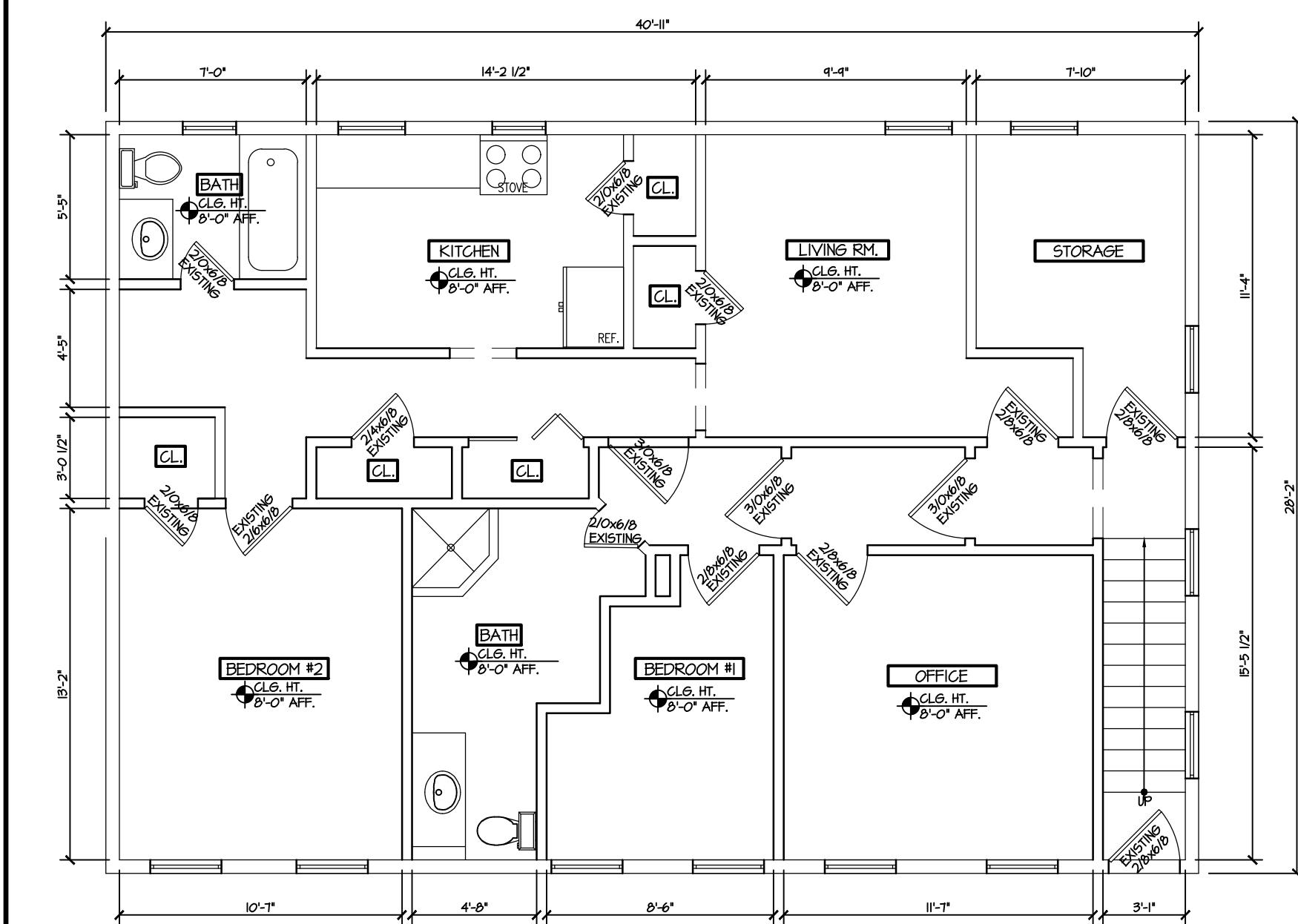
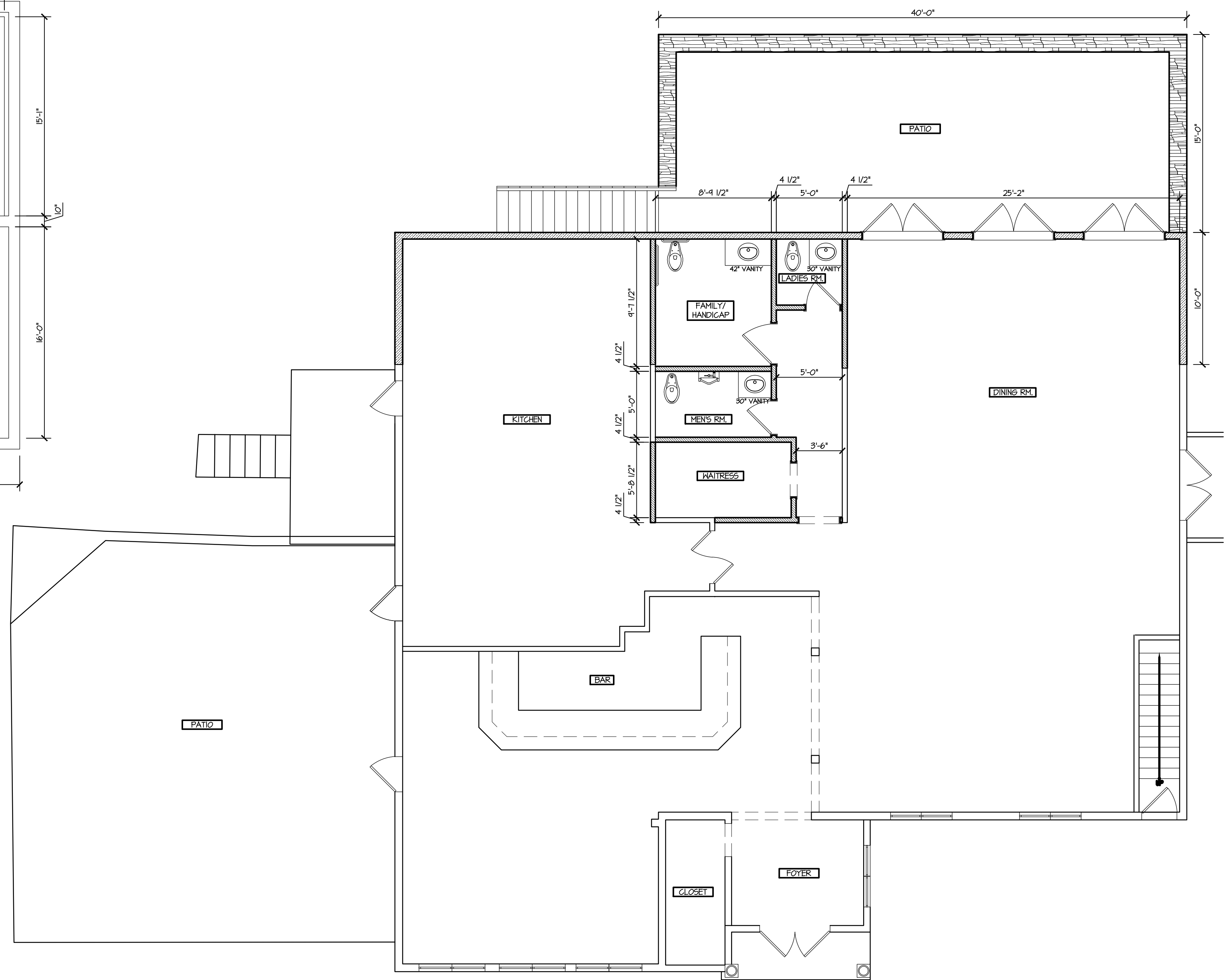


1 PROPOSED BASEMENT PLAN
 A-O SCALE: 3/16"=1'-0"



3 PROPOSED SECOND FLOOR PLAN
 A-O SCALE: 3/16"=1'-0"



2 PROPOSED FIRST FLOOR PLAN
 A-O SCALE: 3/16"=1'-0"

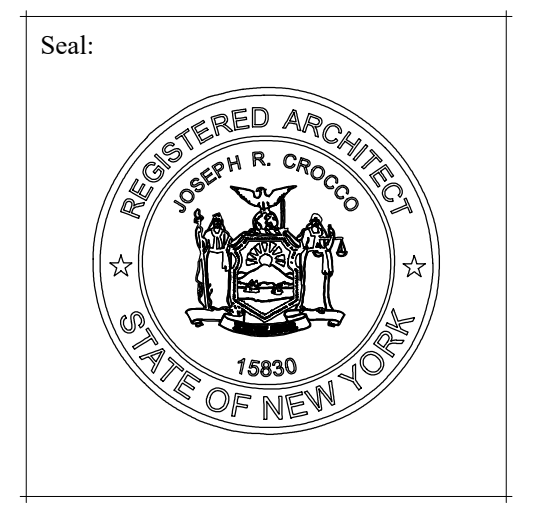
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| REVISION | DATE |
|----------|------|
| | |



Joseph R. Crocco architects
 new jersey architects
 4 macedonald avenue, suite 5
 armonk, new york 10504
 (914) 273-2774 fax: (914) 273-2776

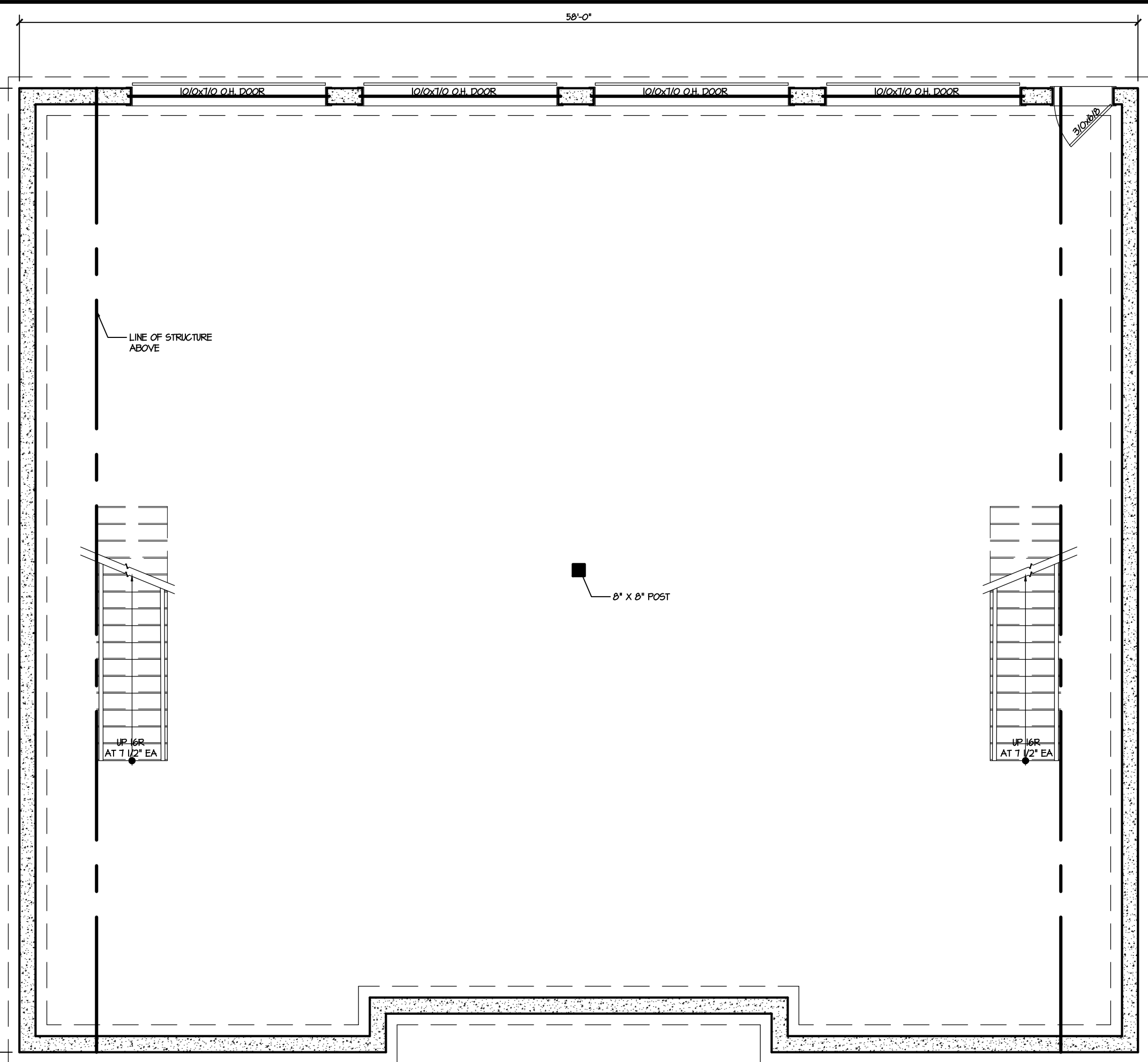
PROPOSED ALTERATION/ ADDITION:
 FOR:
GAVI
 15 OLD RTE 22
 ARMONK, NY

Dwg. Name: **PROPOSED FLOOR PLANS**

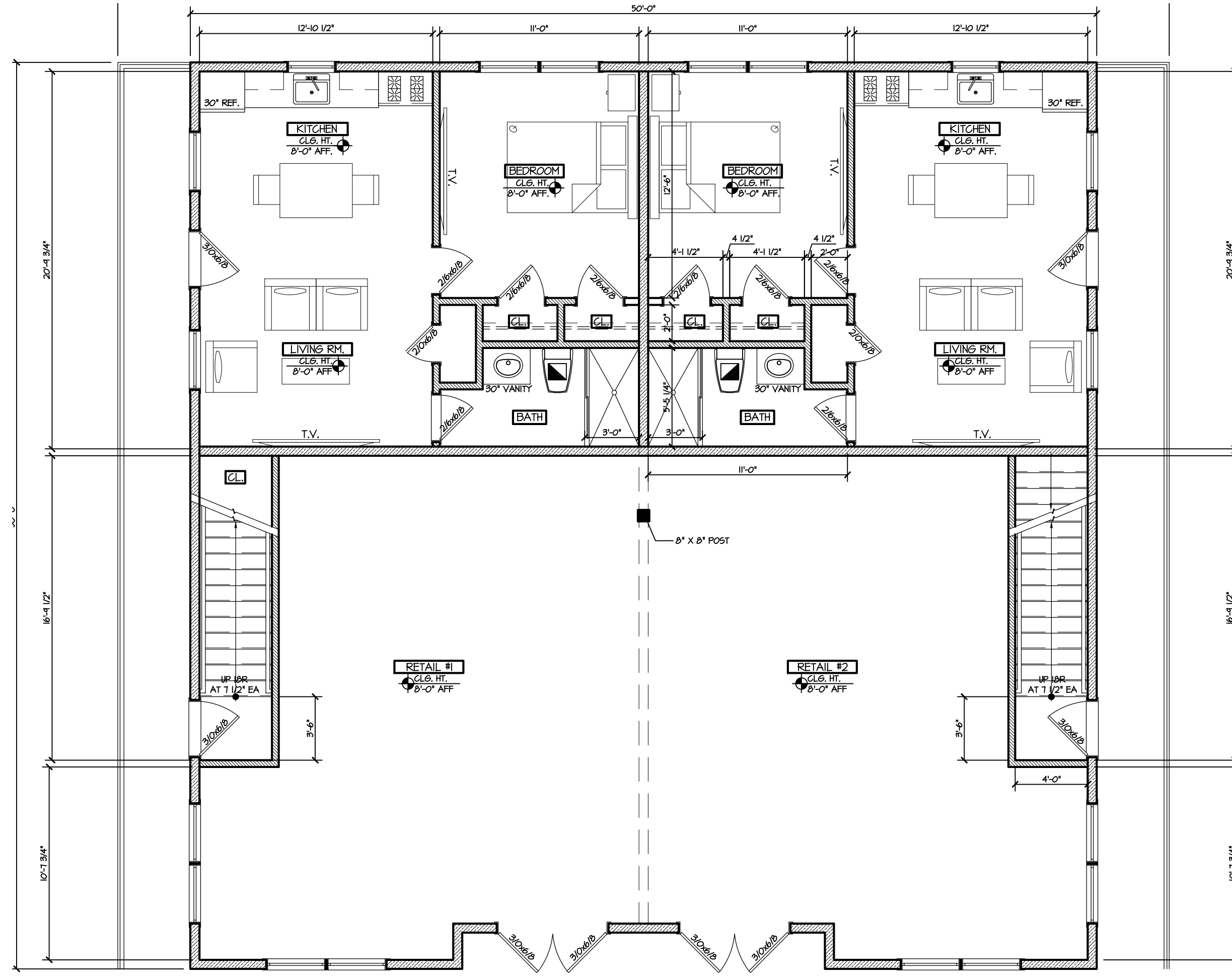
Project No: 23004
 Sheet Number: **A-0**
 Date: APRIL 4, 2023

APPROVED BY THE TOWN OF NORTH CASTLE PLANNING BOARD
 RESOLUTION DATED: _____ DATE _____
 CHRISTOPHER GARTHY, CHAIR
 TOWN OF NORTH CASTLE PLANNING BOARD

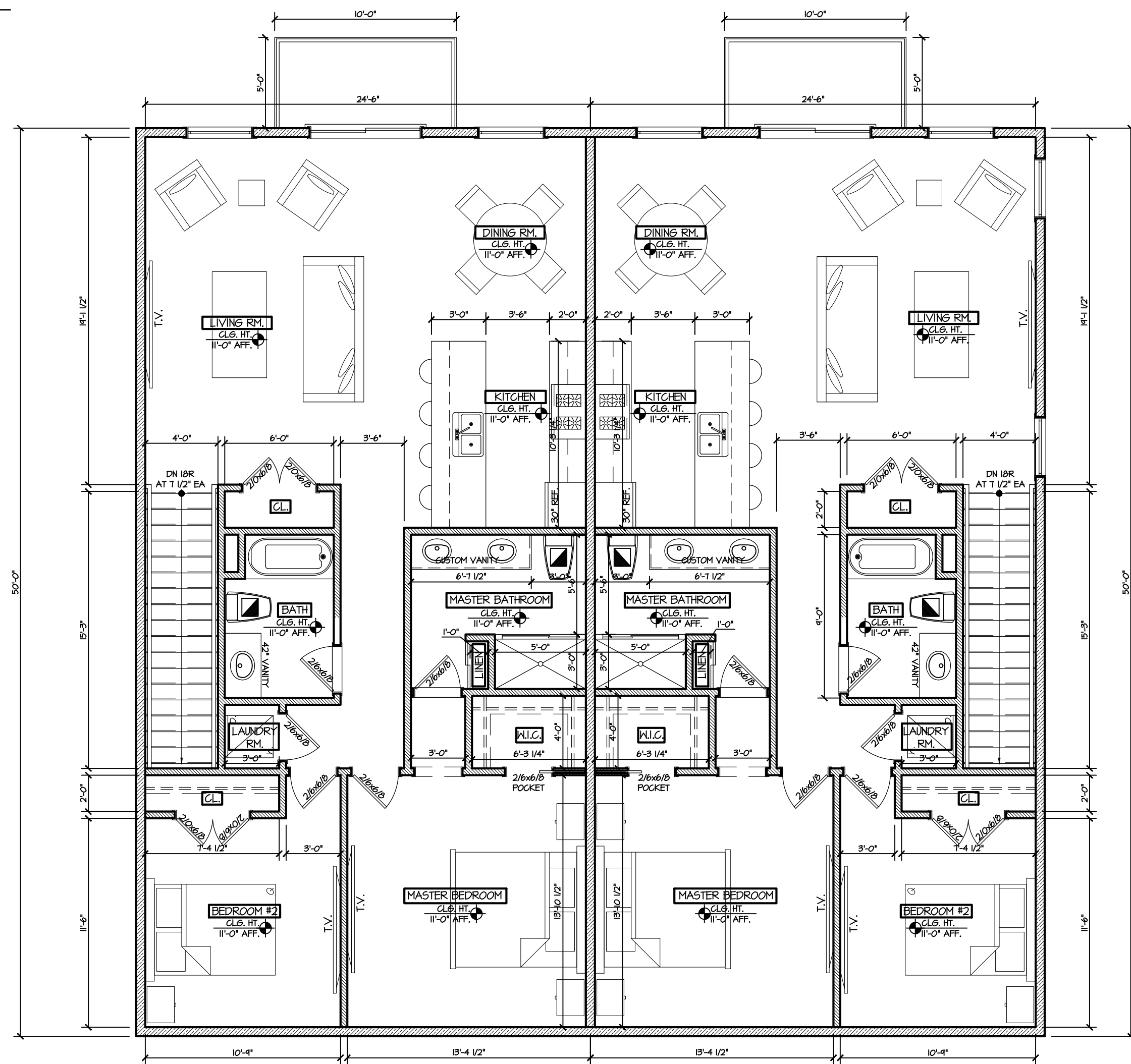
ENGINEERING PLANS REVIEWED FOR CONFORMANCE TO RESOLUTION:
 _____ DATE _____
 JOSEPH CERMELE, P.E.
 KELLARD SESSIONS CONSULTING P.C.
 CONSULTING TOWN ENGINEERS



1 PROPOSED BASEMENT PLAN
SCALE: 3/16"=1'-0"



2 PROPOSED FIRST FLOOR PLAN
SCALE: 3/16"=1'-0"



3 PROPOSED SECOND FLOOR PLAN
SCALE: 3/16"=1'-0"

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| REVISION | DATE |
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| | |



Joseph r. crocco architects

new york connecticut new jersey massachusetts

4 macedonald avenue, suite 5
armonk, new york 10504

(914) 273-2774 fax (914) 273-2776

PROPOSED MIXED USE STRUCTURE:

FOR:
15 OLD RTE 22
ARMONK, NY

APPROVED BY THE TOWN OF NORTH CASTLE PLANNING BOARD
RESOLUTION DATED: _____ DATE _____
CHRISTOPHER GARTHY, CHAIR
TOWN OF NORTH CASTLE PLANNING BOARD

ENGINEERING PLANS REVIEWED FOR CONFORMANCE TO RESOLUTION:

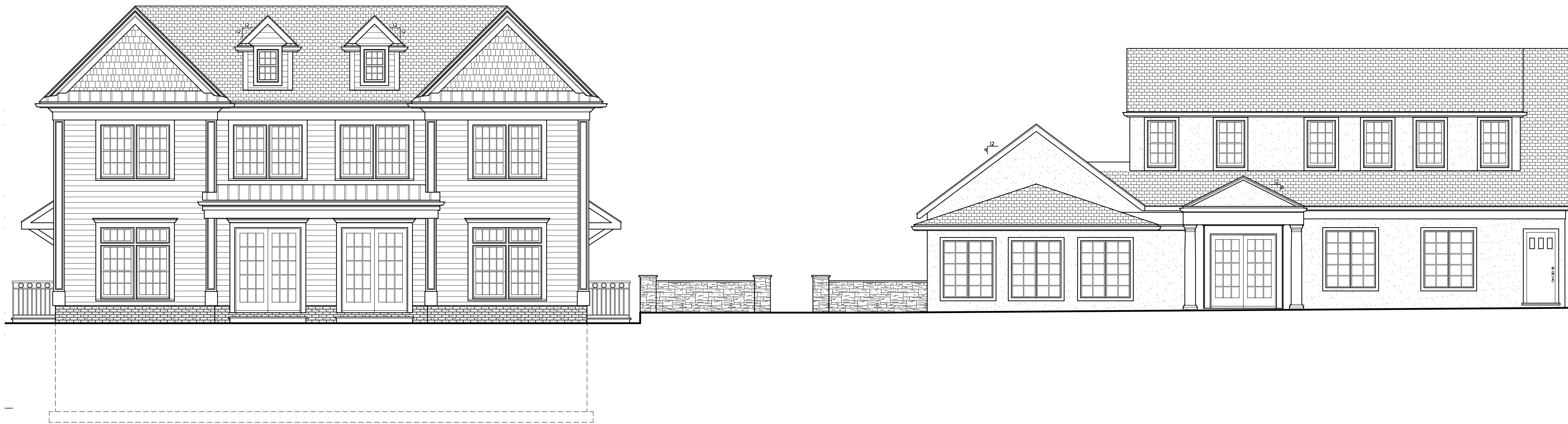
DATE _____
JOSEPH CERMELE, P.E.
KELLARD SESSIONS CONSULTING P.C.
CONSULTING TOWN ENGINEERS

Dwg. Name: **PROPOSED FLOOR PLANS**

Project No: 23004

Date: APRIL 4, 2023

Sheet Number: **A-1**



1 PROPOSED STREET SCAPE
A-2 SCALE: 3/16"=1'-0"



2 PROPOSED FRONT ELEVATION
A-2 SCALE: 1/4"=1'-0"

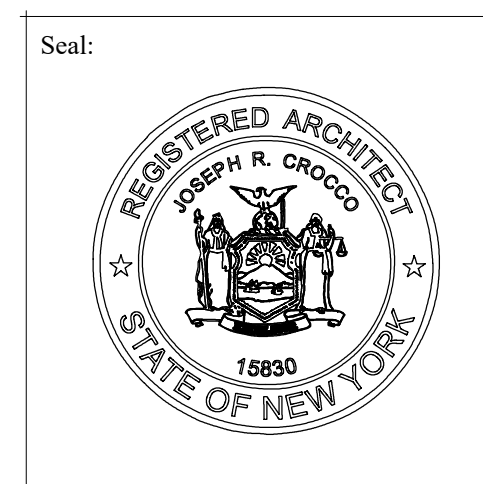
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| REVISION | DATE |
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architects

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armonk, new york 10504
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**PROPOSED
MIXED USE
STRUCTURE:**

FOR:
15 OLD RTE 22
ARMONK, NY

APPROVED BY THE TOWN OF NORTH CASTLE PLANNING BOARD
RESOLUTION DATED: _____ DATE _____
CHRISTOPHER GARTHY, CHAIR
TOWN OF NORTH CASTLE PLANNING BOARD

ENGINEERING PLANS REVIEWED FOR CONFORMANCE TO RESOLUTION:

