0 in		
Chamber System Fill Base Depth	12.0 in		
Chamber System Fill Side Slope	0.000 H:V		
Chamber System End Fill	12.0 in		
Chamber System Includes Header?	False		

Subsection: Composite Rating Curve

Label: OCS

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Composite Outflow Summary

Water Surface Elevation (ft)	Flow (ft³/s)	Tailwater Elevation (ft)	Convergence Error (ft)
579.50	0.00	(N/A)	0.00
580.00	0.00	(N/A)	0.00
580.50	0.00	(N/A)	0.00
581.00	0.00	(N/A)	0.00

Return Event: 100 years

Storm Event: 100 Year

Return Event: 100 years

Storm Event: 100 Year

Subsection: Composite Rating Curve

Return Event: 100 years Label: OCS Storm Event: 100 Year

Scenario: 4 Tripp Street - Synthetic Curve, 100 yrs

# Composite Outflow Summary

Water Surface Elevation (ft)	Flow (ft³/s)	Tailwater Elevation (ft)	Convergence Error (ft)
581.50	0.00	(N/A)	0.00
581.75	0.00	(N/A)	0.00
582.00	0.00	(N/A)	0.00
582.20	0.00	(N/A)	0.00
582.50	0.29	(N/A)	0.00
583.00	1.73	(N/A)	0.00
583.50	2.76	(N/A)	0.00
584.00	3.72	(N/A)	0.00

# Contributing Structures

(no Q: Orifice - 1,Weir -
1,C0)
(no Q: Orifice - 1,Weir -
1,C0)
(no O: Orifice - 1.Weir -

1,C0) (no Q: Orifice - 1, Weir -1,C0)

(no Q: Orifice - 1, Weir -1,C0)

(no Q: Orifice - 1, Weir -1,C0)

(no Q: Orifice - 1,Weir -

1,C0) (no Q: Orifice - 1,Weir -

1,C0)

Orifice - 1,C0 (no Q: Weir - 1)

Orifice - 1,C0 (no Q:

Weir - 1)

Orifice - 1,C0 (no Q:

Weir - 1)