DATE _____
JOSEPH CERMELE, P.E.
KELLARD SESSIONS CONSULTING P.C.
CONSULTING TOWN ENGINEERS

Dwg. Name:
ELEVATIONS

Project No:
23004

Sheet Number:
A-2

Date:
APRIL 4, 2023

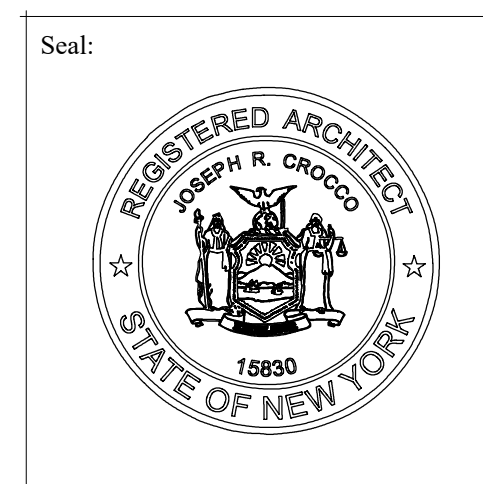
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 (914) 273-2774 fax (914) 273-2776

PROPOSED MIXED USE STRUCTURE:
 FOR:
 15 OLD RTE 22
 ARMONK, NY

Dwg. Name:
ELEVATIONS

Project No:
 23004

Sheet Number:
A-3

Date:
 APRIL 4, 2023

APPROVED BY THE TOWN OF NORTH CASTLE PLANNING BOARD
 RESOLUTION DATED: _____ DATE _____
 CHRISTOPHER CARTHY, CHAIR
 TOWN OF NORTH CASTLE PLANNING BOARD

ENGINEERING PLANS REVIEWED FOR CONFORMANCE TO RESOLUTION:
 _____ DATE _____
 JOSEPH CERMELE, P.E.
 KELLARD SESSIONS CONSULTING P.C.
 CONSULTING TOWN ENGINEERS

2ND FLOOR CEILING
2ND FLOOR WINDOW HEADER HT.
6'-0"

2ND FLOOR FINISHED FLOOR
1ST FLOOR CEILING
1ST FLOOR WINDOW HEADER HT.
8'-0"

1ST FLOOR FINISHED FLOOR
UNDERSIDE OF BASEMENT CLG.
8'-0"

BASEMENT FLOOR SLAB

2ND FLOOR CEILING
2ND FLOOR WINDOW HEADER HT.
6'-0"

2ND FLOOR FINISHED FLOOR
1ST FLOOR CEILING
1ST FLOOR WINDOW HEADER HT.
8'-0"

1ST FLOOR FINISHED FLOOR
UNDERSIDE OF BASEMENT CLG.
8'-0"

BASEMENT FLOOR SLAB

1 PROPOSED RIGHT SIDE ELEVATION
 A-3 SCALE: 3/16"=1'-0"

2 PROPOSED LEFT SIDE ELEVATION
 A-3 SCALE: 3/16"=1'-0"

2ND FLOOR CEILING
2ND FLOOR WINDOW HEADER HT.
6'-0"

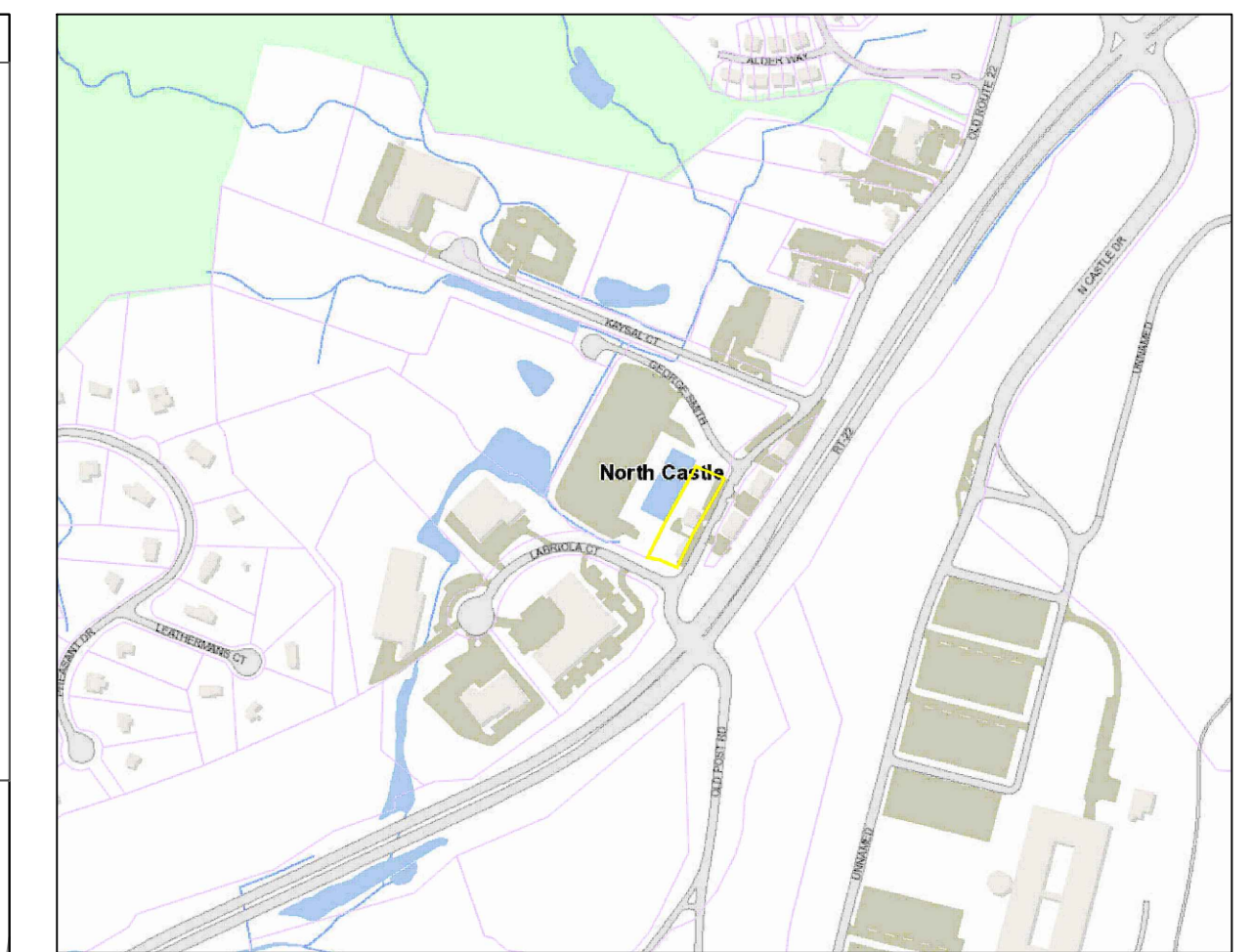
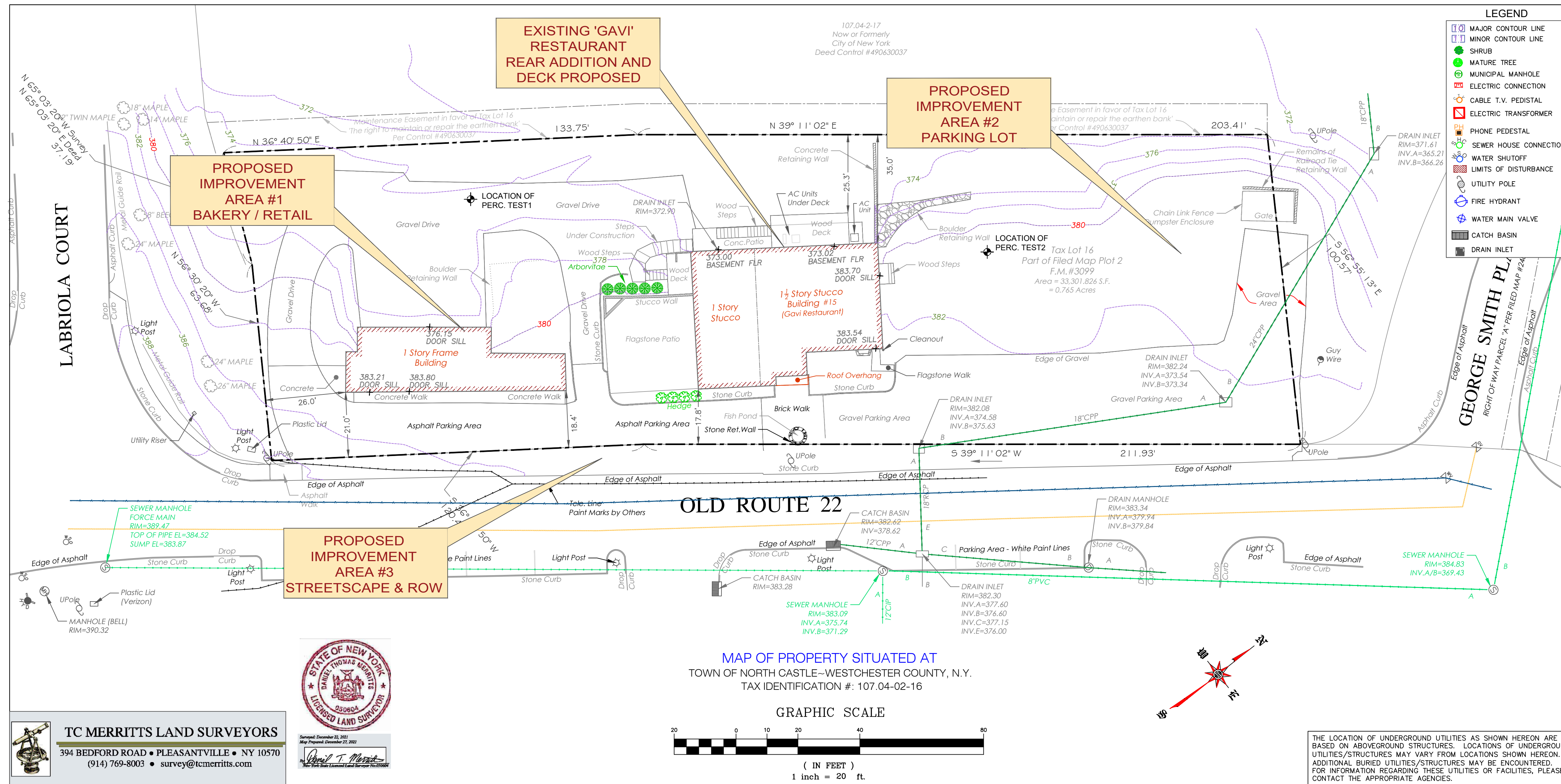
2ND FLOOR FINISHED FLOOR
1ST FLOOR CEILING
1ST FLOOR WINDOW HEADER HT.
8'-0"

1ST FLOOR FINISHED FLOOR
UNDERSIDE OF BASEMENT CLG.
8'-0"

BASEMENT FLOOR SLAB

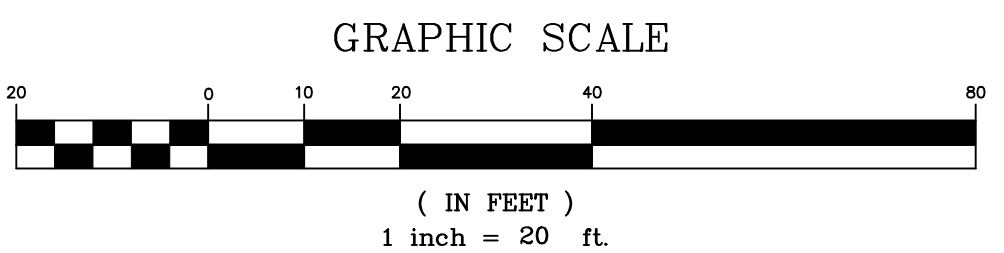
3 PROPOSED REAR ELEVATION
 A-3 SCALE: 1/4"=1'-0"

EXISTING CONDITIONS - TOPOGRAPHICAL SITE PLAN



TC MERRITTS LAND SURVEYORS
 394 BEDFORD ROAD • PLEASANTVILLE • NY 10570
 (914) 769-8003 • survey@tcmeritts.com

MAP OF PROPERTY SITUATED AT
 TOWN OF NORTH CASTLE - WESTCHESTER COUNTY, N.Y.
 TAX IDENTIFICATION #: 107.04-02-16



THE LOCATION OF UNDERGROUND UTILITIES AS SHOWN HEREON ARE BASED ON ABOVEGROUND STRUCTURES. LOCATIONS OF UNDERGROUND UTILITIES/STRUCTURES MAY VARY FROM LOCATIONS SHOWN HEREON. ADDITIONAL BURIED UTILITIES/STRUCTURES MAY BE ENCOUNTERED. FOR INFORMATION REGARDING THESE UTILITIES OR FACILITIES, PLEASE CONTACT THE APPROPRIATE AGENCIES.

SITE PHOTOS - EXISTING CONDITIONS



GENERAL NOTES:

- SCOPE:** THE PURPOSE OF THIS MAP IS TO PRESENT AN ASSESSMENT OF EXISTING CONDITIONS FOR THE ROADSIDE BUSINESS PROPERTY RESIDENTIAL PROPERTY LOCATED AT 15 OLD ROUTE 22 IN THE TOWN OF NORTH CASTLE, NY. PROPOSED ON THE SUBJECT PROPERTY IS THE RECONSTRUCTION OF A VACANT BUILDING TO SERVE AS FOOD SERVICE/RETAIL USE WITH ACCESSORY RESIDENTIAL UNITS ALONG WITH OTHER SITE IMPROVEMENTS RELATED TO CONSTRUCTION OF PAVED PARKING LOTS, ACCESS DRIVEWAYS, WALKWAYS, MODULAR BLOCK GRAVITY RETAINING WALLS AND STORMWATER MANAGEMENT SYSTEMS AS REQUIRED BY CODE. A REAR ADDITION AND RAISED DECK IS PROPOSED FOR THE EXISTING RESTAURANT. AS THE PROPERTY IS ZONED AS NON-RESIDENTIAL, ROADSIDE BUSINESS, ALL PROJECTS INVOLVING THIS DEGREE OF IMPROVEMENT REQUIRES SITE PLAN APPROVAL FROM THE TOWN PLANNING BOARD AS PRESENTED IN CHAPTER 355 OF TOWN CODE. THE PROPOSED USE IS CONSISTENT WITH LOCAL ZONING.
- MAPPING:** THE BASE MAP DEPICTED HEREIN WAS PREPARED FROM A LAND SURVEY PREPARED BY TC MERRITTS LAND SURVEYORS OF PLEASANTVILLE, NEW YORK, DATED OCTOBER 29, 2020 AND FROM AN ARCHITECTURAL CONCEPTUAL SITE PLAN PREPARED BY JOSEPH R. CROCCO ARCHITECTS.
 - PLANNING BOARD APPROVALS:** THE INTENT OF THIS SUBMISSION IS TO SEEK APPROVAL FROM THE PLANNING BOARD FOR A SITE PLAN APPROVAL FOR THE AFOREMENTIONED PROPOSED BUILDING AND SITE IMPROVEMENTS. THE INTENT OF THE SUBMISSION IS TO MEET ALL ZONING REQUIREMENTS WHERE POSSIBLE AND OBTAIN VARIANCES AS NEEDED WITH GUIDANCE FROM THE TOWN.
 - RELEVANT TOWN CODE:** TOWN OF NORTH CASTLE CODE CHAPTER 355 REGULATES ZONING, OFF STREET PARKING AND SITE PLAN APPROVAL AND CHAPTER 267 PROVIDE STATUTE ON LAND DEVELOPMENT ACTIVITY AND REQUIRED STORMWATER POLLUTION AND PREVENTION PLANNING (SWPPP).
 - CURRENT CONDITIONS:** THE EXISTING PROPERTY HAS 33,302 SQUARE FEET OF LAND WHICH CONTAINS TWO ROADSIDE BUSINESS ZONED BUILDINGS, ONE VACANT AND ANOTHER OPERATING AS A RESTAURANT. THE PROPERTY CONTAINS MULTIPLE OFF STREET PARKING SPACES WITHIN GRAVEL/UNPAVED DESIGNATED LOCATIONS TO ACCOMMODATE CURRENT USE AND IS SERVED BY MUNICIPAL SEWER, WATER AND NATURAL GAS. ROAD FRONTAGE IS PROVIDED ALONG OLD ROUTE 22. THE BUILDINGS AND DEVELOPED AREAS APPEAR MEET ZONING LOT COVERAGE AND DIMENSIONAL REQUIREMENTS FOR SIDE, FRONT YARD SETBACKS FOR THE RB ZONING DISTRICT. REAR YARD SETBACK IS PRE-EXISTING NON-COMFORMING.
 - CRITICAL/SENSITIVE AREAS:** THIS PROPERTY DOES NOT CONTAIN ANY FRESHWATER WETLANDS, WETLAND BUFFER AREAS, STEEP SLOPES OR AND FEMA DESIGNATED SPECIAL FLOODPLAIN HAZARD AREAS.
 - LIMITATIONS:** THIS PLAN IS NOT TO BE CONSTRUED TO SUPERCEDE ANY APPROVALS BY THE TOWN OF NORTH CASTLE PLANNING BOARD OR OTHER LAND USE BOARDS FOR SITE PLAN OR COMPLETE ZONING/CODE COMPLIANCE, FACILITY USE, OPERATION OR DESIGN. THIS MAP WAS PREPARED STRICTLY TO ASSESS THE CURRENT AND PROPOSED CONDITIONS CONSISTENT WITH THIS APPLICATION BEFORE THE LOCAL PLANNING BOARD.

ZONING SCHEDULE (RB) - BULK REQUIREMENTS

| SCHEDULE ITEM | REQUIRED | EXISTING | PROPOSED |
|---------------------------|------------------|--------------------|---------------------|
| Lot Area (min) | 30,000 s.f. | 33,302 s.f. | N/C |
| Street Frontage (min) | 100 ft. | 212 ft. | N/C |
| Lot Depth | 300 ft. | 100 ft. | N/C |
| Front Yard | 10 ft. | 17.8 ft. | 10.0 ft. |
| Yard (1 Side) | 10 ft. | 26.0 ft. | 56.3 ft. |
| Yard (Rear) | 10 ft.* | 35.0 ft. | 25 ft. |
| Max Coverage (Building) | 25% (8,325 s.f.) | 10.9% (3,640 s.f.) | 14.7% (4,900 s.f.) |
| Building Height (Feet) | 24 ft. | 24 ft. | N/C |
| Building Height (Stories) | 2.0 | 2.0 | N/C |
| Max FAR | 0.30 | 0.30 | 0.40 |
| Impervious Coverage | n/a | 25.8% (8,601 s.f.) | 77.2% (25,693 s.f.) |

* As per Zoning Schedule in Section 355-29E(1)a

GENERAL SITE DATA:

- PROPERTY INFORMATION & OWNER:**
 GAVI RESTAURANT
 15 OLD ROUTE 22
 ARMONK, N.Y. 10504
 TAX ID: 107.04-2-16
- 5. ENVIRONMENTAL CRITICAL AREAS:**
- LOCAL STEEP SLOPES - NONE
 - FEMA SFHA - NONE
 - FRESHWATER WETLANDS - NONE
 - WATERCOURSES - NONE
- 6. NRCS - USDA SOIL CLASSIFICATION:**
 Soil Type: Ub - Udorthents, smoothed

FOR ROADSIDE BUSINESS DISTRICT USE:

- LOT AREA (MIN) - 30,000 SF
- TOTAL BUILDING COVERAGE - 25% (8,325 SF)
- LOT DEPTH (MIN) - 300 FEET
- FRONT YARD (MIN) - 10 FEET
- SIDE (MIN ONE) - 10 FEET
- REAR (MIN) - 10 FEET
- HEIGHT (MAX STORIES) - 2.0 STORIES
- TOTAL PARKING PROPOSED = 54 SPACES
- PARKING REQ'D ADA (1 PER 50 PER USE) = 3 SPACES
- TOTAL PARKING REQ'D (AS PER 355-67) = 58 SPACES
- TREES REQ'D (AS PER 355-68A) = 6 TREES

3. LAND USE DEVELOPED AREA SUMMARY:

- EXISTING LOT AREA - 33,302 SF
- EXISTING TOTAL BUILDING COVERAGE - 3,640 SF (10.9%)
- EXISTING IMP. COVERAGE - 8,601 SF (25.8%)
- EXISTING PARKING PROVIDED - 35+V. EST.

4. UTILITY SERVICES:

- WATER - ARMONK WATER DISTRICT #4
- SEWER - ARMONK SEWER DISTRICT #2
- GAS - CON EDISON COMPANY OF NY



DAVID A. GOESSL, PE
CIVIL ENGINEER
 622 SPROUT BROOK ROAD
 PUTNAM VALLEY, NY 10579 (914) 227-0258

PROPOSED SITE IMPROVEMENTS TO
 GAVI RESTAURANT
 15 OLD ROUTE 22, ARMONK, NY 10504

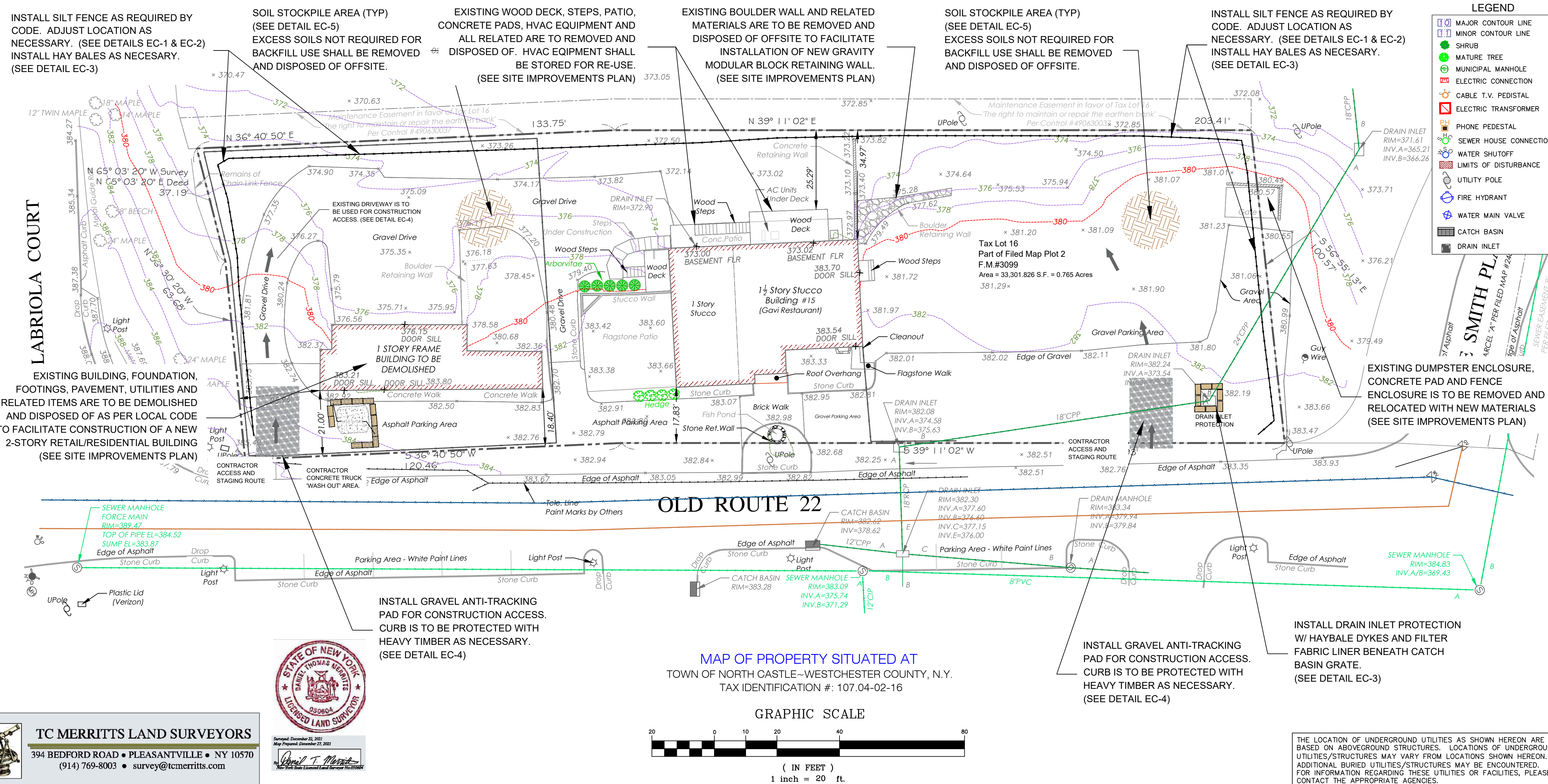
PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO
 DATE: APRIL 26, 2023 SCALE: 1" = 20 FEET SHEET: 1 OF 9

| NO. | REVISION | DATE |
|-----|---|-----------------|
| 1 | ADDED PROPOSED TWO STORY ADDITION AND RAISED DECK FOR GAVI RESTAURANT | July 18, 2023 |
| 2 | REVISED AS PER TOWN REVIEW COMMENTS | August 19, 2023 |

ANY UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING A SEAL OF A LICENSED LAND SURVEYOR OR PROFESSIONAL ENGINEER IS A VIOLATION OF SECTION 7209 OF THE NYS EDUCATION LAW.

NOTE: ADDITIONAL PLANIMETRIC SURVEY DATA SHOWN HEREIN ON THIS PLAN OF THE PROPERTY OF 15 OLD ROUTE 22, TOWN OF NORTH CASTLE, WESTCHESTER COUNTY, NEW YORK, 10504 WAS PREPARED FROM CONCEPTUAL PLANS PREPARED BY JOSEPH R. CROCCO ARCHITECTS, WESTCHESTER COUNTY GIS DATA, REFERENCED LAND SURVEY AND RECORDED DEED FOR SAID PROPERTY. ENGINEER ACCEPTS NO LIABILITY TO ERRORS AND OMISSIONS PROVIDED ON REFERENCED MAP SOURCES.

EROSION AND SEDIMENT CONTROL PLAN WITH PROPOSED DEMOLITION & REMOVALS



INSTALLATION & MAINTENANCE OF EROSION CONTROL CONSTRUCTION SCHEDULE:

- PRE-CONSTRUCTION EROSION CONTROL MEASURES**
 - Install all erosion control measures prior to start of construction.
 - Call for inspection from the appropriate Municipal Agency having jurisdiction at least 2 days prior to finish. All pre-construction measures shall be in full conformance with any NYSDEC SWPPP permits that may be issued for the project.
 - MAINTENANCE ACTIVITIES DURING ALL PHASES OF CONSTRUCTION**
 - After any rain causing runoff Contractor to inspect haybales, etc. and remove any excessive sediment, and inspect stockpiles and correct any problems with seed establishment.
 - Inspections shall be documented in writing and submitted to the appropriate Municipal Agency having jurisdiction.
 - Inspections for NYSDEC SWPPP permitting shall be documented and filed on the job for access and viewing and with the appropriate Town officials.
 - STOCKPILING OF SOILS AND ROUGH GRADING OF SITE**
 - Strip topsoil and stockpile soil for reuse and properly dispose of all excess soils.
 - Stockpile excavation subgrade materials and properly dispose of all excess soils.
 - Seed stockpiles with 1 lb. total annual rye or mix as per engineer.
 - Perform rough grading activities as soon as practical. Call for inspections as required.
 - FINE GRADING OF SITE**
 - Remove all remaining excess soils from site. Compact all graded materials as required.
 - Call for inspection from the appropriate Municipal Agency having jurisdiction at least 2 days prior to finish.
 - Perform all additional fine grading activities as required. Call for reinspection.
 - ESTABLISHMENT OF TURF, FINAL LANDSCAPING AND PLANTINGS**
 - Spread topsoil evenly over areas to be seeded. Hand rake level.
 - Broadcast 1.25 lb. Bag of Jonathan Green Tall Fescue mix or equal over areas to be seeded. Apply straw mulch and water within 2 days of completion of top placement. Application Rate 20 lbs per acre.
 - Install turf (optional) landscaping materials and any replacement trees.
 - Demobilize all equipment and materials from site as necessary. Erosion controls may be removed upon 80% established uniform density of restorative turf and plantings.
 - Call for inspection from the appropriate Municipal Agency having jurisdiction at least 2 days prior to finish.
- FINAL INSPECTION**
- Perform any as-built drawings, land surveys and or engineering certifications. Submit documents to the appropriate Municipal Agency having jurisdiction.
 - Contractor/Owner shall file Notice of Termination for any open NYSDEC SWPPP permit(s).
 - Call for inspection from the appropriate Municipal Agency having jurisdiction at least 2 days prior to finish.
 - Remove all erosion control measures upon establishment of turf or as per the Municipal Agency having jurisdiction.

CONTRACTOR CERTIFICATION FOR SWPPP/SWEC COMPLIANCE:

THE UNDERSIGNED HEREBY CERTIFIES AND AGREES TO COMPLY WITH THE TERMS AND CONDITIONS OF THE STORM WATER, POLLUTION PREVENTION PLAN AND AGREES TO IMPLEMENT ANY AND ALL CORRECTIVE ACTIONS IDENTIFIED BY THE NYSDEC QUALIFIED INSPECTOR AND/OR TOWN ENGINEER AND/OR BUILDING INSPECTOR DURING ALL SITE INSPECTIONS. FURTHERMORE THE UNDERSIGNED UNDERSTANDS THAT THE OWNER AND/OR PERMIT HOLDER SHALL COMPLY WITH ALL LOCAL CODES FOR STORMWATER MANAGEMENT AND ALL TERMS AND CONDITIONS OF NEW YORK STATE POLLUTANT DISCHARGE ELIMINATION SYSTEM (SPDES) GENERAL PERMIT FOR STORMWATER DISCHARGES FROM ACTIVE CONSTRUCTION SITES AS IT IS UNLAWFUL FOR ANY PERSON TO CAUSE OR CONTRIBUTE TO A VIOLATION(S) OF WATER QUALITY STANDARDS.

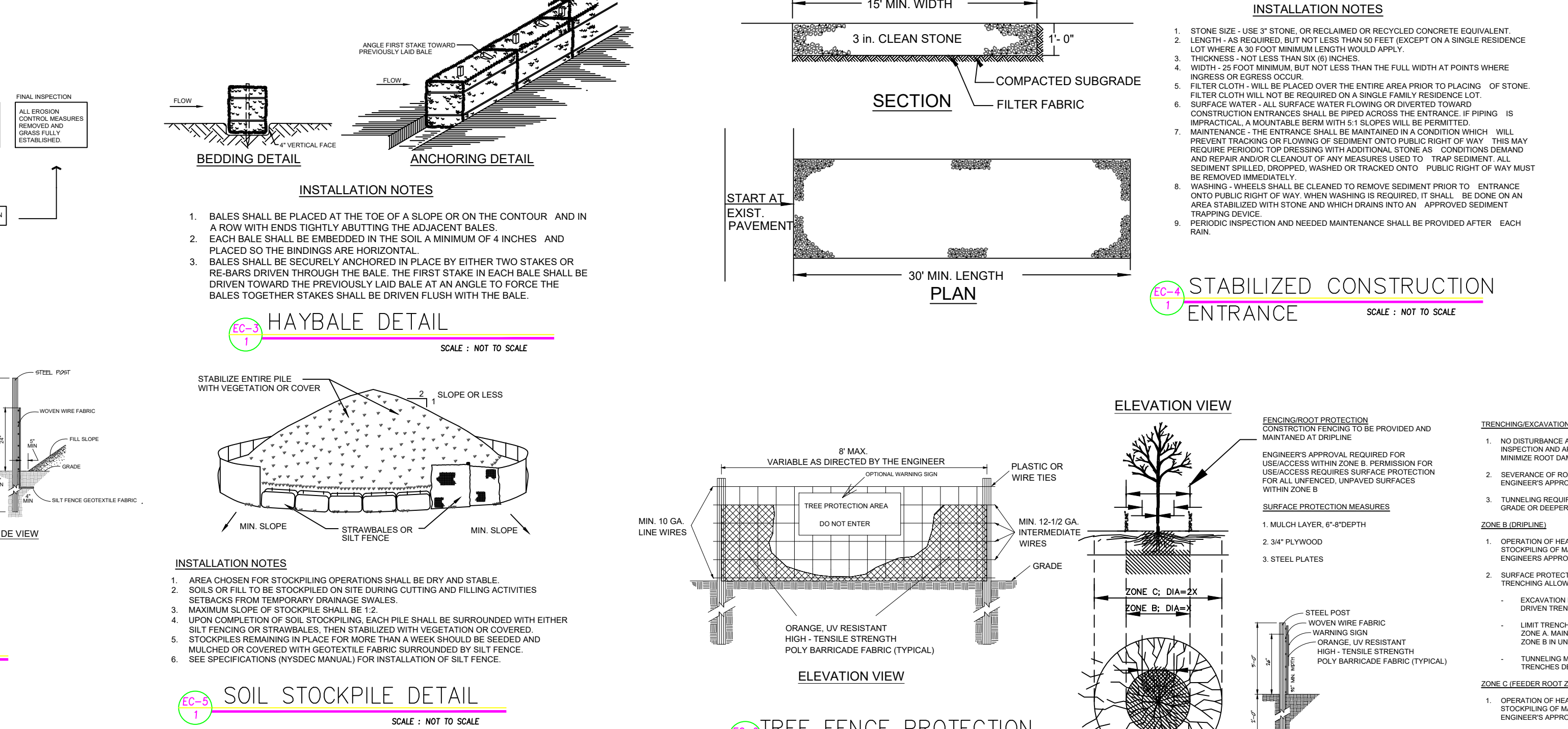
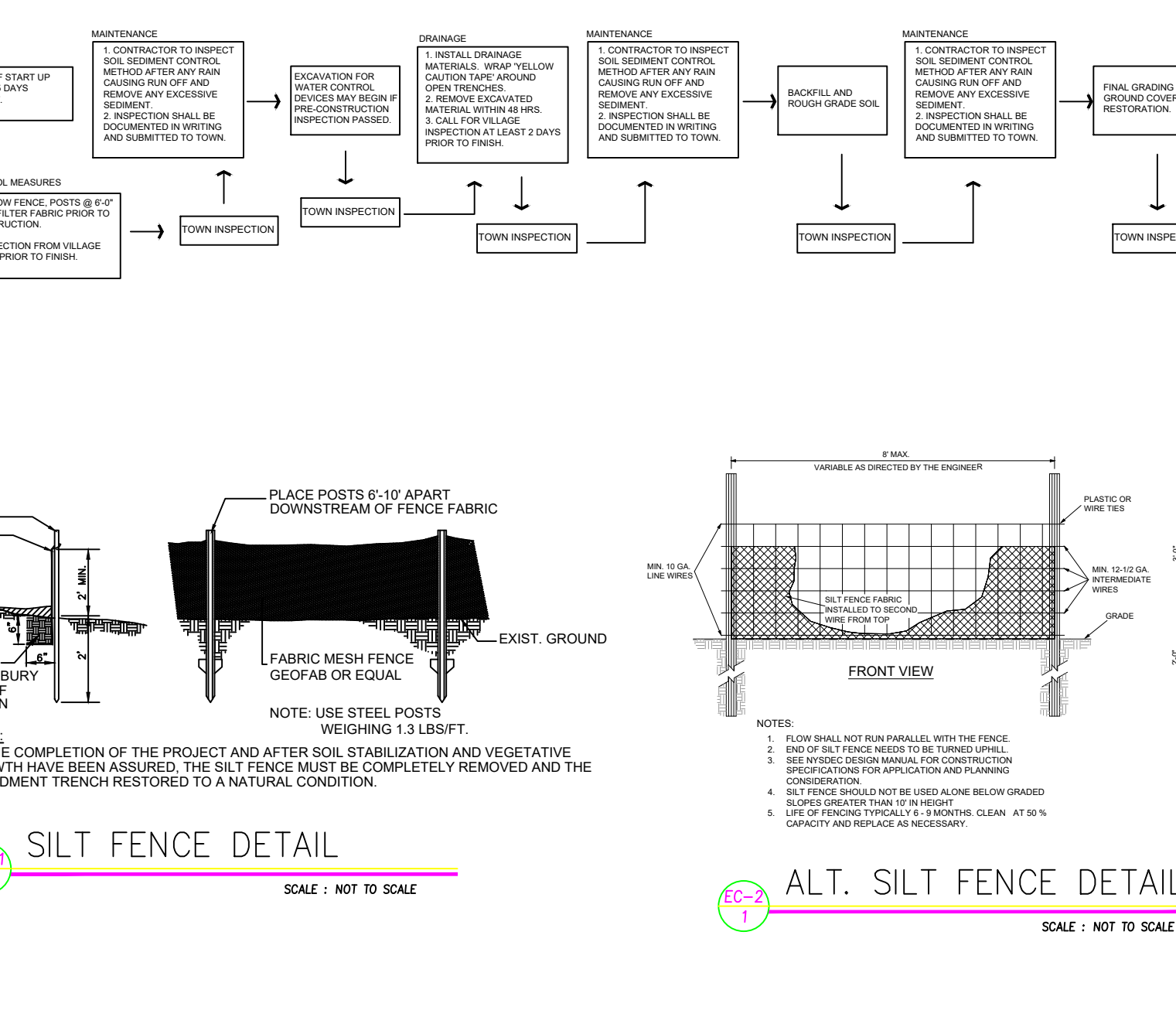
NAME: _____
SIGNATURE: _____
DATED: _____

OWNER ACKNOWLEDGEMENT FOR POST CONSTRUCTION MAINTENANCE & COMPLIANCE:

- PRIOR TO THE ISSUANCE OF A CERTIFICATE OF OCCUPANCY, THE APPLICANT SHALL PROVIDE A MAINTENANCE SCHEDULE AND PROCEDURES FOR ALL PROPOSED STORMWATER MANAGEMENT INFRASTRUCTURE.
- PRIOR TO THE ISSUANCE OF A CERTIFICATE OF OCCUPANCY, THE APPLICANT SHALL SUBMIT A STORMWATER AS-BUILT SURVEY THAT INCLUDES TOPOGRAPHY AND THE LOCATION, RIM ELEVATIONS AND INVERT ELEVATIONS OF ALL ON-SITE STORMWATER FACILITIES FOR REVIEW BY THE TOWN.
- PRIOR TO THE ISSUANCE OF A CERTIFICATE OF OCCUPANCY, A CONSTRUCTION, MAINTENANCE AND INSPECTION DECLARATION FOR THE STORMWATER MANAGEMENT FACILITIES INSTALLED IN A FORM SATISFACTORY TO THE TOWN, SHALL BE FULLY EXECUTED AND SUBMITTED TO THE TOWN.

NAME: _____
SIGNATURE: _____
DATED: _____

EROSION CONTROL SCHEDULE AND DETAILS



DAVID A. GOESSL, PE
CIVIL ENGINEER
622 SPROUT BROOK ROAD
PUTNAM VALLEY, NY 10579 (914) 227-0258

PROPOSED SITE IMPROVEMENTS TO
GAVI RESTAURANT
15 OLD ROUTE 22, ARMONK, NY 10504

PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO

DATE: APRIL 26, 2023 SCALE: 1"=20 FEET SHEET: 2 OF 9

| NO. | REVISION | DATE |
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| 2 | REVISED AS PER TOWN REVIEW COMMENTS | August 19, 2023 |

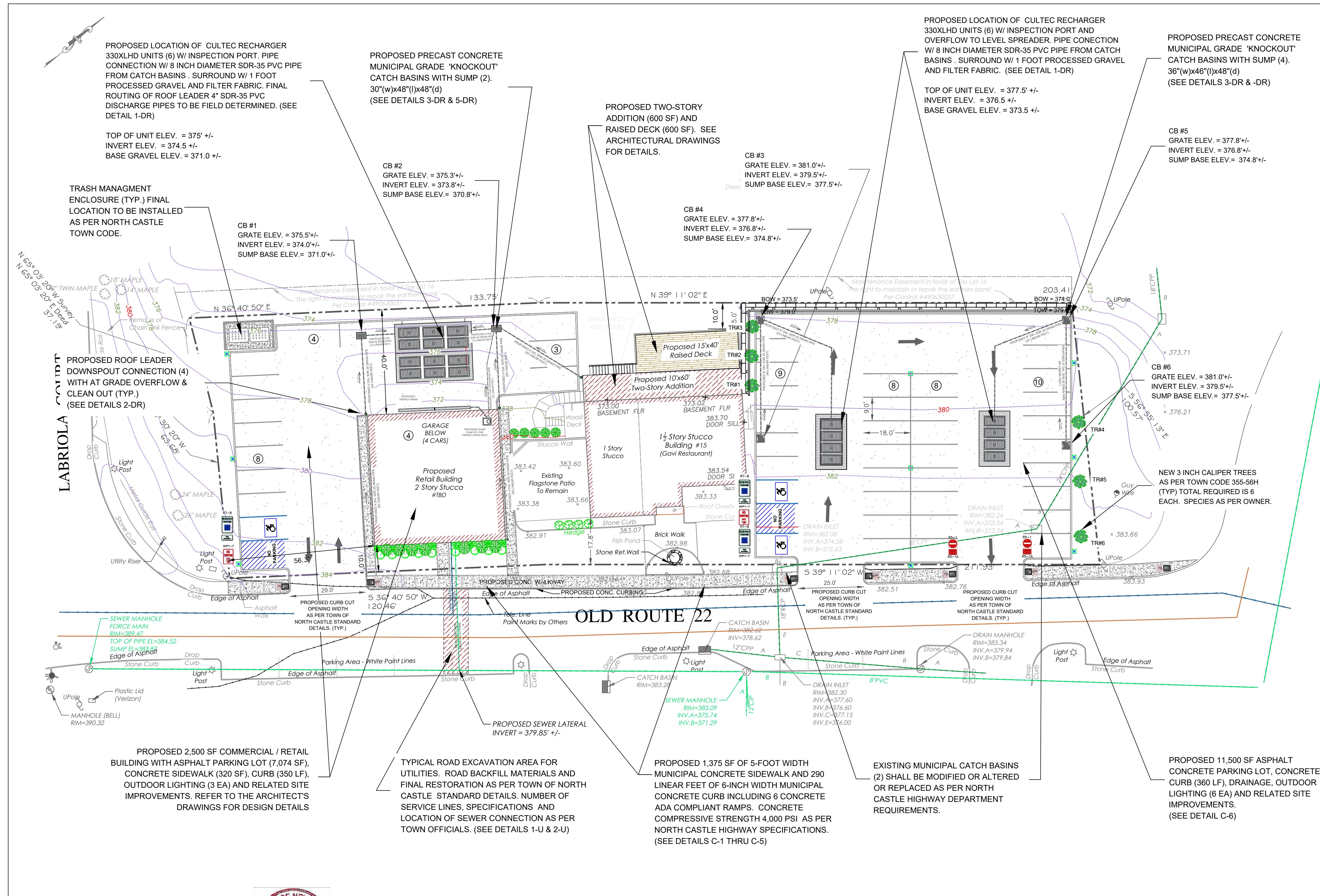
TC MERRITTS LAND SURVEYORS
394 BEDFORD ROAD • PLEASANTVILLE • NY 10570
(914) 769-8003 • survey@tcmeritts.com



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PROPOSED CONDITIONS - SITE IMPROVEMENTS AND DRAINAGE PLAN



GENERAL CONSTRUCTION NOTES:

- The Applicant shall secure all of the necessary permits from the Town of North Castle to ensure compliance with Local, County and State Building, Highway and Sanitary Codes. The Applicant is responsible to contact the Building Department to schedule an inspection of the sediment and erosion control practices prior to the start of construction.
- During work and upon completion, the Applicant shall schedule all of the necessary inspections and certificates of approval with the Town of North Castle officials.
- The Applicant shall secure the services of a NYS licensed land surveyor as necessary to stake out the exact location of proposed improvements and as required by the Town for record documents.
- The Applicant shall verify location of all underground utilities by calling Dig Safe NY @ 1-(800) 962-7962 to ensure that there are no conflicts with existing systems. Private installations shall also be identified as required.
- Any existing utilities, pavement, sidewalk, curbing, grass areas etc., disturbed and/or damaged during construction, must be replaced and/or repaired at the Applicant's expense.
- The Applicant shall secure the work zone through proper placement of construction fencing materials, cones, barricades, and caution tape.
- All debris, excess soils and waste materials, as a result of this proposed improvement, shall be removed from site and disposed of properly. All construction fuels and chemicals shall be transported in approved sealed containers and shall be removed from the site by the Contractor daily.
- All fill material shall consist of clean soils, or soil-rock mixture free from organic matter, construction debris or other deleterious material. Materials shall contain no rock or lump over 6" in greatest dimension and not more than 15% of the rocks or lumps shall be larger than 2.5" in greatest dimension.
- Should unforeseen conditions or circumstances develop or other causes necessitate changes to the approved plans, the Applicant shall notify the Design Engineer of record.
- All erosion controls and protective measures shall conform to the "New York State Standards for Erosion and Sediment Control." The Town Inspector may specify additional sediment and erosion control measures to safeguard the public right of way and adjacent properties. All areas of disturbance shall be restored at the earliest practical date and/or immediately upon suspension of work. Temporary erosion and sediment control measures shall not be removed until site stabilization (80% uniform density of permanent vegetation or permanent mulch/stone) has been achieved.
- Construction erosion control and protection measures shall be inspected by a qualified engineer or trained individual having received NYSDEC 4-hour erosion and sediment control training at a minimum of weekly and following all rain events greater than 0.5 inch.

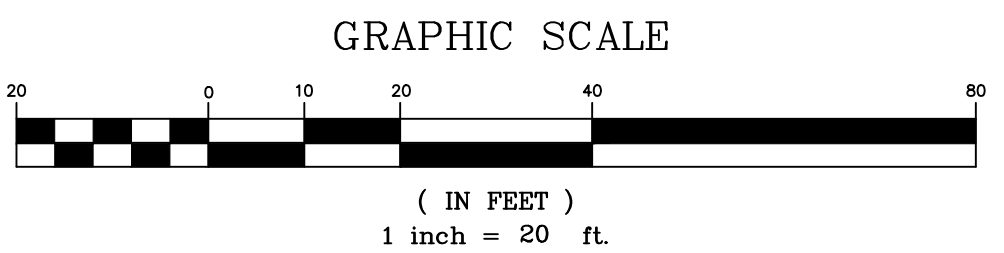
STORMWATER SYSTEM NOTES:

- The Applicant shall safeguard the limits of improvements through proper installation of silt fencing and hay bales downgrade from all excavation areas and stockpiles soil and gravels materials.
- The Contractor shall verify all field dimensions and drainage layouts prior to performing any installation. Any discrepancies shall be immediately reported to the Engineer of record.
- The Contractor shall verify depth upon excavation for suitable soils and consult with the Design Engineer prior to installing any drainage systems. The Design Engineer will verify soil percolation rates and prior test results at the time of construction. Any design changes to the storm water system during construction due to unforeseen circumstances such as shallow groundwater, rock, utility conflict etc., must be resubmitted to the Town of North Castle Building and Engineering Departments for approval prior to construction.
- The Contractor shall schedule required inspections at least 48 hours in advance to both Engineer of record and Town Inspector, and that no work shall be covered or concealed until the required inspections are passed.
- Stormwater drainage systems shall be installed along the proposed pathway as indicated on the plans. Pipe materials for catch basin and roof leader downspouts shall be SDR-35 PVC (or Sch. 40) piping. Underground infiltrating stormwater chamber(s) shall not be buried within ten feet of a building foundation nor ten feet from any adjacent developed property or right of way. The proposed drainage system is designed to handle a 24 hour, 100 year design storm in accordance with NYSDEC Stormwater Design Manual for net impervious surfaces created by the proposed parking lots, paved surfaces and building improvements and shall be phased with this work to be commenced upon completion of the proposed building, site grading and Redi-Rock retaining walls as to avoid incidental damage from construction and heavy equipment.
- The proposed stormwater system consists of 12 Cultec 330XLHD Chambers for the retail portion of the property and another 8 Cultec 330XLHD Chambers for the paved parking lot adjacent to Gavi Restaurant. All chambers are to be set level and include interconnections consisting of 6" diameter PVC (or HDPE) piping. The garage lower level of the retail building will contain an exterior trench drain with flow into a new sump pump pit with final discharge to the new drywells.
- The proposed location of the drywell systems shall be in the rear and right side yards maintaining minimum 10 foot setbacks from building and property lines. Owner/Contractor shall contact the Design Engineer should conflict(s) exist.

OWNER POST CONSTRUCTION MAINTENANCE:

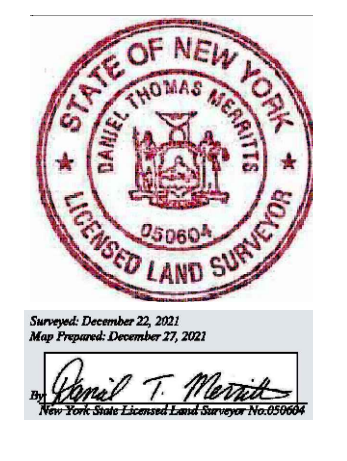
- The owner shall inspect all roof leader downspouts, inspections ports and cleanout caps once per year to ensure proper connections are in place.
- The owner shall inspect and remove all debris from the grate of any open yard drain and catch basins regularly with additional emphasis during the fall and winter months.
- The owner shall inspect and remove all accumulated debris from the sumps of any catch basin or yard drain at a minimum of once per year. Adjust frequency as necessary.
- Storm water facilities shall be maintained in accordance with best management practices and and Cultec maintenance literature. The owner shall have the said system inspected and certified at 5-year intervals (minimum) or in accordance to local codes whichever is more stringent.

MAP OF PROPERTY SITUATED AT
TOWN OF NORTH CASTLE - WESTCHESTER COUNTY, N.Y.
TAX IDENTIFICATION #: 107.04-02-16



THE LOCATION OF UNDERGROUND UTILITIES AS SHOWN HEREON ARE BASED ON ABOVEGROUND STRUCTURES. LOCATIONS OF UNDERGROUND UTILITIES/STRUCTURES MAY VARY FROM LOCATIONS SHOWN HEREON. ADDITIONAL BURIED UTILITIES/STRUCTURES MAY BE ENCOUNTERED. FOR INFORMATION REGARDING THESE UTILITIES OR FACILITIES, PLEASE CONTACT THE APPROPRIATE AGENCIES.