Orifice - 1,Weir - 1,C0

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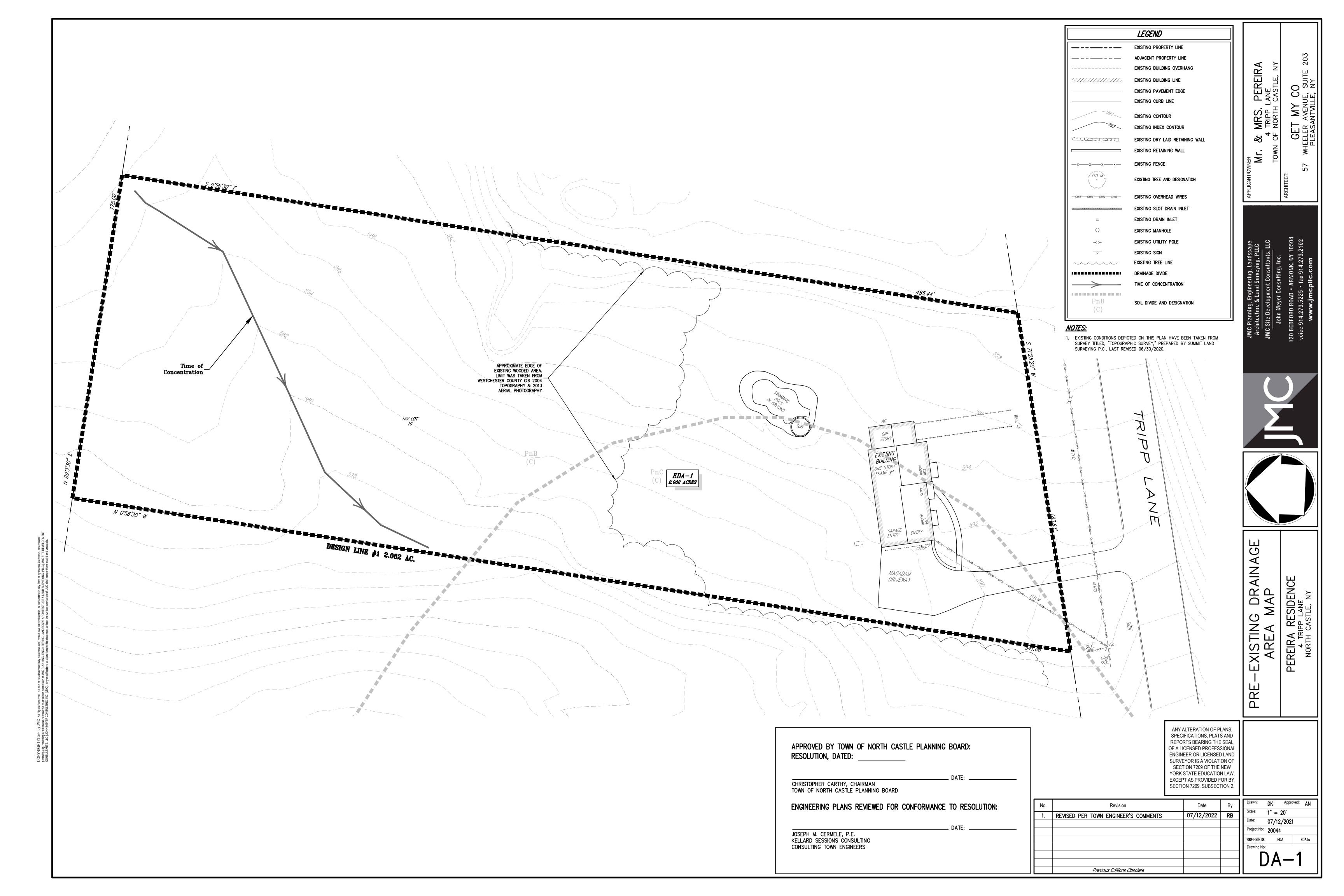
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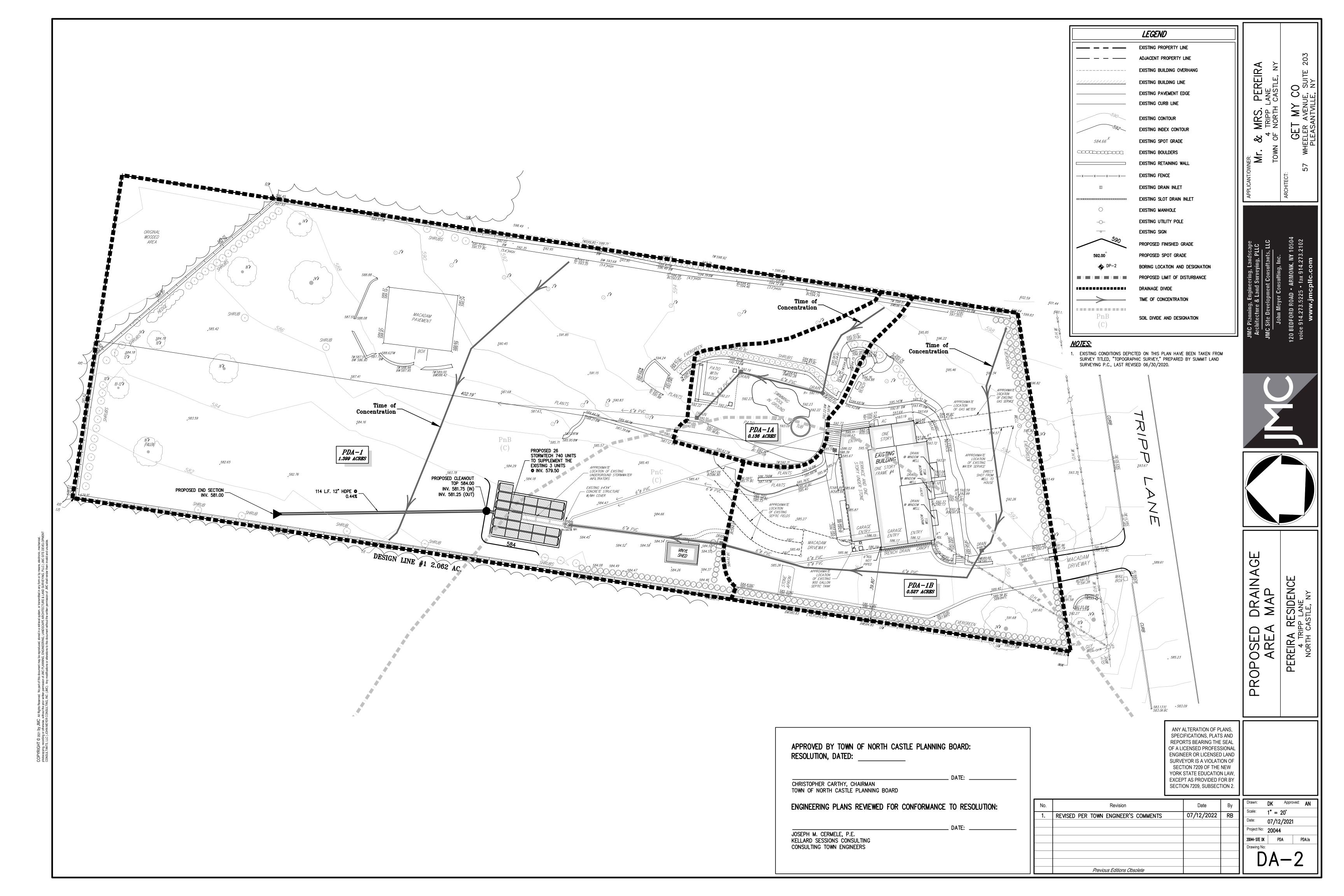
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# APPENDIX C DRAWINGS