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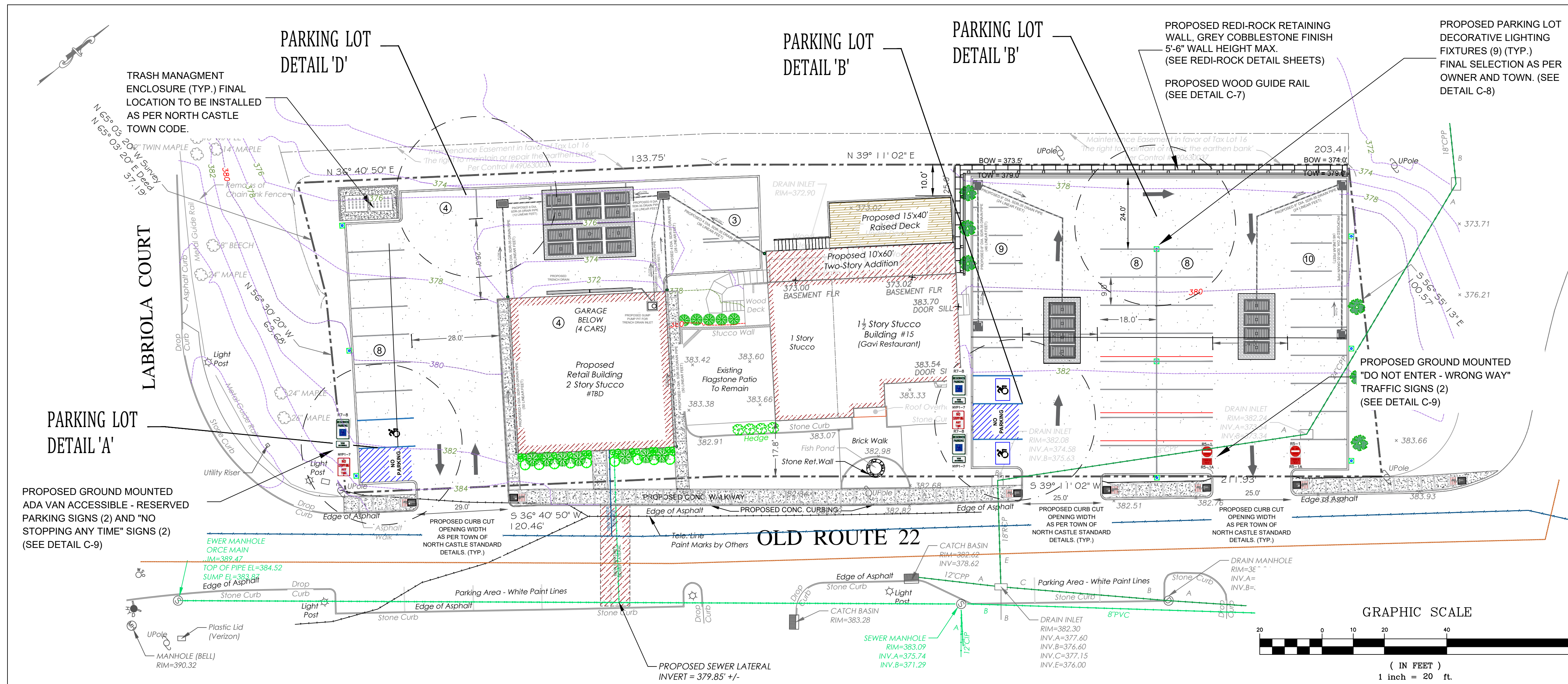
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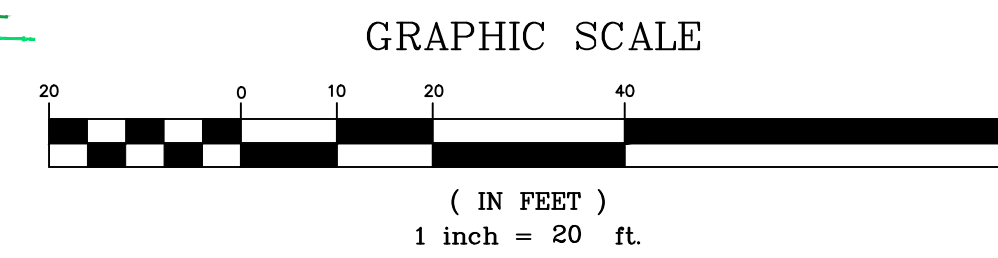
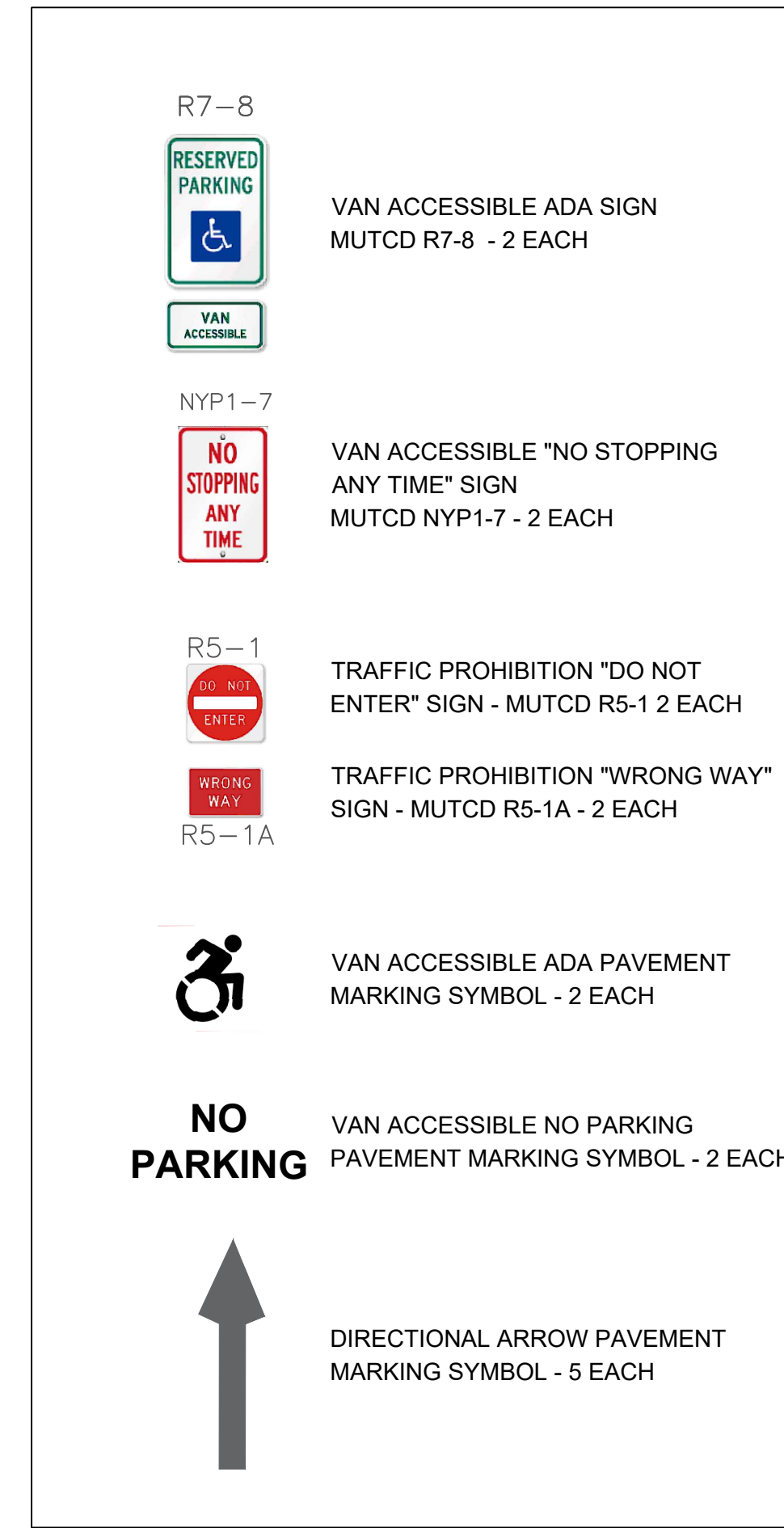
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PARKING LOT LAYOUT PLAN



SIGN AND SYMBOL INDEX

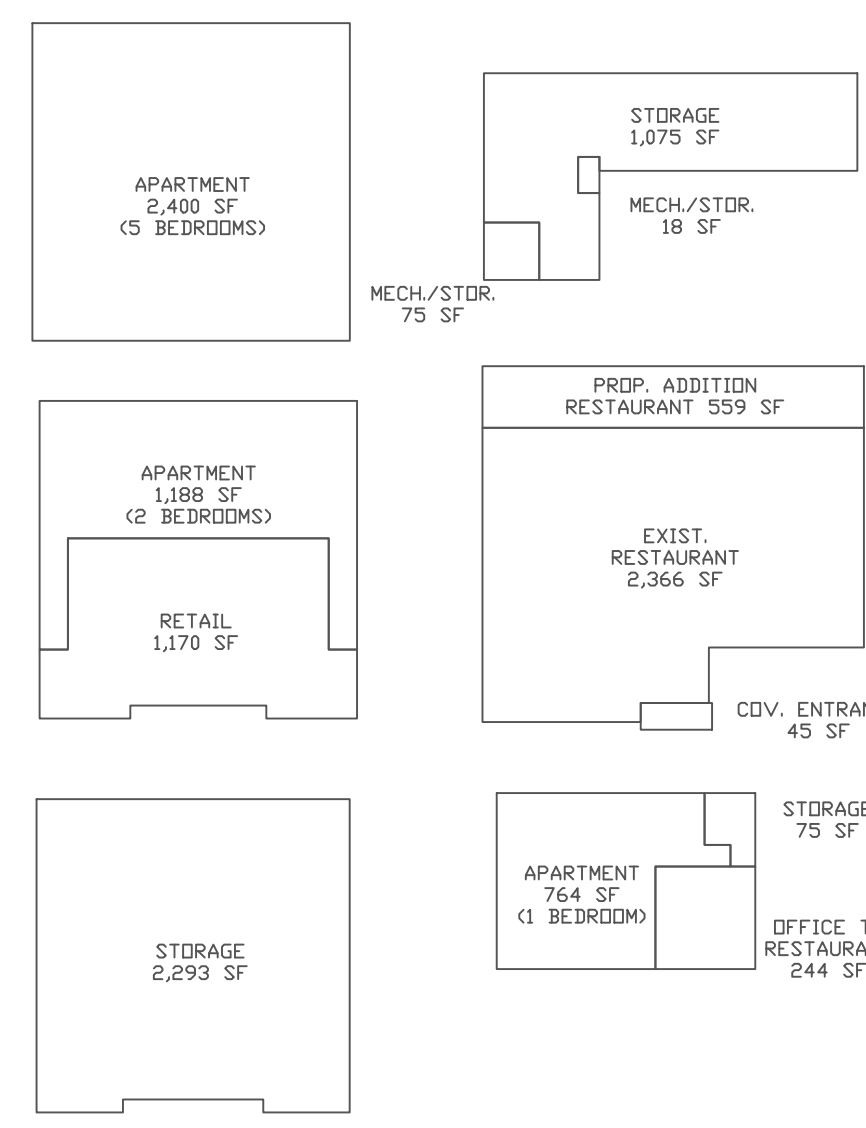


PARKING SPACE ANALYSIS (355-57):

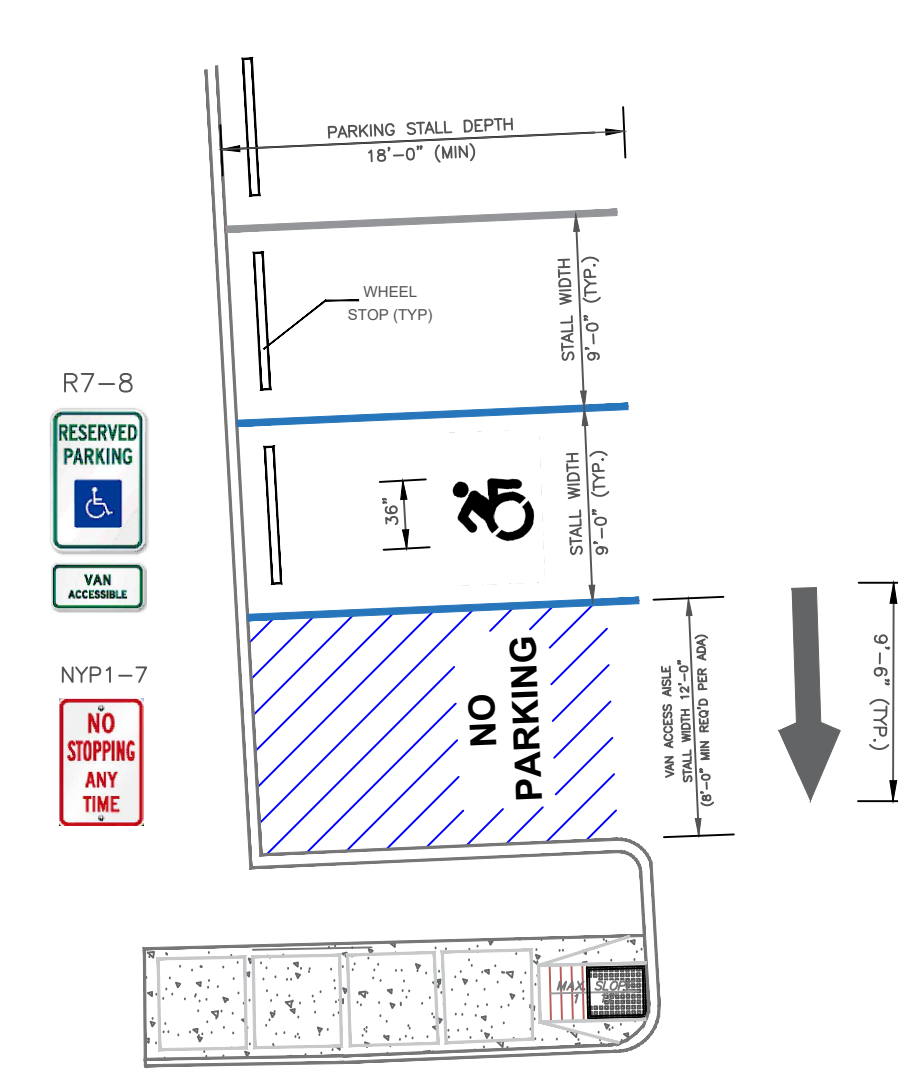
- MINIMUM OFF STREET PARKING PER USE:
- ACCESSORY APARTMENT 1 PER BEDROOM
 - RESTAURANT 1 PER 75 SF
 - RETAIL 1 PER 200 SF
 - OFFICE 1 PER 250 SF
 - STORAGE 1 PER 1,200 SF

- AREA USE ANALYSIS:
- ACCESSORY APARTMENT (8 ROOMS)
 - RESTAURANT SPACE = 2,366 + 559 = 2,925 SF
 - RETAIL SPACE = 1,170 SF
 - OFFICE = 244 SF
 - STORAGE = 2,293 + 1,075 + 18 + 75 + 75 = 3,536 SF

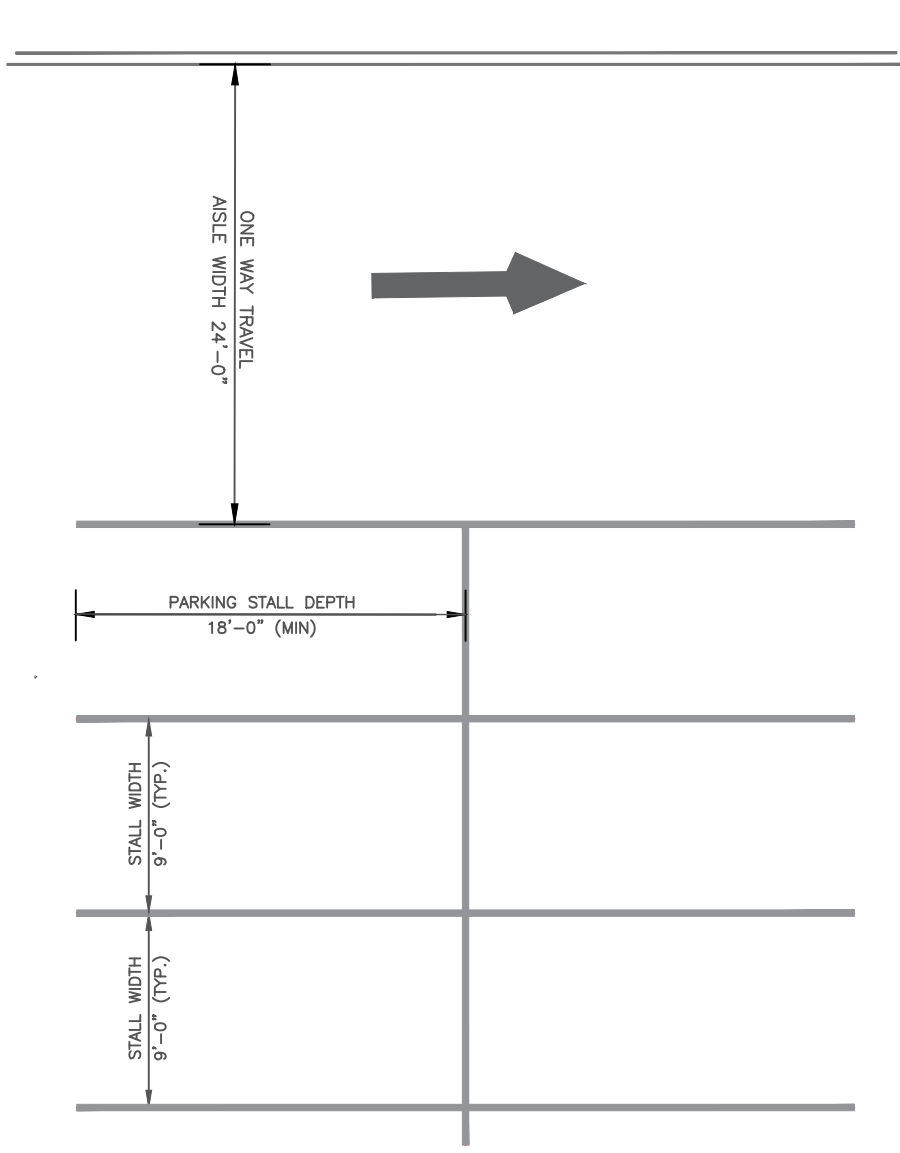
- PARKING REQUIREMENT ANALYSIS:
- APARTMENT - 8 SPACES
 - RESTAURANT - 2,925SF @ 1/75SF = 39 SPACES
 - RETAIL - 1,170SF @ 1/200SF = 5.85 SPACES
 - OFFICE - 244SF @ 1/250SF = 0.98 SPACES
 - STORAGE - 3,536SF @ 1/1,200SF = 2.94 SPACES
 - TOTAL PARKING REQUIRED = 56.77 SPACES (ROUND 58)
 - TOTAL PARKING PROPOSED = 53 SPACES
 - PARKING REQ'D ADA (1 PER 50 PER USE) = 3 SPACES



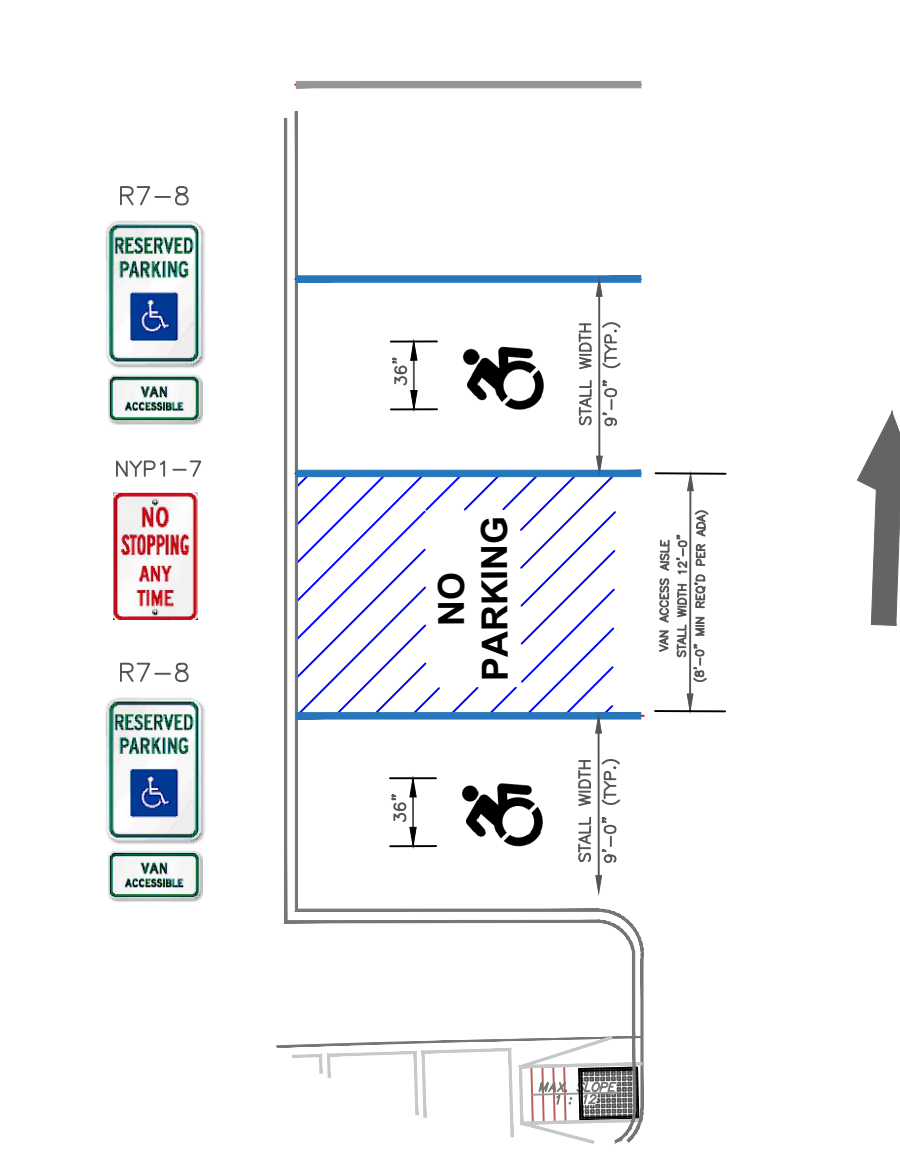
PARKING LOT DETAIL 'A'



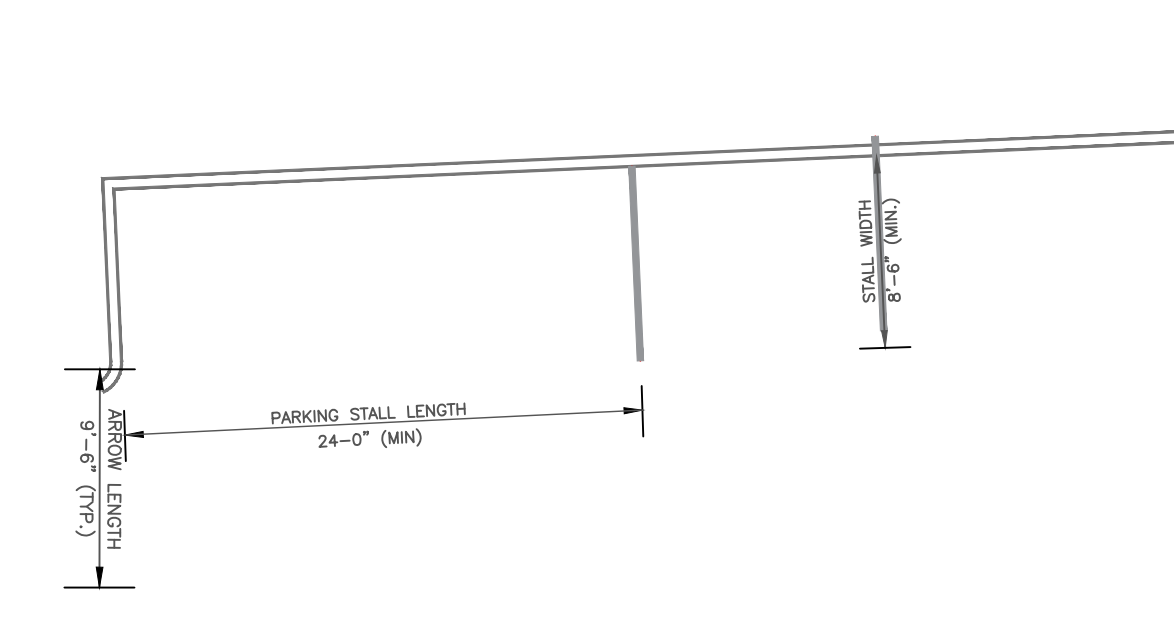
PARKING LOT DETAIL 'B'



PARKING LOT DETAIL 'C'



PARKING LOT DETAIL 'D'



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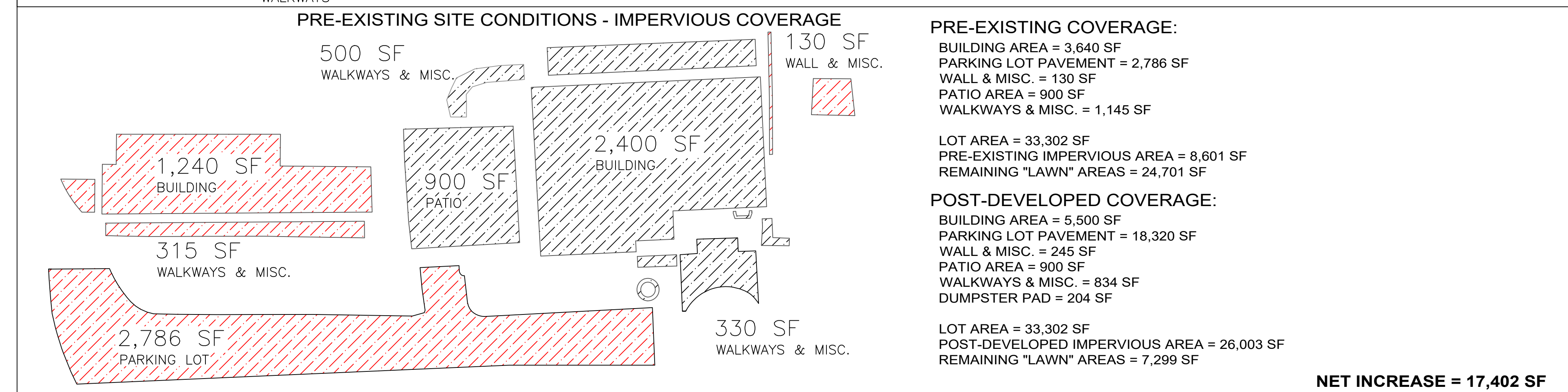
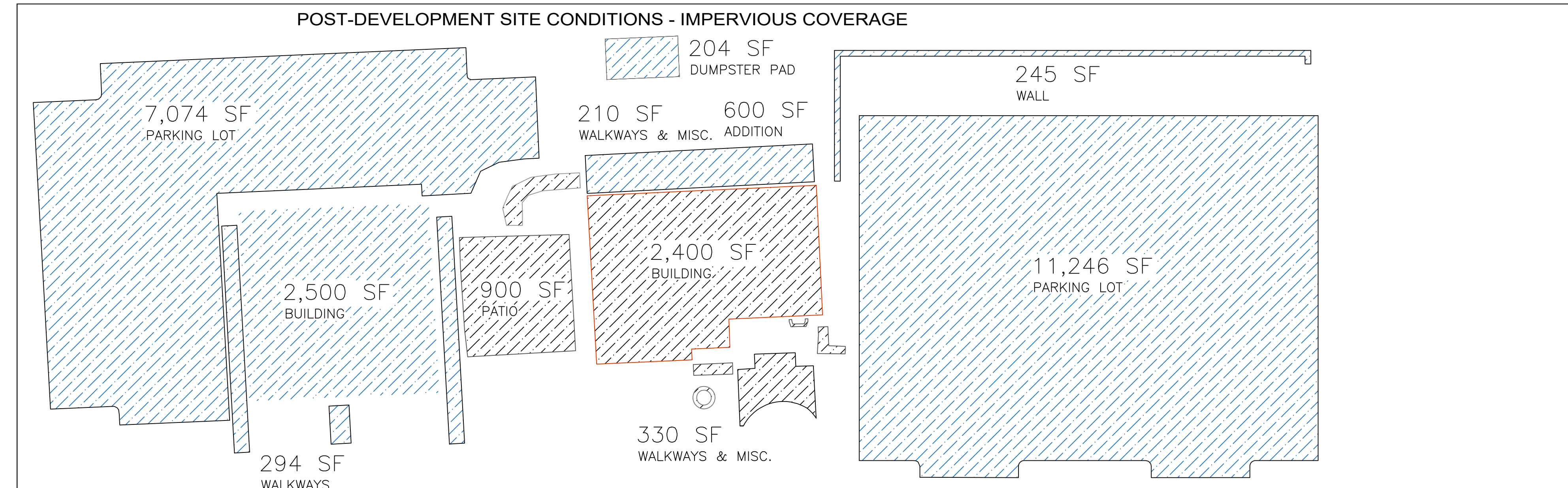
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DRAINAGE MODELING (AS PER NYSDEC SWDM)