# **APPENDIX D**

# STORMTECH MODEL SC-740 DETENTION SYSTEM DESIGN SHEETS

STORM\_TECH RECHARGER SC 740

THE VOLUMES ACCOUNT FOR VOID SPACE IN THE 6" STONE BASE AND SURROUNDING STONE ADDITIONAL STONE IS CALCULATED AT 40% VOID SPACE

SPACE
NOID
- 40%
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STONE
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												DIM.	f.t.		2.50
														s.f.	
														AREA/UNIT	HEIGHT
			90	52	41	16	99	17	19	35	23	36	31	9,	00
STORAGE	W/STONE	cf/unit	74.9	71.52	. '89	64.7	29.6	54.	48.	41.8	35.2	28.3	21.3	6.7	0.0
TORAGE	PLAIN	cf/ft													
S	IGE	f.t.	3.50	3.25	3.00	2.75	2.50	2.25	2.00	1.75	1.50	1.25	1.00	0.50	0
	EIGHT STAGE		3.00	2.75	2.50	2.25	2.00	1.75	1.50	1.25	1.00	0.75	0.50	0	RAVEL
	Ξ	#													0
															TONE
			VER	STONE COVER	Crown									nvert	ROKEN S
			TONE CO	TONE CO	ormTech	B MOTTC									
			w.	w.	S	S	S	S	S	S	S	S	S	S	ă