PRE-EXISTING COVERAGE:
 BUILDING AREA = 3,640 SF
 PARKING LOT PAVEMENT = 2,786 SF
 WALL & MISC. = 130 SF
 PATIO AREA = 900 SF
 WALKWAYS & MISC. = 1,145 SF

LOT AREA = 33,302 SF
PRE-EXISTING IMPERVIOUS AREA = 8,601 SF
REMAINING "LAWN" AREAS = 24,701 SF

POST-DEVELOPED COVERAGE:
 BUILDING AREA = 5,500 SF
 PARKING LOT PAVEMENT = 18,320 SF
 WALL & MISC. = 245 SF
 PATIO AREA = 900 SF
 WALKWAYS & MISC. = 834 SF
 DUMPSTER PAD = 204 SF

LOT AREA = 33,302 SF
POST-DEVELOPED IMPERVIOUS AREA = 26,003 SF
REMAINING "LAWN" AREAS = 7,299 SF

NET INCREASE = 17,402 SF

FINAL PERCOLATION AND DEEP TEST PIT DATA:

TEST DATE: TBD
 WEATHER: TBD
 PRE-SOAK TBD
 WITNESS: N/A

DEEP TEST PIT:
 *** CONTRACTOR SHALL PROVIDE DESIGN ENGINEER WITH ADDITIONAL DEEP TEST PIT DATA AT TIME OF CONSTRUCTION.

| PERCOLATION TEST #1 (3 RUNS PERFORMED) | PERCOLATION TEST #2 (3 RUNS PERFORMED) | PERCOLATION TEST #3 (3 RUNS PERFORMED) |
|---|---|---|
| FINAL RUN RESULTS: START TIME: TBD END TIME: TBD | FINAL RUN RESULTS: START TIME: TBD END TIME: TBD | FINAL RUN RESULTS: START TIME: TBD END TIME: TBD |
| START DEPTH FROM SURFACE: 0" END DEPTH FROM SURFACE: 3" RESULT: TBD / 3" DROP | START DEPTH FROM SURFACE: 0" END DEPTH FROM SURFACE: 3" RESULT: TBD / 3" DROP | START DEPTH FROM SURFACE: 0" END DEPTH FROM SURFACE: 3" RESULT: TBD / 3" DROP |

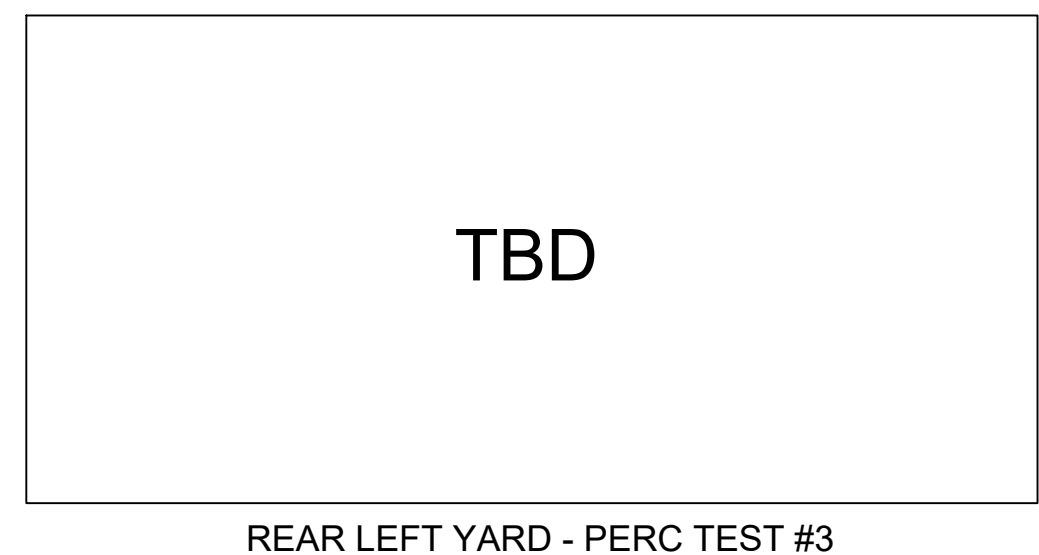
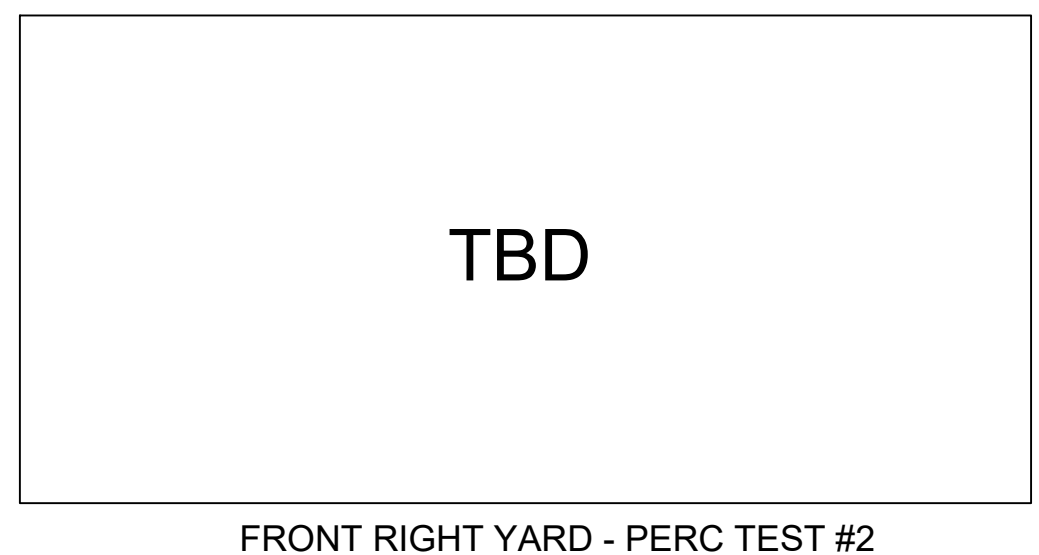
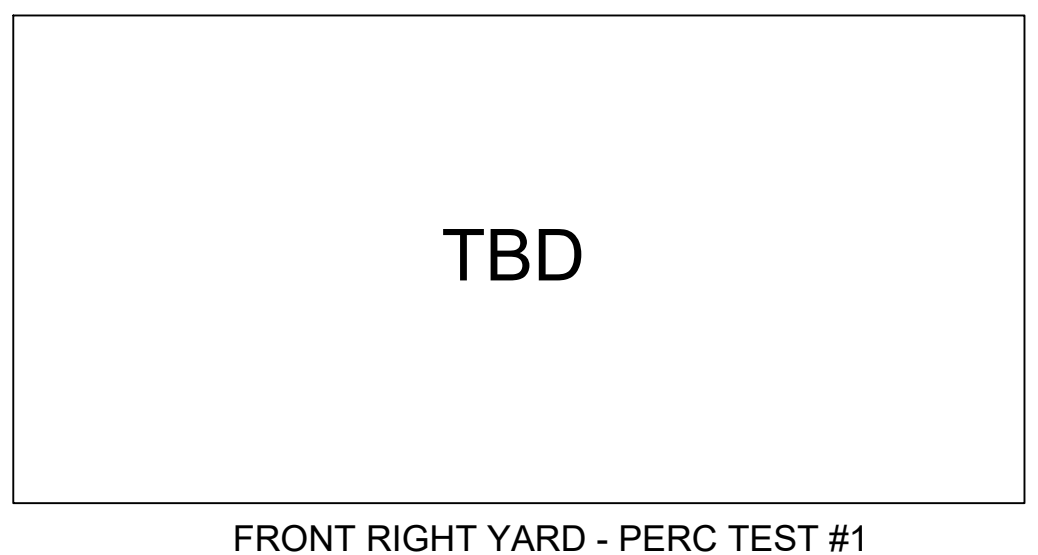
(FOR DESIGN, USE 20 MIN PER 1 INCH DROP IN FRONT YARD)

Constant Slope

| Smooth Wall PVC | GPM with 1% | Flow Velocity (ft/sec) | GPM with 2% | Flow Velocity (ft/sec) | GPM with 3% | Flow Velocity (ft/sec) | GPM with 4% | Flow Velocity (ft/sec) | GPM with 5% | Flow Velocity (ft/sec) |
|-----------------|-------------|------------------------|-------------|------------------------|-------------|------------------------|-------------|------------------------|-------------|------------------------|
| 1/2" | 0.6 | 0.9 | 0.8 | 1.3 | 1 | 1.7 | 1.2 | 2 | 1.4 | 2.2 |
| 3/4" | 1.6 | 1.2 | 2.4 | 1.7 | 3 | 2.2 | 3.5 | 2.5 | 3.9 | 2.9 |
| 1" | 3.5 | 1.4 | 5.1 | 2.1 | 6.4 | 2.6 | 7.4 | 3 | 8.4 | 3.4 |
| 1 1/4" | 6.3 | 1.7 | 9.2 | 2.4 | 11.4 | 3 | 13.4 | 3.5 | 15.1 | 3.9 |
| 1 1/2" | 10.2 | 1.9 | 14.8 | 2.7 | 18.5 | 3.4 | 21.6 | 3.9 | 24.3 | 4.4 |
| 2" | 21.7 | 2.2 | 31.6 | 3.2 | 39 | 4 | 46 | 4.7 | 52 | 5.3 |
| 3" | 63 | 2.9 | 92 | 4.2 | 114 | 5.2 | 133 | 6.1 | 151 | 6.8 |
| * 4" | 135 | 3.4 | 196 | 5 | 244 | 6.2 | 284 | 7.3 | 321 | 8.2 |
| * 6" | 391 | 4.4 | 568 | 6.4 | 707 | 8 | 826 | 9.4 | 932 | 10.6 |

PIPE SIZE ADEQUACY: FOR PROPOSED 4" DIAMETER PVC PIPE SET AT 2% SLOPE, DESIGN FLOW RATE AS PROVIDED BY MANUFACTURER IS 196 GALLONS PER MINUTE. 24 HOUR DESIGN VOLUME IS 276 CUBIC FEET WHICH IS EQUIVALENT 2,065 GALLONS. USING CONVERSION FACTOR, STANDARDIZED PER MINUTE VOLUME IS 1.43 GALLONS PER MINUTE. AS SUCH, THE PROPOSED DISCHARGE ROUTED TO THE DESIGNED CULTEC DRAINAGE SYSTEM ARE SIZED ACCORDINGLY.

PHOTOS - FIELD PERCOLATION TESTING FOR SOILS



STORMWATER DRAINAGE DESIGN FOR 15 OLD ROUTE 22 ARMONK, NY 10504

The proposed storm water modeling utilized is for a net zero increase in site surface runoff. The modeling will capture surface water runoff from the increased impervious surfaces for the new building, paved parking areas, walkways and related. The total net increase of developed impervious surface areas, equating to 17,402 square feet, is modeled using the 24 hour, 100 year design storm of 0.17 inches. Proposed drainage consists of onsite percolation using Cultec Recharger chambers beneath the paved parking areas of the property surrounded by one foot of crushed processed gravel. Water quality pretreatment is proposed with use catch basin "drop in basket" type filters for the 6 proposed catch basins coupled with 1'-6" sumps provided in each of the basins.

| LOT AREA FOR DESIGN: | | | | | POST-DEVELOPMENT - PROPOSED CONDITIONS | | | | |
|--|-------------|------------|-------|--------------|---|-------------|------------|-------|--------------|
| DESCRIPTION | SQUARE FEET | CONVERSION | ACRES | CURVE NUMBER | DESCRIPTION | SQUARE FEET | CONVERSION | ACRES | CURVE NUMBER |
| Total Lot Area | 33,302 | 43,560 | 0.765 | | Total Lot Area | 33,302 | 43,560 | 0.765 | |
| Buildings | 3,640 | 43,560 | 0.084 | 98 | Buildings | 5,500 | 43,560 | 0.126 | 98 |
| Parking Lot | 2,786 | 43,560 | 0.064 | 98 | Parking Lot | 18,320 | 43,560 | 0.421 | 98 |
| Patio, Walls & W/ | 2,175 | 43,560 | 0.050 | 98 | Patio, Walls & W/ | 1,279 | 43,560 | 0.029 | 98 |
| Open Space | 24,701 | 43,560 | 0.567 | 72 | Dumpster Pad | 204 | 43,560 | 0.005 | 98 |
| | | | | | Open Space | 7,299 | 43,560 | 0.169 | 72 |
| COMPOSITE CURVE NUMBER = 78.7 | | | | | COMPOSITE CURVE NUMBER = 93.3 | | | | |
| TOTAL IMPERVIOUS AREAS = 8,686 SF | | | | | TOTAL IMPERVIOUS AREAS = 24,848 SF | | | | |

WATER QUANTITY VOLUME ANALYSIS:

- Reference NYSDEC Stormwater Design Manual Chapter 4 and NRCSS TR-55 Modeling for Urban Hydrology for Small Watersheds
- Design Storm used is 25 year, 24 hour
- Pre-Developed Composite Curve Number (CN)
- Post-Developed Composite Curve Number (CN)
- Rainfall Intensity (i), 100 Year 24 Hr Storm
- Pre-Developed Impervious Area (A)
- Post-Developed Impervious Area (A)

Using the TR-55 SCS Runoff Equation

Max Retention (S) = 1,000(CN) - 10
 Runoff (Q) = (P - 0.25)/(P+0.955)
 Runoff Volume (V) = Q x A

1) Pre-Development Runoff Determination

Pre-Development S = 2,704 Inches
 Pre-Development Q = 6.49 Inches
 Pre-Development V = 4,699.7 Cubic Feet

2) Post-Development Runoff Determination

Post-Development S = 0.834 Inches
 Post-Development Q = 8.21 Inches
 Post-Development V = 16,989.9 Cubic Feet

3) Water Quantity Volume for Storage

Storage Volume = V_{post} - V_{pre}
 New Volume = 12,290.18 Cubic Feet

SOIL PERCOLATION RATE:

a) Area of Percolation (A_c):
 1) Surface Area of Cylinder (A_s) = 32 in
 Perc Hole Depth = 4 inches
 Diameter = 4 inches
 Water Depth (h_w) = 0 inches
 A_c = π D h_w = 0.00 in²
 A_c = 0.00 in²

2) Cylinder Bottom Area
 A_b = π r²
 A_b = 0.007 in²

3) Percolation Area
 A_c + A_b = 0.007 in²
 A_p = 0.007 in²

b) Volume of Percolation (V_p):
 V_p = V_c A_p h
 V_p = 0.007 in³

c) Soil percolation rate (R):
 S = volume / area / time
 S = 0.00994 in³/min
 S = 0.00994 in³/day
 S = 7.89 in³/day

VOLUME PER DRYWELL (V_d):

| Chamber | Stone Volume (CF) | Stone Length (inches) | Stone Width (inches) | Stone Height (inches) | Total Volume (CF) | # Units |
|----------|-------------------|-----------------------|----------------------|-----------------------|-------------------|---------|
| 330 XLHD | 52.27 | 126.00 | 76.00 | 42.50 | 73.30 | 1 |

Total Storage Provided: V_d = 125.57 in³

24-HOUR PERCOLATION VOLUME PER DRYWELL (V_p):

V_p = 624.52 in³

PERCOLATION VOLUME OF DRYWELL (V_d):

V_d = 498.75 in³

TOTAL 24-HOUR VOLUME PER DRYWELL (V_t):

V_t = 1123.27 in³

NUMBER OF DRYWELLS REQUIRED (DWR):

DWR = Total Volume per Drywell (V_t) / Required Volume of Storage (V_d)
 DWR = 19.89 (Round to 20 Units)

WATER QUALITY VOLUME ANALYSIS (WQv & Vt):

Reference NYSDEC Stormwater Design Manual Chapter 4, Sections 4.2 and 4.3

Water Quality Volume (WQv) = 236.78 Cubic Feet
 Total Volume (Vt) of SAMP's Provided = 8,740.48 Cubic Feet

Reference NYSDEC Stormwater Design Manual Chapter 6, Sections 6.2 and 6.3

Water Quality Volume (WQv) = 236.78 Cubic Feet
 48 Hour Perc. Volume of Drywells (V_d) x #Units Proposed = 13,965.00 Cubic Feet

WATER QUALITY VOLUME PRE-TREATMENT ANALYSIS:

Reference NYSDEC Stormwater Design Manual Chapter 6, Section 6.4.3

Camp-Hazen Equation A_s = 1'1"QW^{0.7}(L-E)

A_s = 1.91 Square Feet

A = Sedimentation Basin Surface Area (ft²)
 E = Sedimentation Trap Efficiency (90%)
 W = Particle Settling Velocity (0.0033 FPS)
 Q = Basin Discharge Rate (WQv/24/3600)
 WQv = Water Quality Volume

Calculations determine that twenty Cultec Model 330XLHD chambers are sufficient to handle the design impervious surfaces while managing the design water quality volume (WQv). The proposed system meets NYSDEC design criteria for 48-hour infiltration of WQv. Furthermore the field determined infiltration rates meet the minimum design parameters of 0.5 in/hour. The proposed stormwater management system consists of three sets of chambers surrounded by one foot of 1/4 to 1/2 inch nominal size processed gravel adjacent to the percolation test pit locations. For NYSDEC water quality pre-treatment qualification, all parking lot catch basins will contain 1-1/2 foot minimum depth sumps and each basin will be retrofitted with "drop in basket" type filters.

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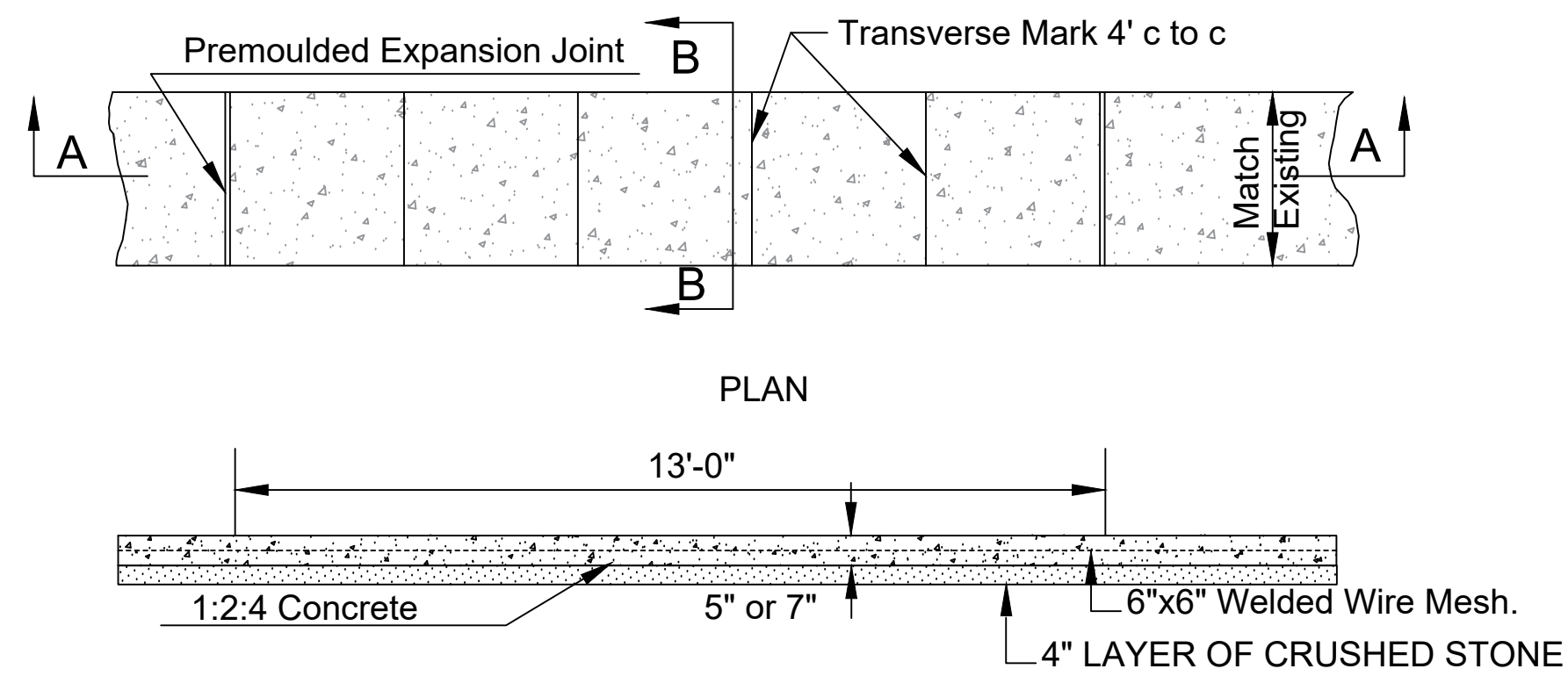
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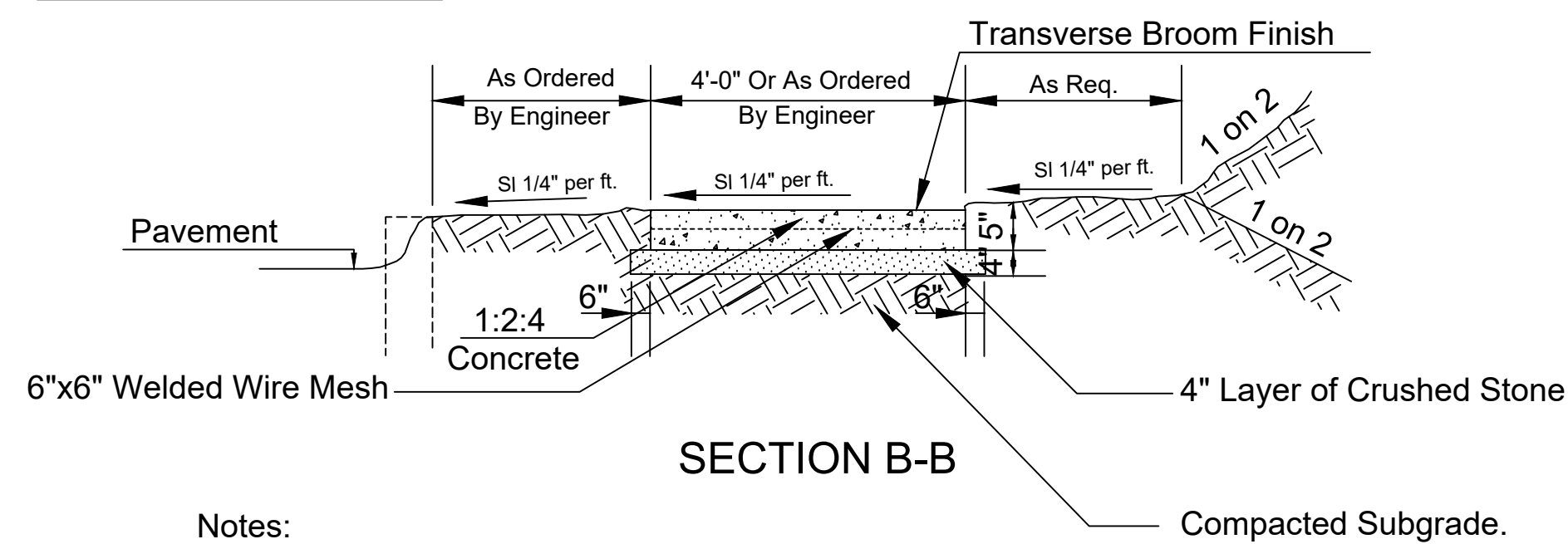
ANY UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING A SEAL OF A LICENSED LAND SURVEYOR OR PROFESSIONAL ENGINEER IS A VIOLATION OF SECTION 7209 OF THE NYS EDUCATION LAW.

STANDARD CONSTRUCTION DETAILS



SECTION A-A

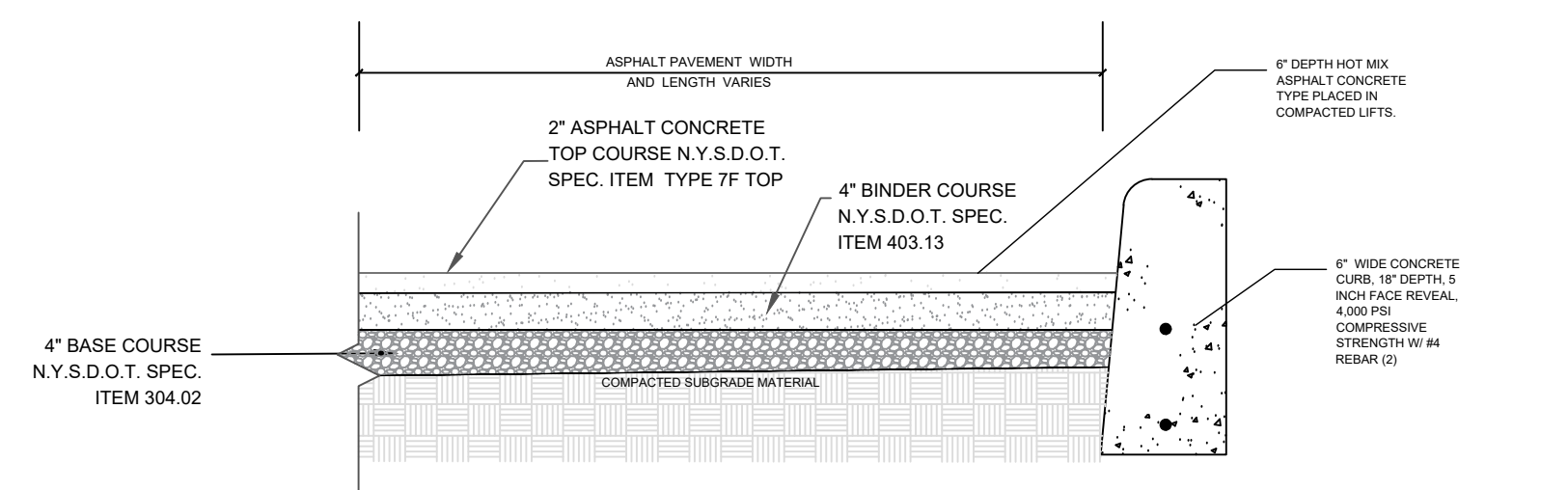
NOTES:
1. NEW 4" LAYER OF CRUSHED STONE UNDER NEW CONCRETE SIDEWALK IS INCLUDED UNDER THIS ITEM.