LAY-UP f.t. 33.82 3.50

		SUIDANCE	M-quantity	Volume	Storage +		nfiltration	cţ		3,682	5,522	7,363	9,204	11,045	12,886	14,726	16,567	18,408	20,249	22,090	23,930	25,771	27,612	29,453	31,294
	ļ	O	>		infiltrate Storage +		in 12 hrs Infiltration	cf		3,382	5,073	6,764	8,455	10,146	11,837	13,528	15,219	16,910	18,601	20,292	21,983	23,674	25,365	27,056	28,747
7.12	4.75						AREA*UNIT		33.82	135.28	202.92	270.56	338.20	405.84	473.48	541.12	92.809	676.40	744.04	811.68	879.32	946.96	1,014.60	1,082.24	1,149.88
7.56	4.25				NSTANT			cfs	0.020	0.078	0.117	0.157	0.196	0.235	0.274	0.313	0.352	0.391	0.431	0.470	0.509	0.548	0.587	0.626	0.665
					STAGE CONSTANT	42	3.50 FLOW RATE	583.00	74.90	300	449	299	749	899	1,049	1,198	1,348	1,498	1,648	1,798	1,947	2,097	2,247	2,397	2,547
LENGTH	Ē			GRAVEI	STAGE	39	3.25	582.75	71.52	286	429	572	715	828	1,001	1,144	1,287	1,430	1,573	1,716	1,860	2,003	2,146	2,289	2,432
LEN	WIDE				STAGE	36	3.00	582.50	68.14	273	409	545	681	818	954	1,090	1,227	1,363	1,499	1,635	1,772	1,908	2,044	2,180	2,317
		GUIDANCE	WQ volume		STAGE	33	2.75	582.25	64.5	258	387	516	645	774	902	1,031	1,160	1,289	1,418	1,547	1,676	1,805	1,934	2,063	2,192
		INS	WQ		STAGE	30	2.50	582.00	99.69	239	358	477	265	716	835	955	1,074	1,193	1,313	1,432	1,551	1,670	1,790	1,909	2,028
				SC 740	STAGE	27	2.25	581.75	54.17	217	325	433	542	650	758	867	975	1,083	1,192	1,300	1,408	1,517	1,625	1,733	1,842
ınit	CUMMULATIVE			ECHARGER	STAGE	24	2.00	581.50	48.19	193	289	386	482	578	675	771	867	964	1,060	1,157	1,253	1,349	1,446	1,542	1,638
.0195718 cfs/unit	CUM		iE (cf.)	ORM-TECH RECHARGER SC 740	STAGE	21	1.75	581.25	41.85	167	251	335	419	502	586	670	753	837	921	1,004	1,088	1,172	1,256	1,339	1,423
0			EACH STAG	STO	STAGE	18	1.50	581.00	35.23	141	211	282	352	423	493	564	634	202	775	846	916	986	1,057	1,127	1,198
25.00 in/hr	579.50		VOLUME OF STORAGE IN EACH STAGE (cf.)		STAGE	15	1.25	580.75	28.36	113	170	227	284	340	397	454	510	295	624	681	737	794	851	806	964
	NE		-UME OF ST		STAGE	12	1.00	580.50	21.31	85	128	170	213	256	298	341	384	426	469	511	554	265	639	682	725
	TTOM STOI		NOI		STAGE	9	0.50	580.00	92.9	27	4	25	89	81	92	108	122	135	149	162	176	189	203	216	230
INFILTRATION	<b>ELEVATION BOTTOM STONE</b>			GRAVEL	STAGE	0	0.00	579.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ŗ	ELE			2	2	inch	LINO ON	ELEV.	~	4	9	∞	10	12	4	16	18	20	22	24	26	28	30	32	8

# APPENDIX E WEB SOIL SURVEY INFORMATION



# MAP INFORMATION MAP LEGEND

Not rated or not available Streams and Canals Interstate Highways Local Roads Major Roads US Routes Rails C/D Water Features **Transportation** ŧ Not rated or not available Area of Interest (AOI) Soil Rating Polygons Area of Interest (AOI) C/D

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of Warning: Soil Map may not be valid at this scale. 1:12,000.

The soil surveys that comprise your AOI were mapped at

Please rely on the bar scale on each map sheet for map measurements.

scale.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Westchester County, New York

Survey Area Data: Version 16, Jun 11, 2020

Soil map units are labeled (as space allows) for map scales

1:50,000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Oct

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

ΑD

B/D

# **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
Се	Catden muck, 0 to 2 percent slopes	B/D	31.4	19.5%
CrC	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	В	18.4	11.5%
CsD	Chatfield-Charlton complex, 15 to 35 percent slopes, very rocky	В	0.5	0.3%
CtC	Chatfield-Hollis-Rock outcrop complex, 0 to 15 percent slopes	В	6.1	3.8%
LcB	Leicester loam, 3 to 8 percent slopes, stony	A/D	4.1	2.6%
NcA	Natchaug muck, 0 to 2 percent slopes	B/D	5.4	3.3%
PnB	Paxton fine sandy loam, 3 to 8 percent slopes	С	47.6	29.6%
PnC	Paxton fine sandy loam, 8 to 15 percent slopes	С	6.6	4.1%
RdB	Ridgebury complex, 3 to 8 percent slopes	D	5.3	3.3%
Ub	Udorthents, smoothed	В	28.8	17.9%
W	Water		0.2	0.1%
WdB	Woodbridge loam, 3 to 8 percent slopes	C/D	6.4	4.0%
Totals for Area of Inter	rest	•	160.8	100.0%

# **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

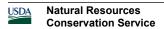
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

# **Rating Options**

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



# **Extreme Precipitation Tables**

# **Northeast Regional Climate Center**

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing Yes

State New York

Location

**Longitude** 73.687 degrees West **Latitude** 41.135 degrees North

Elevation 0 feet

**Date/Time** Mon, 12 Jul 2021 07:14:58 -0400

# **Extreme Precipitation Estimates**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.34	0.52	0.64	0.84	1.05	1.31	1yr	0.91	1.23	1.50	1.85	2.28	2.81	3.18	1yr	2.49	3.06	3.55	4.26	4.91	1yr
2yr	0.40	0.62	0.77	1.02	1.28	1.60	2yr	1.10	1.49	1.84	2.27	2.79	3.43	3.86	2yr	3.03	3.71	4.26	5.05	5.72	2yr
5yr	0.47	0.73	0.92	1.23	1.58	1.99	5yr	1.36	1.83	2.30	2.85	3.51	4.31	4.88	5yr	3.81	4.69	5.44	6.33	7.10	5yr
10yr	0.53	0.83	1.05	1.42	1.85	2.36	10yr	1.60	2.15	2.73	3.40	4.18	5.12	5.84	10yr	4.53	5.61	6.55	7.52	8.36	10yr
25yr	0.61	0.97	1.24	1.72	2.29	2.95	25yr	1.97	2.66	3.43	4.28	5.28	6.44	7.40	25yr	5.70	7.12	8.38	9.43	10.38	25yr
50yr	0.69	1.11	1.43	2.00	2.69	3.50	50yr	2.32	3.12	4.08	5.10	6.28	7.67	8.86	50yr	6.78	8.52	10.09	11.21	12.24	50yr
100yr	0.79	1.27	1.64	2.33	3.17	4.15	100yr	2.74	3.67	4.86	6.08	7.50	9.13	10.61	100yr	8.08	10.21	12.17	13.32	14.43	100yr
200yr	0.89	1.46	1.89	2.71	3.74	4.93	200yr	3.23	4.32	5.78	7.26	8.94	10.89	12.72	200yr	9.64	12.23	14.68	15.83	17.02	200yr
500yr	1.07	1.76	2.29	3.33	4.66	6.19	500yr	4.02	5.35	7.28	9.16	11.30	13.75	16.17	500yr	12.17	15.55	18.81	19.89	21.18	500yr