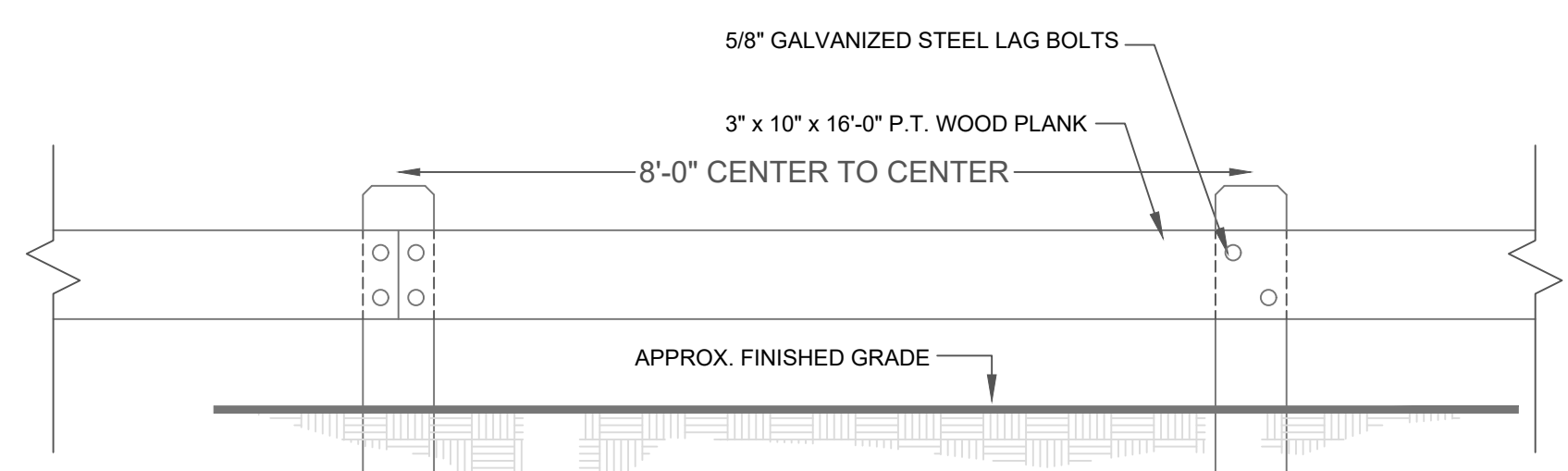
SECTION B-B

- Notes:
1. Concrete shall be NYSDOT Specs Class A Concrete.
 2. Sidewalks Not At Driveways Shall Be 5 inches Thick On a 4 inch Base of crushed stone, With 6"x6" Welded Wire Mesh.
 3. Sidewalks at Driveways Shall Be 7 inches Thick, on a 4 inch Base of crushed stone, With 6"x6" Welded Wire Mesh.

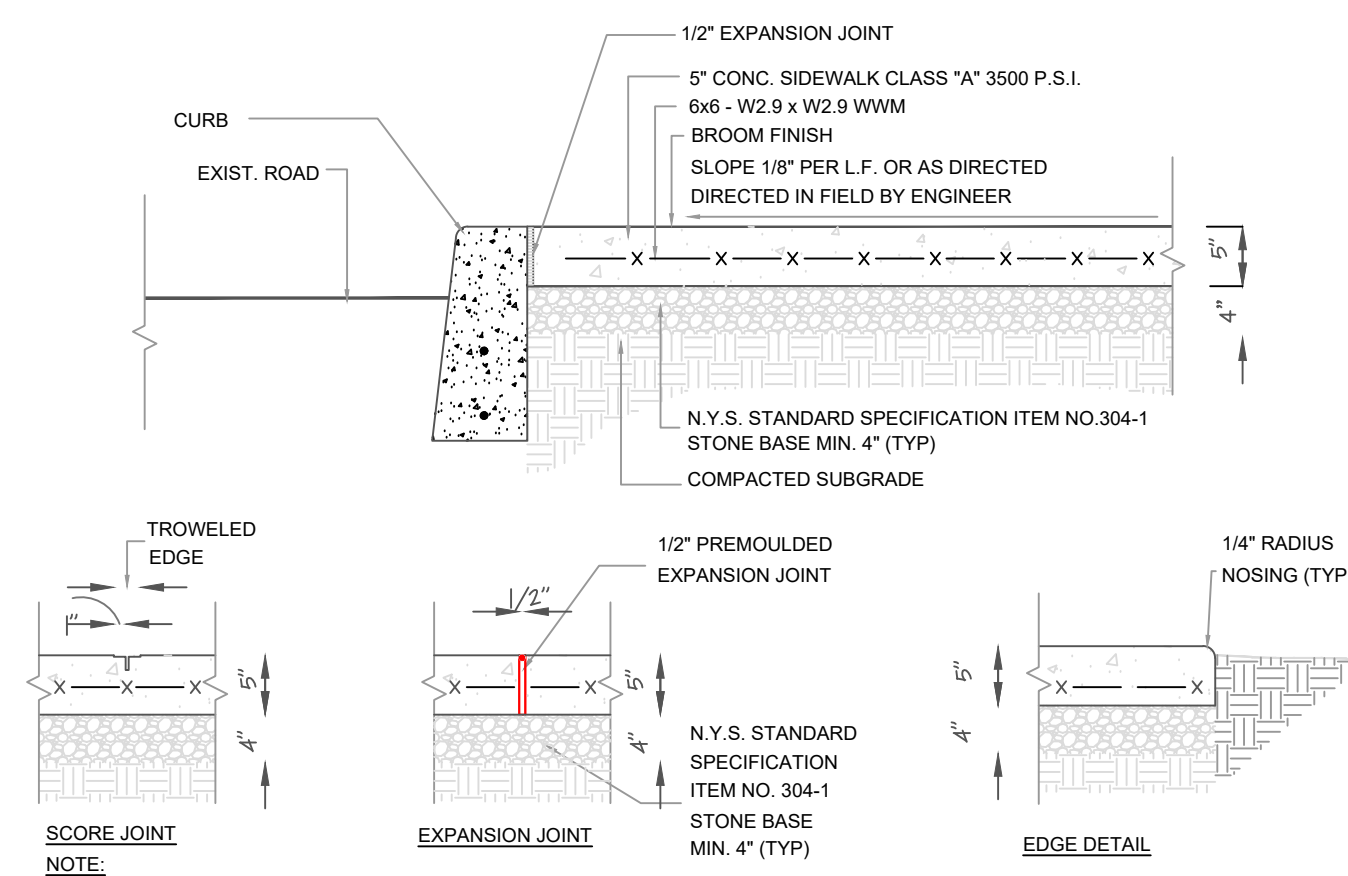
C-1
3 CONCRETE SIDEWALK SECTIONS
SCALE : NOT TO SCALE



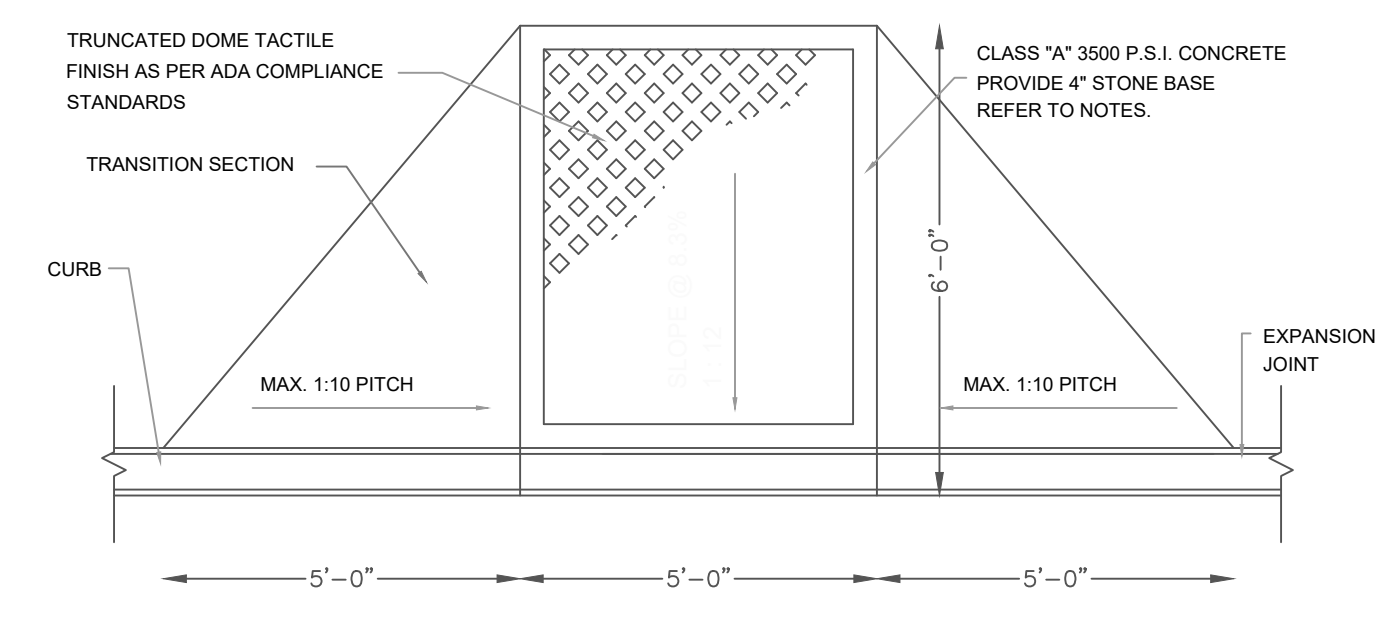
C-6
3 ASPHALT PAVEMENT DETAIL
SCALE : NOT TO SCALE



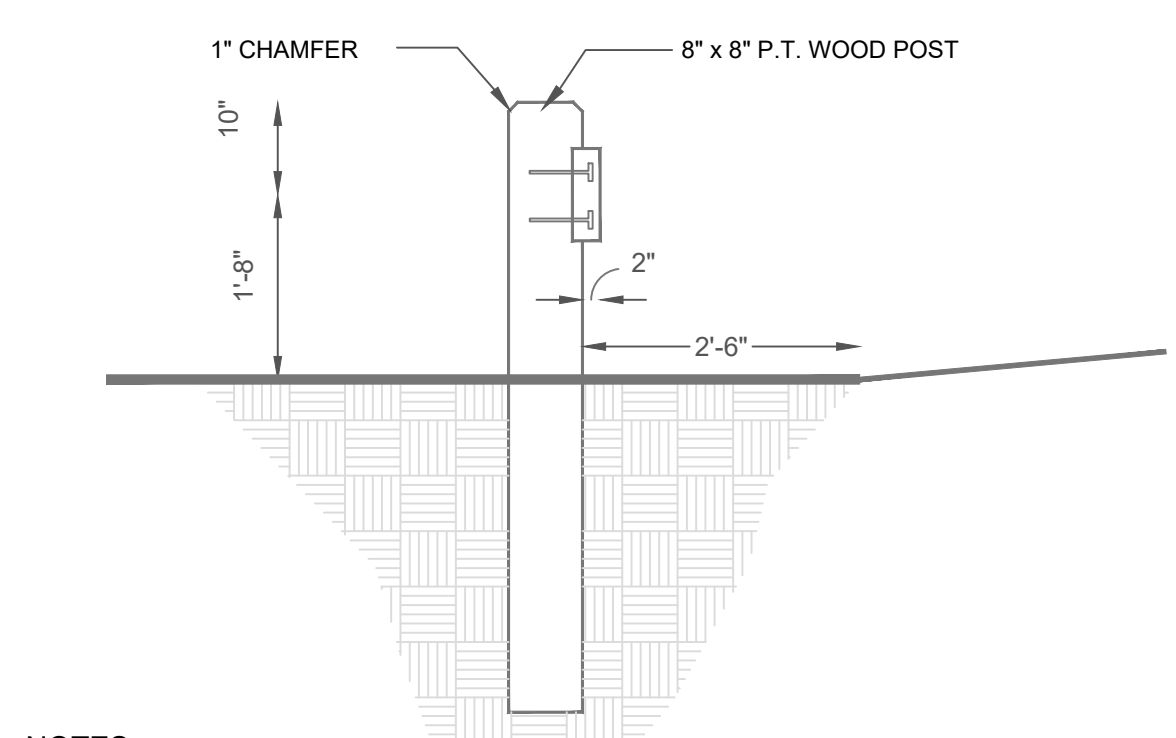
C-7
3 WOOD GUIDE RAIL DETAIL
SCALE : NOT TO SCALE



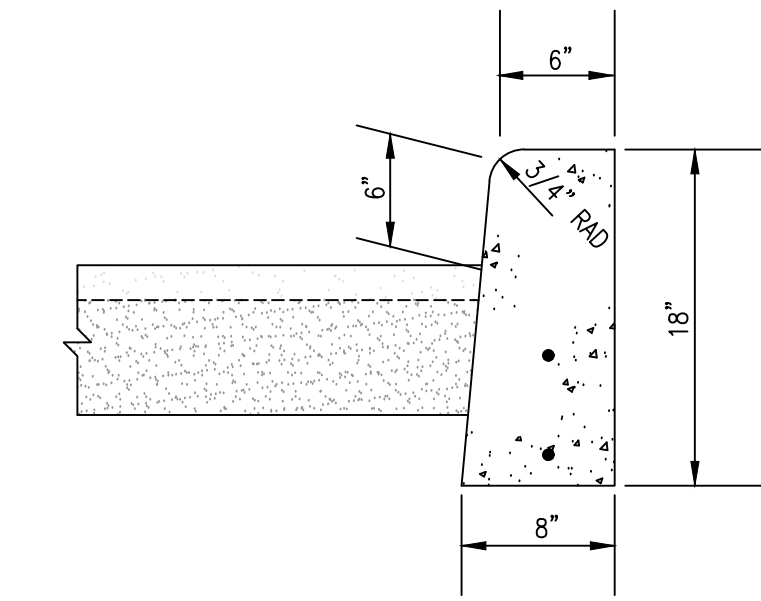
C-2
3 5" REINFORCED CLASS "A" CONCRETE SIDEWALK
SCALE : NOT TO SCALE



C-4
3 PEDESTRIAN RAMP AND DROP CURB DETAIL
SCALE : NOT TO SCALE

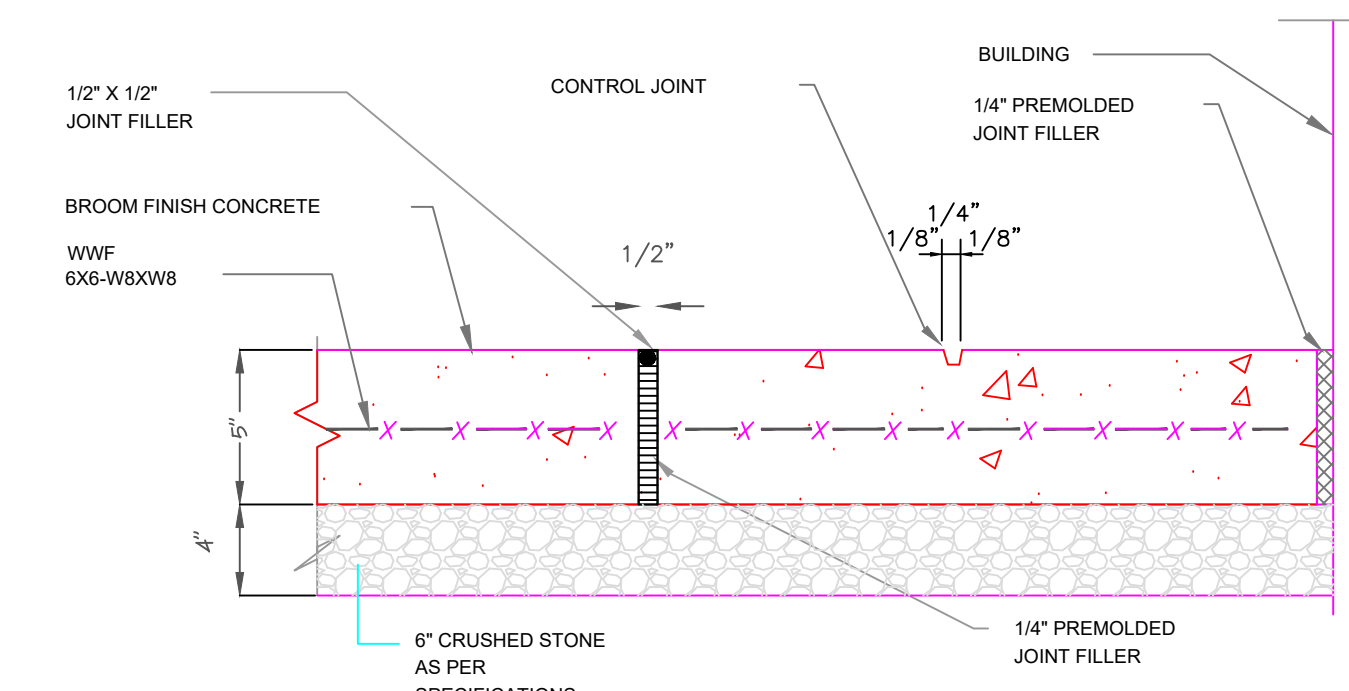


- NOTES:
1. ALL WOOD TO BE SEASONED No. 1 DOUGLAS FIR, SOUTHERN PINE OR OTHER APPROVED STRUCTURAL LUMBER.
 2. ALL WOOD TO BE PRESSURE TREATED.

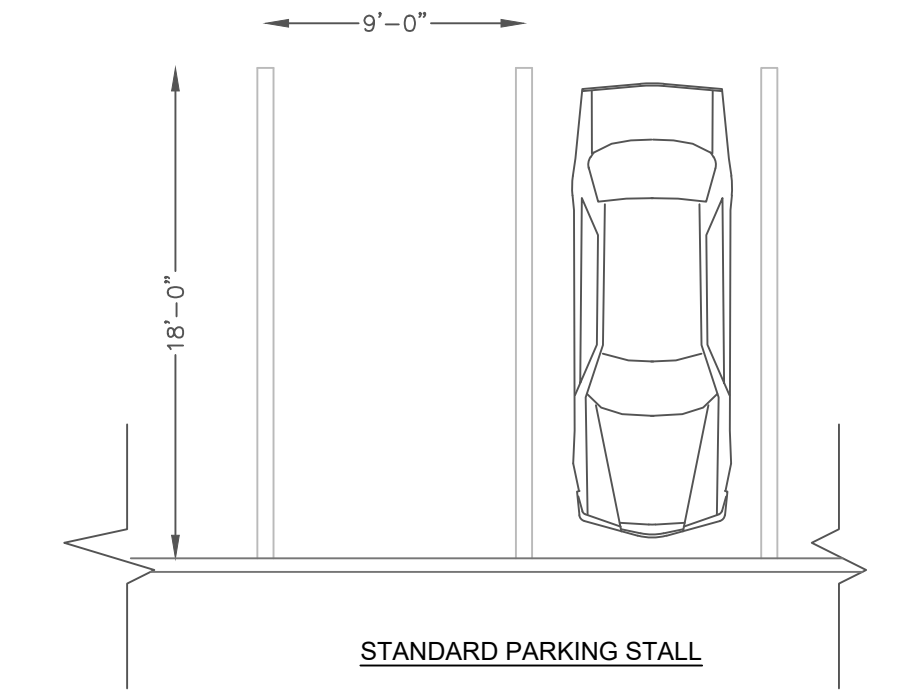


- Note:
1. Concrete Shall Be N.Y.S.D.O.T. Specs. Class "A" Concrete. 4,000 psi comp. strength
 2. Drop Curbs For Driveways Shall Have 1-1/2" Reveal.
 3. Full Height Curb Sections Shall Have a Min. Reveal of 6-inches along municipal road.

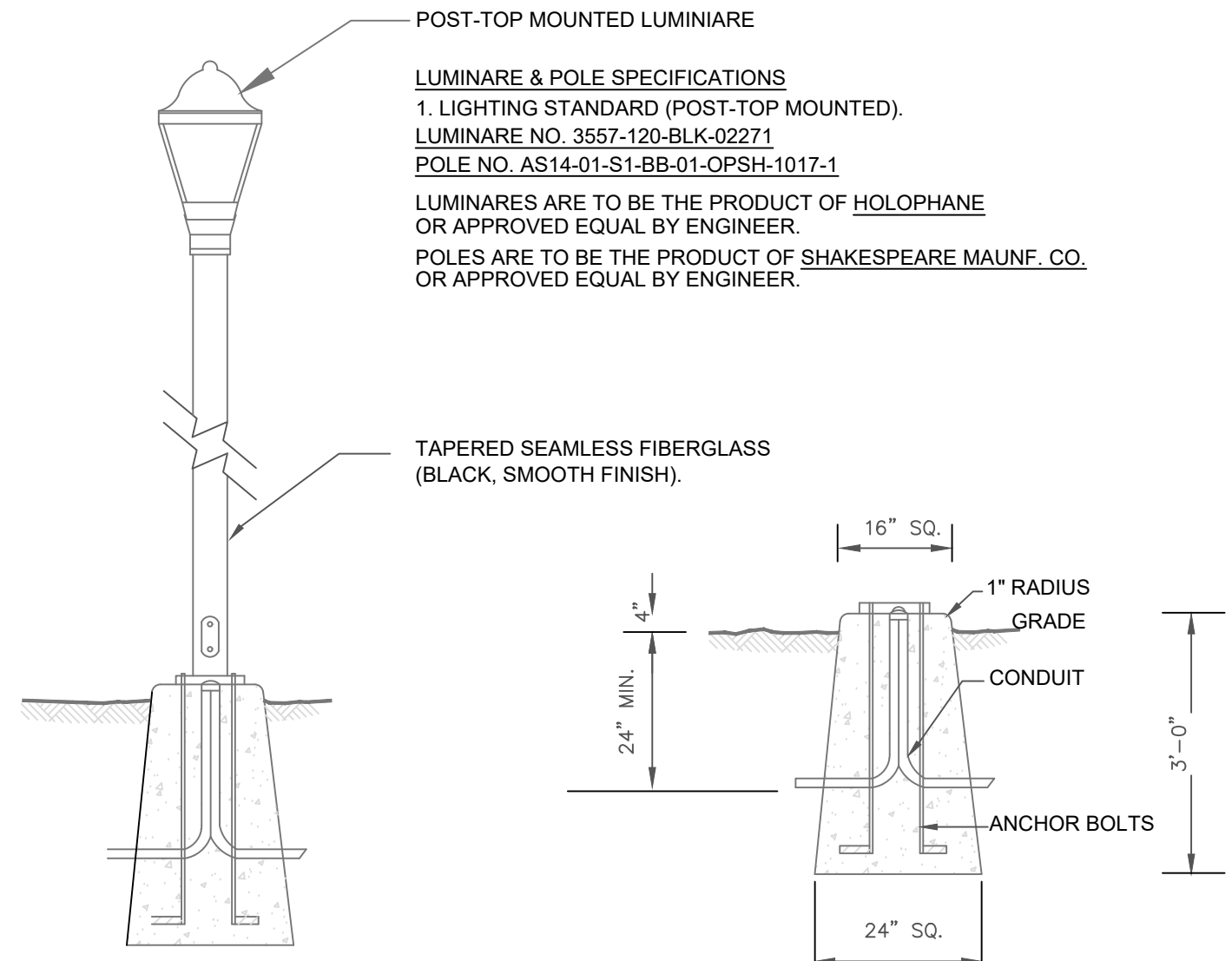
C-3
3 CONCRETE CURB STANDARD SECTION
SCALE : NOT TO SCALE



C-5
3 TYPICAL SIDEWALK SECTION
SCALE : NOT TO SCALE

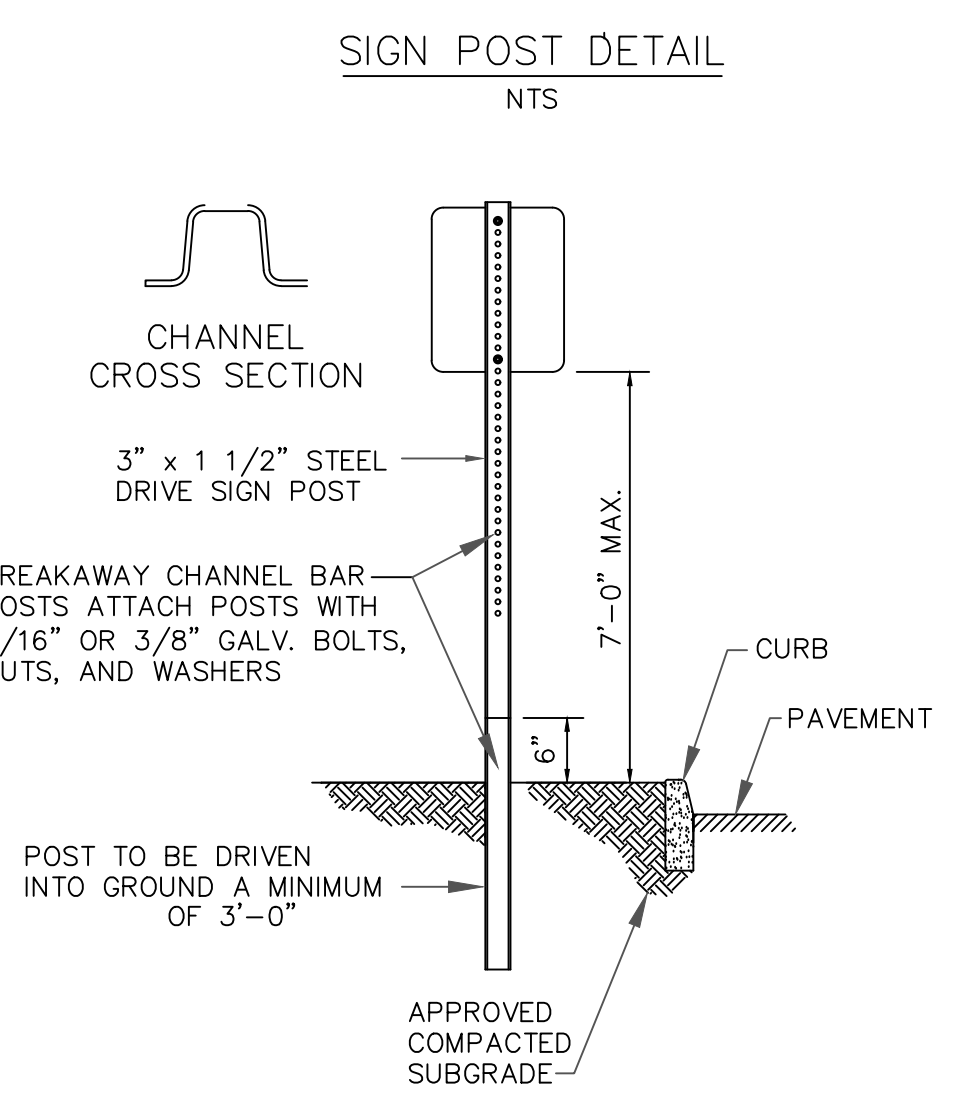


C-10
3 DIMENSIONAL SCHEMATIC OF PROPOSED PARKING STALLS
SCALE : NOT TO SCALE



- NOTES:
1. POLES SHALL BE 14'-0" LENGTH TAPERED SEAMLESS FIBERGLASS WITH HAND HOLE FOR SPLICE AND FUSE HOLDER. POLE IS TO BE ANCHORED TO CONCRETE BASE IN ACCORDANCE WITH MANUF. SPECIFICATIONS.
 2. FACE OF POLE TO BE SET BACK A MINIMUM OF 3'-0" BEHIND EDGE OF ASPHALT PAVEMENT.
 3. LUMINARIES FOR HIGH PRESSURE SODIUM TO BE MANUFACTURED BY HOLOPHANE, (RSL350).
 4. POLE BASES TO BE INSPECTED PRIOR TO INSTALLATION OR BACKFILL.
 5. CONCRETE BASE MUST PROJECT A MINIMUM OF 4" ABOVE FINISHED GRADE.
 6. ALL EXCAVATION FOR LIGHT POST BASES SHALL BE INSPECTED PRIOR TO BASE INSTALLATION.
 7. EACH LIGHT SHOULD BE WIRED SEPARATELY, AND NOT SERIES, AND EACH LAMP SHOULD BE SEPARATELY FUSED.