# **Lower Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.48	0.65	0.80	0.96	1yr	0.69	0.94	1.29	1.60	2.00	2.58	2.74	1yr	2.28	2.64	3.20	3.72	4.24	1yr
2yr	0.39	0.61	0.75	1.01	1.24	1.49	2yr	1.07	1.45	1.70	2.17	2.74	3.32	3.74	2yr	2.94	3.60	4.13	4.89	5.56	2yr
5yr	0.43	0.66	0.82	1.13	1.44	1.74	5yr	1.24	1.70	1.97	2.57	3.21	3.96	4.51	5yr	3.51	4.34	5.01	5.82	6.58	5yr
10yr	0.47	0.72	0.89	1.24	1.60	1.96	10yr	1.38	1.92	2.22	2.93	3.64	4.53	5.20	10yr	4.01	5.00	5.79	6.57	7.47	10yr
25yr	0.50	0.77	0.95	1.36	1.79	2.28	25yr	1.55	2.23	2.57	3.46	4.29	5.39	6.28	25yr	4.77	6.04	7.01	7.69	8.81	25yr
50yr	0.53	0.80	1.00	1.44	1.93	2.55	50yr	1.67	2.49	2.89	3.94	4.87	6.15	7.25	50yr	5.44	6.97	8.09	8.59	9.98	50yr
100yr	0.56	0.84	1.06	1.53	2.09	2.83	100yr	1.81	2.77	3.25	4.50	5.48	7.02	8.38	100yr	6.21	8.06	9.34	9.63	11.31	100yr
200yr	0.59	0.89	1.13	1.63	2.27	3.16	200yr	1.96	3.09	3.66	5.14	6.23	7.99	9.68	200yr	7.07	9.31	10.80	10.70	12.82	200yr
500yr	0.63	0.94	1.20	1.75	2.49	3.66	500yr	2.15	3.58	4.29	6.19	7.39	9.51	11.71	500yr	8.41	11.26	13.06	12.27	15.11	500yr

# **Upper Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.37	0.57	0.70	0.94	1.16	1.40	1yr	1.00	1.37	1.59	2.08	2.61	3.04	3.45	1yr	2.69	3.32	3.83	4.61	5.31	1yr
2yr	0.43	0.66	0.82	1.10	1.36	1.58	2yr	1.18	1.55	1.81	2.31	2.89	3.55	3.99	2yr	3.14	3.84	4.42	5.30	5.93	2yr
5yr	0.51	0.79	0.98	1.35	1.72	2.02	5yr	1.48	1.97	2.32	2.97	3.71	4.66	5.27	5yr	4.12	5.07	5.88	6.84	7.64	5yr
10yr	0.61	0.94	1.16	1.62	2.09	2.43	10yr	1.81	2.37	2.82	3.59	4.51	5.74	6.51	10yr	5.08	6.26	7.30	8.40	9.29	10yr
25yr	0.77	1.18	1.46	2.09	2.75	3.13	25yr	2.37	3.06	3.65	4.63	5.80	7.56	8.62	25yr	6.69	8.29	9.75	11.05	12.02	25yr
50yr	0.92	1.40	1.74	2.51	3.37	3.80	50yr	2.91	3.72	4.45	5.61	7.04	9.33	10.66	50yr	8.26	10.25	12.14	13.60	14.61	50yr
100yr	1.11	1.68	2.10	3.03	4.16	4.63	100yr	3.59	4.52	5.42	6.81	8.69	11.53	13.20	100yr	10.21	12.69	15.14	16.77	17.78	100yr
200yr	1.33	2.01	2.55	3.68	5.14	5.62	200yr	4.43	5.50	6.61	8.24	10.57	14.26	16.34	200yr	12.62	15.71	18.88	20.67	21.65	200yr
500yr	1.73	2.57	3.31	4.81	6.84	7.27	500yr	5.90	7.11	8.59	10.63	13.72	18.89	21.69	500yr	16.72	20.85	25.30	27.36	28.07	500yr