C-8
3 LIGHTING POLE AND BASE DETAIL
SCALE : NOT TO SCALE



C-9
3 STANDARD SIGN POST DETAIL
SCALE : NOT TO SCALE

DAVID A. GOESSL, PE
CIVIL ENGINEER
622 SPROUT BROOK ROAD
PUTNAM VALLEY, NY 10579 (914) 227-0258

PROPOSED SITE IMPROVEMENTS TO
GAVI RESTAURANT
15 OLD ROUTE 22, ARMONK, NY 10504

PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO
DATE: APRIL 26, 2023 SCALE: NONE SHEET: 6 OF 11

| NO. | REVISION | DATE |
|-----|---|-----------------|
| 1 | ADDED PROPOSED TWO STORY ADDITION AND RAISED DECK FOR GAVI RESTAURANT | July 18, 2023 |
| 2 | REVISED AS PER TOWN REVIEW COMMENTS | August 19, 2023 |
| | | |
| | | |

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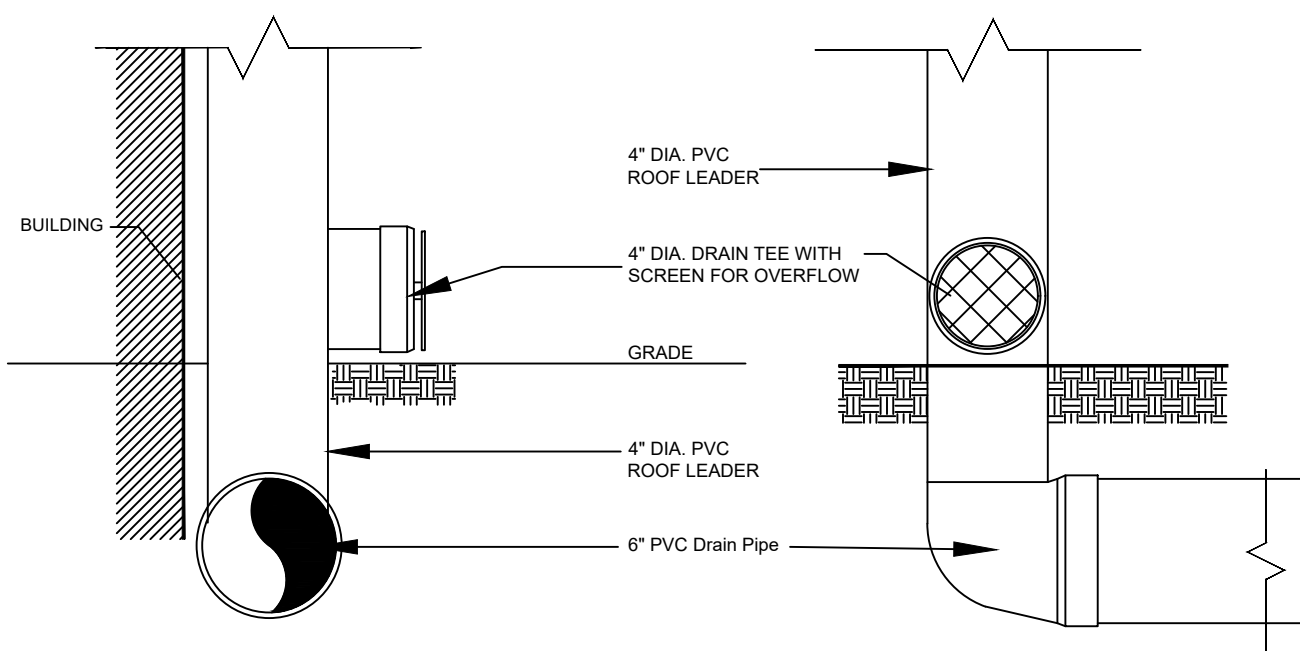
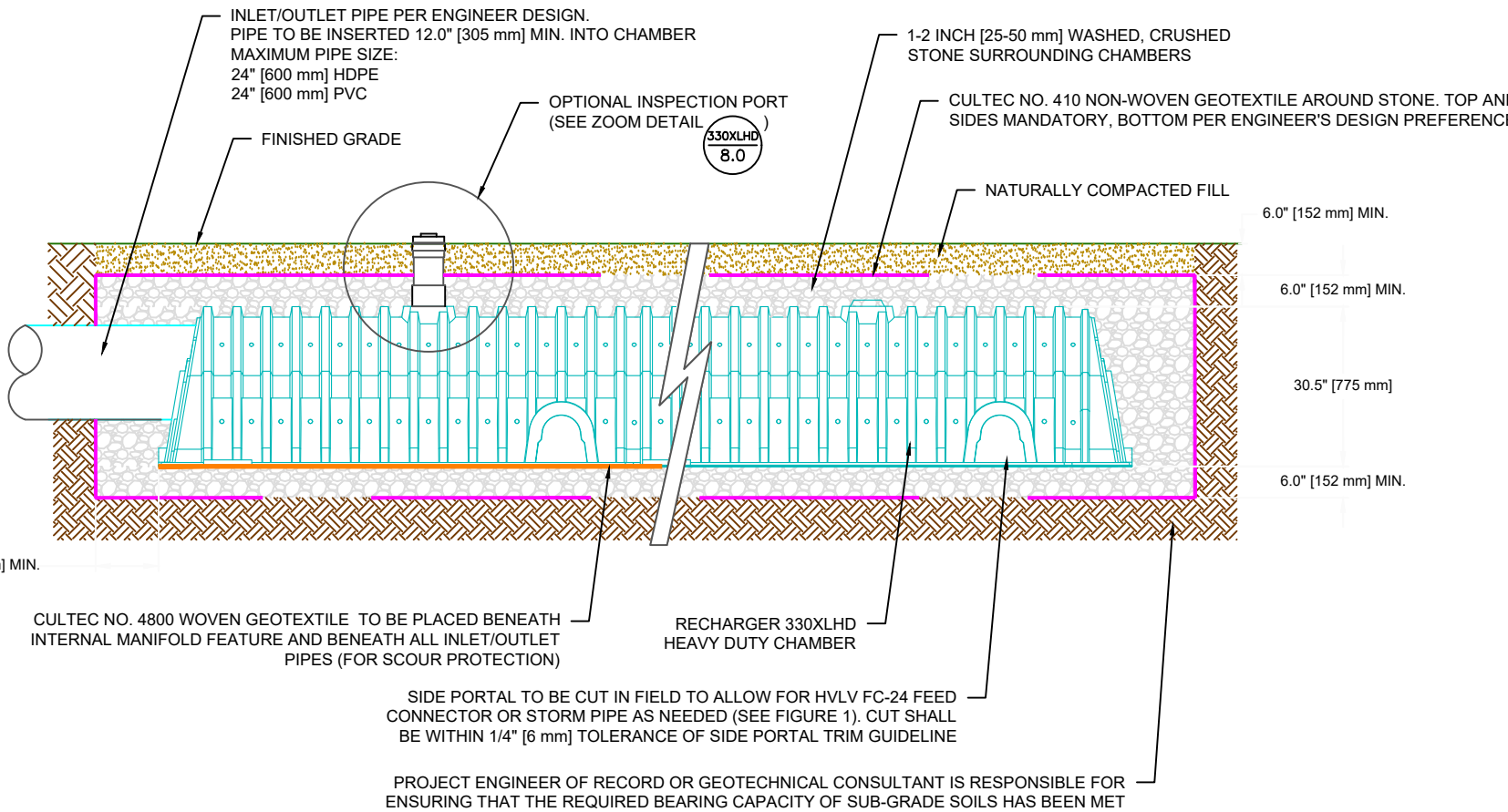
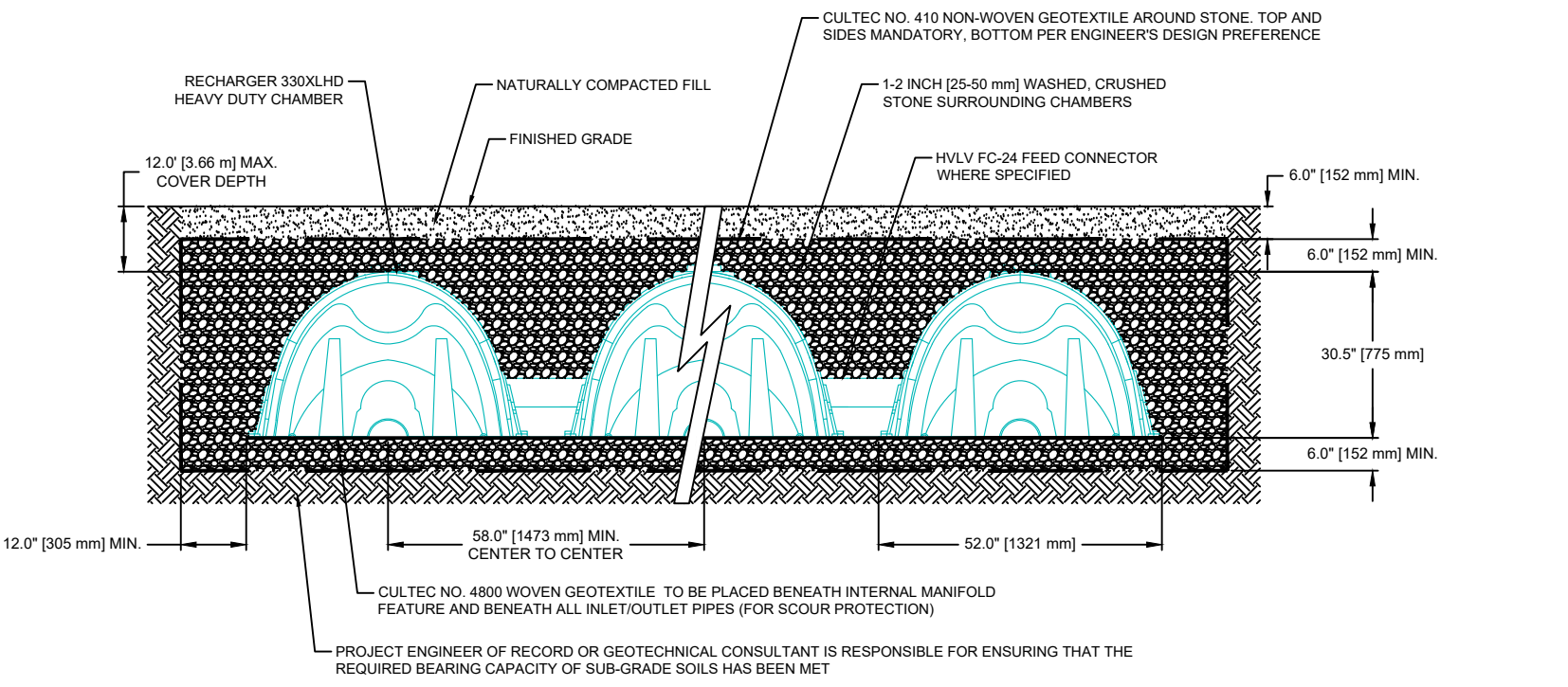
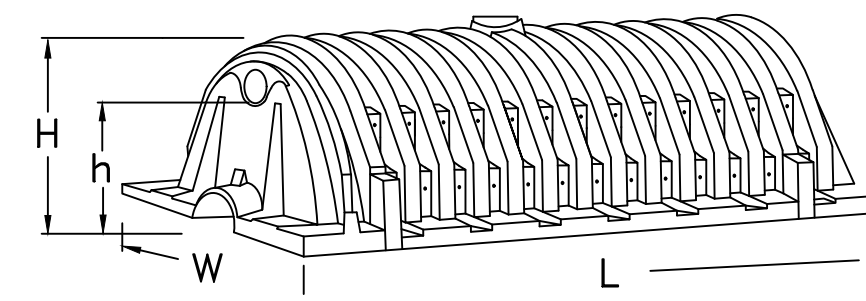


STANDARD DRAINAGE DETAILS

CULTEC 330XLHD INFILTRATING CHAMBERS

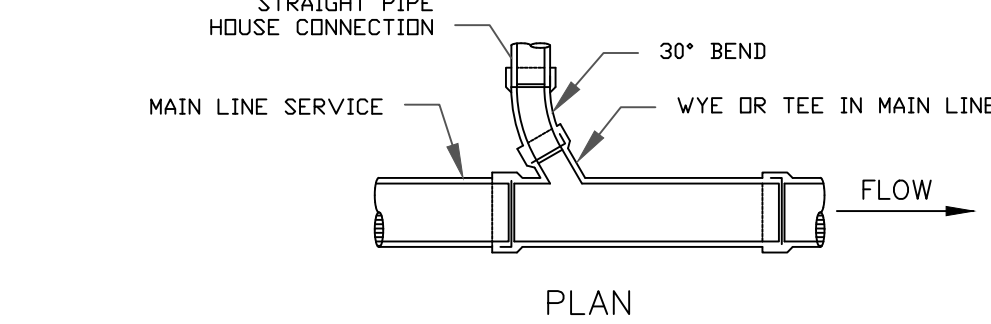
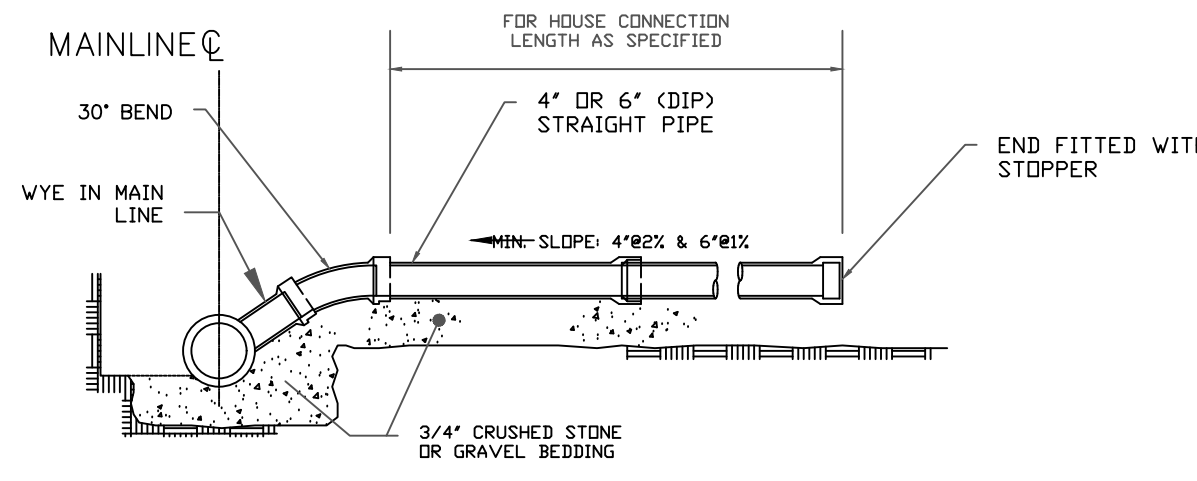
SCALE: NOT TO SCALE

| CHAMBER MODEL | RECHARGER 330XHD |
|--------------------|------------------|
| DIMENSIONS L | 84.0" |
| W | 52.0" |
| H | 30.5" |
| h | 22.0" |
| CAPACITY (gallons) | 391.0 |
| (cubic ft.) | 52.2 |

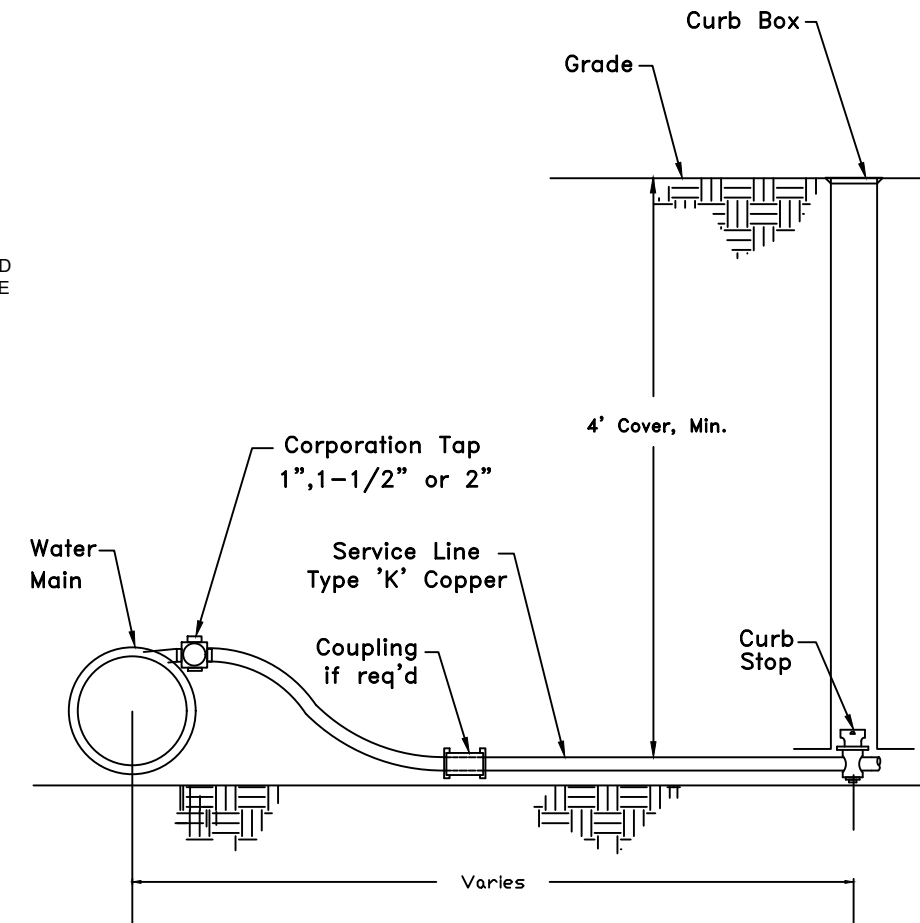


2-DR 2 ROOF LEADER OVERFLOW @ GRADE
SCALE: NOT TO SCALE

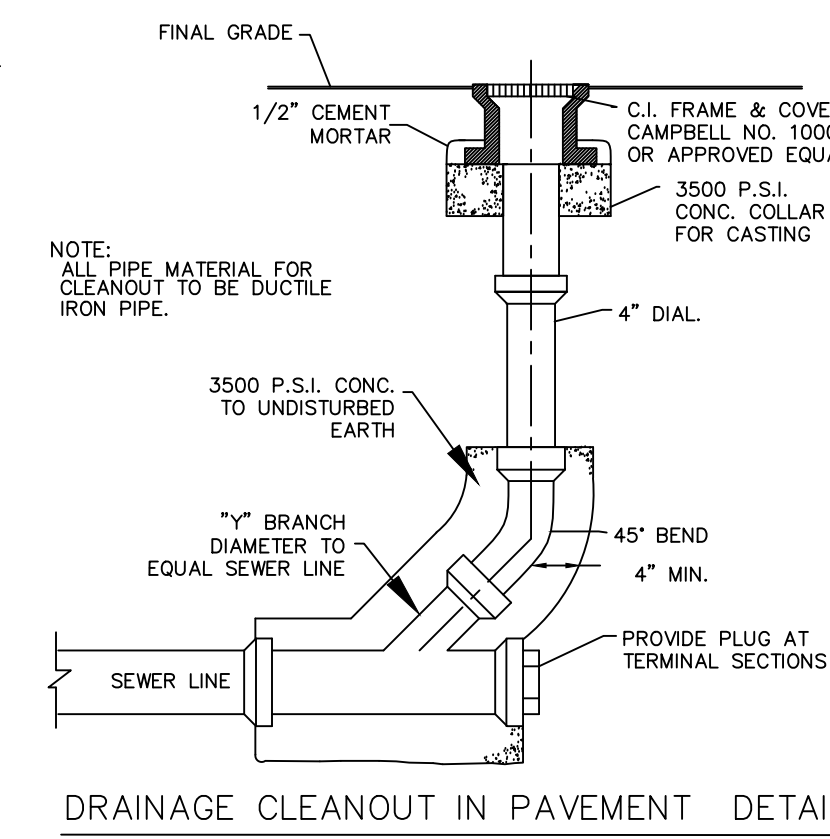
UTILITY DETAILS



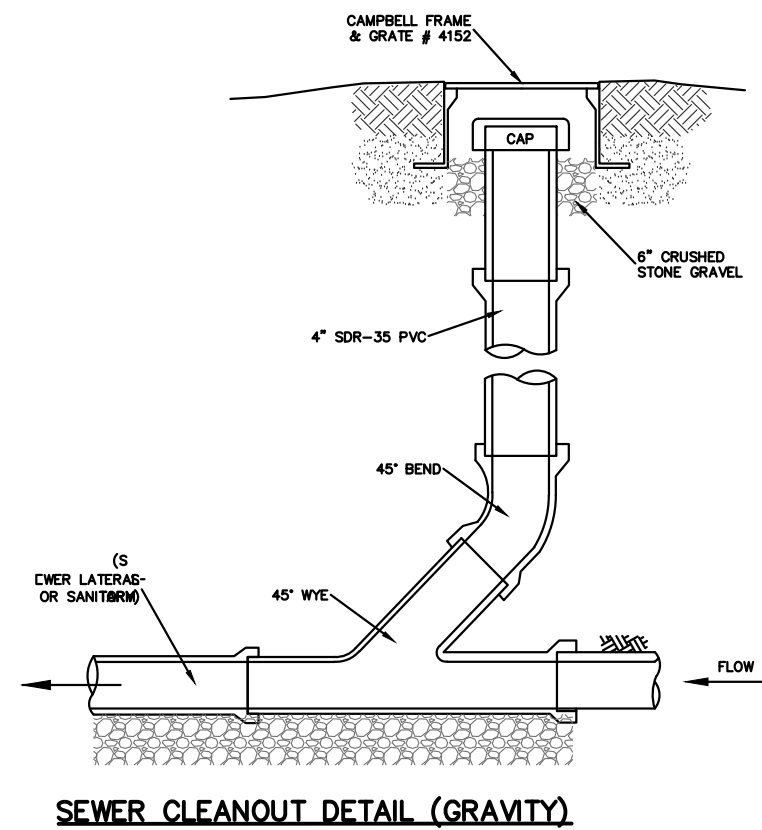
1-U 3 STANDARD DETAILS FOR SANITARY SEWER LATERAL
SCALE: NOT TO SCALE



2-U 3 STANDARD DETAILS FOR DOMESTIC WATER SERVICE
SCALE: NOT TO SCALE



DRAINAGE CLEANOUT IN PAVEMENT DETAIL
NTS

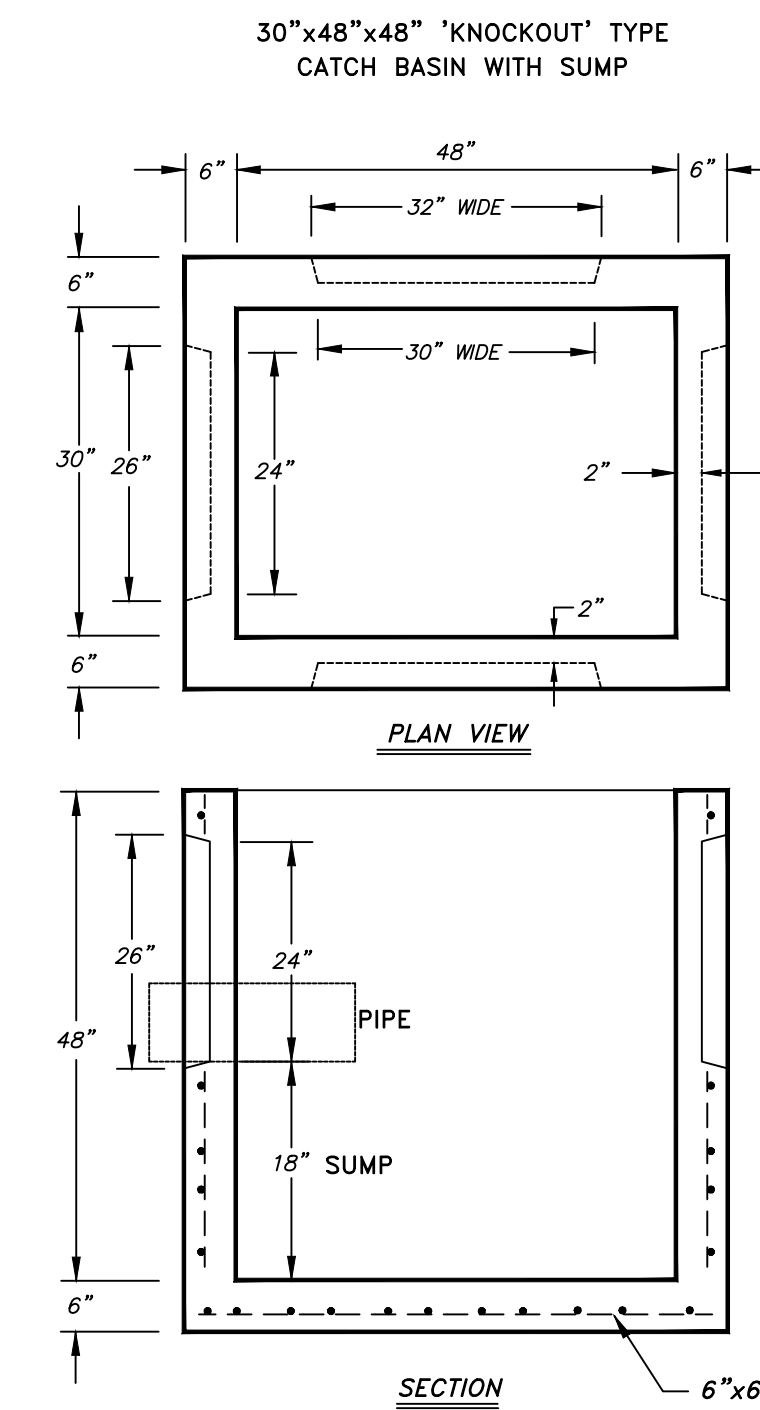


SEWER CLEANOUT DETAIL (GRAVITY)

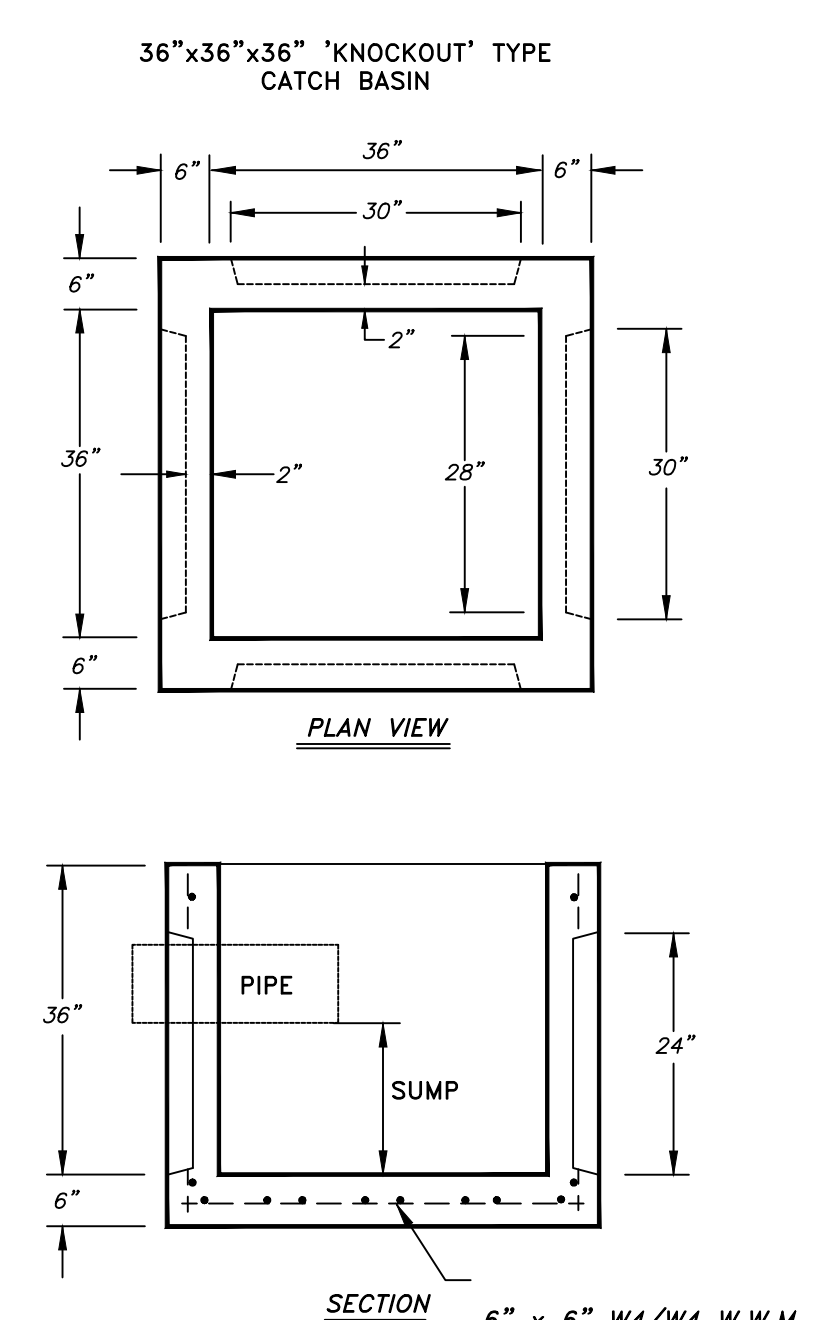
- REFER TO PLAN FOR SPECIFIC PIPE SIZING, SLOPE AND SPECIFICATIONS. SANITARY SEWER LATERAL SHALL BE 4" DIAMETER SDR-35 PVC PIPE ON PRIVATE PROPERTY AND MAY BE SPECIFIED AS EXTRA HEAVY CAST IRON PIPE WITHIN THE ROAD AND RIGHT OF WAY.
- CLEANOUTS SHALL BE PLACED AT EACH SIGNIFICANT PIPE BEND OR CHANGE IN DIRECTION. MAXIMUM SPACE BETWEEN CLEANOUTS IS 50 FEET.
- PIPE SHALL BE BEDDED WITH CLEAN SAND AND COVERED ONE FOOT WITH SAME. BACKFILL IN ROAD AND RIGHT OF WAY WITH K-CRETE MATERIALS AND SELECT FILL IN ALL OTHER AREAS.

NOTES:

- CONTRACTOR SHALL CONFIRM CORPORATION, SERVICE TUBING, CURB STOP AND BOX MATERIALS WITH TOWN OF NORTH CASTLE
- CONTRACTOR PROVIDES ALL EXCAVATION, LABOR, BACKFILL AND RESTORATION.
- THE CURB BOX SHALL BE LOCATED BETWEEN THE EDGE OF PAVEMENT, OR CURB WHERE CURBS ARE IN PLACE, AND THE PROPERTY LINE. WHERE SIDEWALKS EXIST OR ARE TO BE BUILT, THE CURB STOP SHALL BE LOCATED NO FURTHER THAN THREE (3) FEET FROM THE EDGE OF PAVEMENT, OR CURB WHERE CURBS ARE IN PLACE.

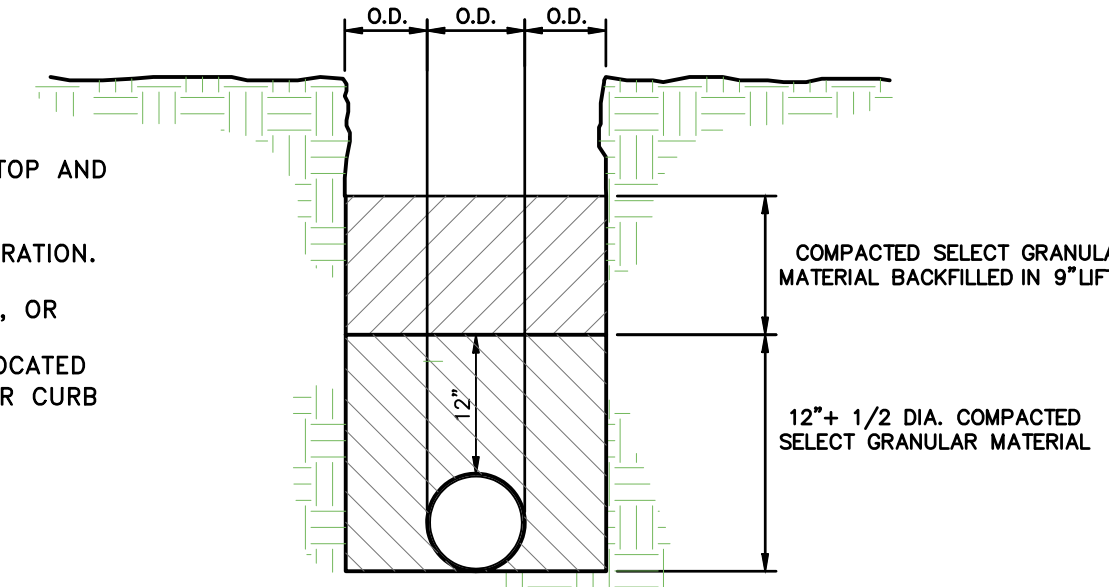


3-DR 3 STANDARD CONCRETE KNOCKOUT CATCH BASINS
SCALE: NOT TO SCALE

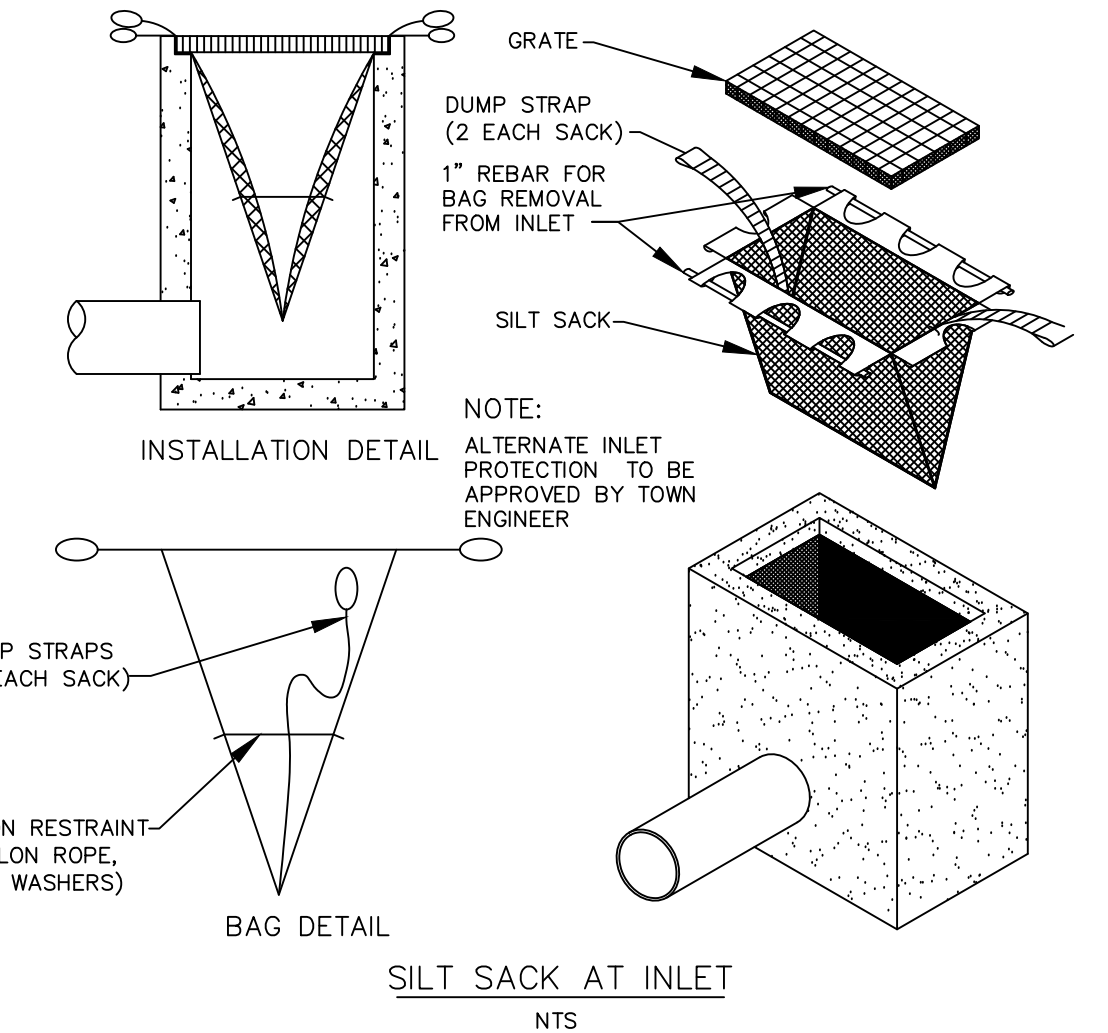


NOTES:
*CONCRETE: 4,000 PSI @ 28 DAYS
*REINFORCING: AS PER ASTM A-185 6" x 6" W4/W4 W.W.M.
*WEIGHTS: CATCH BASIN - 3,360 LBS.

Precast Concrete Sales Co.
123 Route 303 Valley Cottage, N.Y. 10989
Tel. (845) 268-4949 - Fax (845) 268-4376

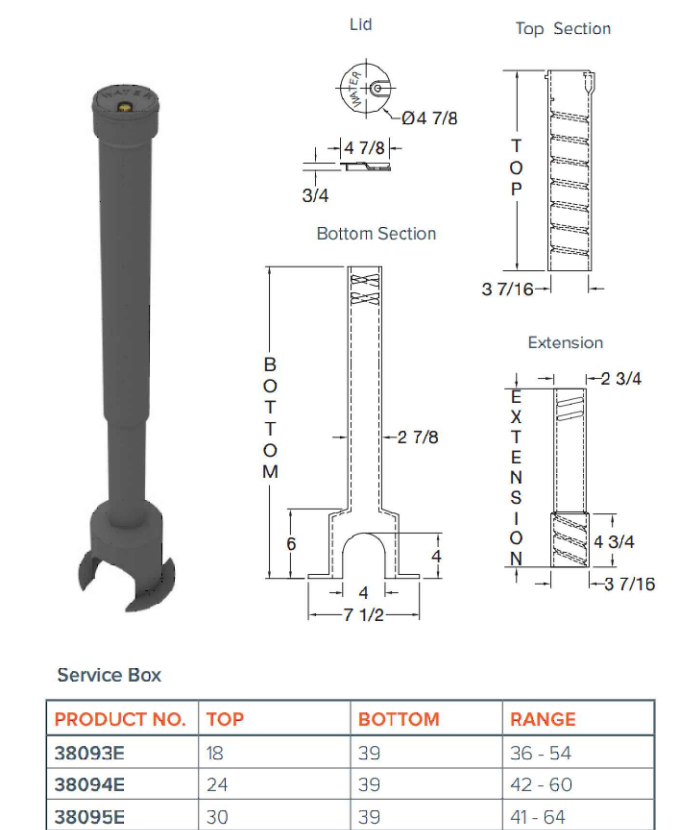


4-DR 2 TRENCH BEDDING DETAIL
SCALE: NOT TO SCALE



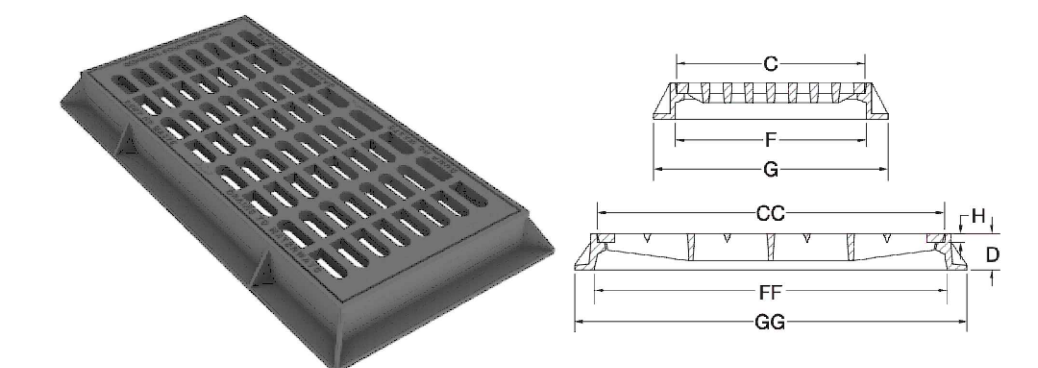
5-DR 3 STANDARD CATCH BASIN SILT TRAP PROTECTION
SCALE: NOT TO SCALE

GENERAL FOUNDRIES



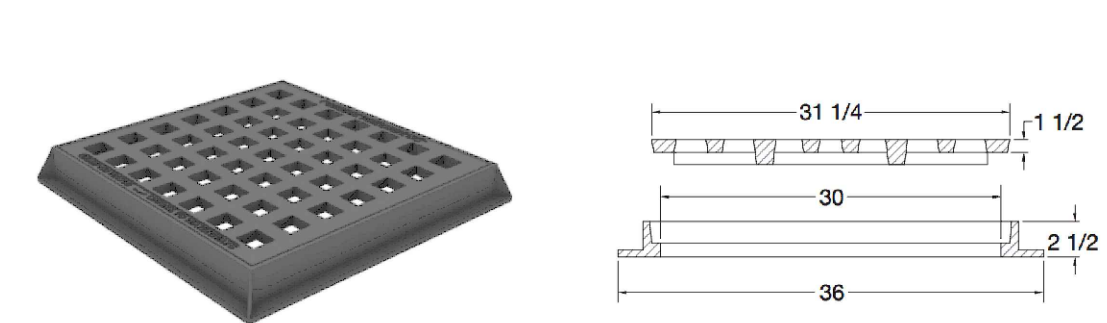
| PRODUCT NO. | TOP | BOTTOM | RANGE |
|-------------|-----|--------|-------|
| 38093E | 18 | 39 | 36-54 |
| 38094E | 24 | 39 | 42-60 |
| 38095E | 30 | 39 | 48-64 |

GENERAL FOUNDRIES



| PRODUCT NO. | C | CC | D | F | FF | G | GG | H |
|-------------|--------|--------|---|--------|--------|----|--------|-------|
| 23404 | 20-1/2 | 34-1/8 | 4 | 22 | 32-3/4 | 28 | 41-1/4 | 1-1/4 |
| 23405 | 21-3/4 | 47-3/4 | 5 | 22 | 48 | 28 | 54 | 1-1/4 |
| 23406 | 21-3/4 | 35-3/4 | 5 | 22 | 36 | 28 | 42 | 1-1/4 |
| 23408 | 30 | 49-1/4 | 5 | 30-1/4 | 49-1/2 | 36 | 55-1/2 | 1-1/4 |
| 23444 | 25-3/4 | 47-3/4 | 5 | 26 | 48 | 32 | 54 | 1-1/4 |
| 23449 | 25-3/4 | 47-3/4 | 9 | 26 | 48 | 34 | 56 | 1-1/4 |

GENERAL FOUNDRIES



| PRODUCT NO. |
|-------------|
| 23134 |

NOTES:
- Dimensions are approximate & in inches
- Gray Iron, Class 350
- Conforms to ASTM A48 / A48M-03 specifications

STANDARD CAST IRON FRAME AND GRATE ASSEMBLIES

5-DR 3 SCALE: NOT TO SCALE

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STANDARD CAST IRON WATER SERVICE CURB STOP ASSEMBLY

3-U 3 SCALE: NOT TO SCALE

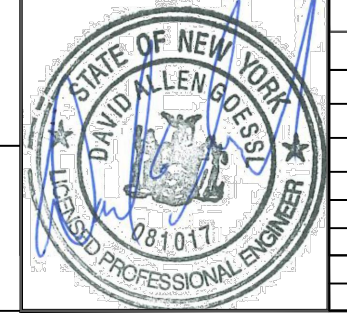
DAVID A. GOESSL, PE
CIVIL ENGINEER
622 SPROUT BROOK ROAD
PUTNAM VALLEY, NY 10579 (914) 227-0258

PROPOSED SITE IMPROVEMENTS TO
GAVI RESTAURANT
15 OLD ROUTE 22, ARMONK, NY 10504

PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO

DATE: APRIL 26, 2023 SCALE: NONE SHEET: 7 OF 11

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STANDARD REDI-ROCK CONSTRUCTION DETAILS

STEP FOOTING DETAILS

PROFILE VIEW - CRUSHED STONE FOOTING
 (No Scale)

PROFILE VIEW - CONCRETE FOOTING
 (No Scale)

Labels: MIDDLE BLOCK, BOTTOM BLOCK, FOOTING DEPTH, d, CRUSHED STONE FOOTING, 1 ON 1 OR FLATTER, BOTTOM HALF BLOCK, CONCRETE FOOTING, 2" GAP (CONSTRUCTION TOLERANCE), BOTTOM HALF BLOCK.

DATE: 06-22-2015
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 6 Step Footing Details 062215.dwg
REDI-ROCK

Typical Gravity Wall Section

Labels: Top block, Grade to drain surface water away from wall, RETAINED SOIL, Non-woven geotextile fabric, Drainstone (AASHTO No. 57 or equivalent), Fill wedge between adjacent blocks, Middle block, Solid bottom block, Drain, Leveling pad.

DATE: 17MAR2016
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 1 Typical Gravity Wall Detail 031716.dwg
REDI-ROCK

Typical Gravity Wall Section with Freestanding Hollow Core Coping

Labels: Cap block cast with Flanchora, F-HC block, Cast-in-place concrete and reinforcing steel, Hook engaged with lifting insert of retaining block, PC retaining block, Infill stone, Non-woven geotextile fabric, Backfill, Middle block, Solid bottom block, Drain, Leveling pad.

DATE: 31MAY2018
 DRAWN BY: NWL
 CHECKED BY: JRJ
 PROJECT: 1 Typical Gravity Wall with F-HC Section.dwg
REDI-ROCK

LEVELING PAD OPTIONS FOR RETAINING WALL BLOCKS

Labels: AASHTO NO. 57 STONE, PERFORATED DRAIN, OPEN-GRADED CRUSHED STONE LEVELING PAD, CONCRETE OR DENSE GRAVEL LEVELING PAD.

DATE: 06-22-2015
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 3 Leveling Pad Options 062215.dwg
REDI-ROCK

BLOCK-TO-BLOCK SETBACK OPTIONS

Labels: Five degree (5°) setback, One degree (1°) setback, Zero (0°) setback.

DATE: 06-22-2015
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 4 Block Setback Options Normal Batter 062215.dwg
REDI-ROCK

90° Outside Corner

Labels: Isometric View of Corner, Top View of Bottom Two Rows.

DATE: 17MAR2016
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 1 90deg Outside Corner Detail-Corner Block 031716.dwg
REDI-ROCK

Wall Drain Weep Hole Options

Labels: Solid PVC or HDPE drain pipe cast into block, Custom Pipe Cast into Block, Field Installed Pipe.

DATE: 06-22-2015
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 5 Drainage Weep Options 062215.dwg
REDI-ROCK

Fence or Pedestrian Guard Connection Locations

Labels: Front View, Side View, Top View.

DATE: 06-22-2015
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 5 Fence or Pedestrian Guard Connection Locations 062215.dwg
REDI-ROCK

Fence or Pedestrian Guard Connection Options

Labels: Grouted Connection (1 Block), Grouted Connection (2 Blocks), Flange Base Plate Connection, Moment Slab Connection.

DATE: 22MAR2016
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 5 Fence or Pedestrian Guard Connection Options 062215.dwg
REDI-ROCK

Sample Plan and Profile Gravity Wall

Labels: LEGEND, PROFILE.

DATE: 22MAR2016
 DRAWN BY: JRJ
 CHECKED BY: JRJ
 PROJECT: 2 Sample Plan and Profile Gravity Wall 032216.dwg
REDI-ROCK

GENERAL CONDITIONS:

- The applicant/contractor shall consult with a licensed professional civil engineer to verify field and site soil conditions prior to the construction of the proposed Redi-Rock retaining wall system.
- No soils or geotechnical information was available at the time that these design drawings were prepared. The design engineer does not make any representation to the quality of existing materials on the property.
- The foundation soils at the base of the wall shall be inspected by the licensed engineer. Any organic or unsuitable soils or improperly compacted embankment materials shall be removed and replaced with materials capable of providing proper bearing capacity.
- The applicant/contractor shall report any groundwater or surface runoff conditions that may adversely affect the wall as additional provisions may be required in the field as determined by the licensed engineer.
- The applicant/contractor shall only use suitable soil and gravel materials. Where materials are imported to the project location, the applicant/contractor shall provide supplier material certifications to demonstrate acceptability. Use of processed/recycled materials may be considered for use.
- The contractor shall establish and maintain standards for quality control to ensure that the wall construction complies with design plans and manufacturer's specifications.
- The contractor consult with the design engineer and demonstrate the establishment of all lines, grades and slopes for compliance with the approved plans.

SPECIFIC CONDITIONS:

- The work to be done includes sourcing, providing and installing Redi-Rock concrete modular gravity retaining wall units to the lines and grades as specified on the design plans in keeping with manufacturer's specifications.
 - The work includes the demolition and proper disposal of all pre-existing materials including timber walls, tree removals, organic soils and brush materials.
 - The work shall include furnishing and installing all related construction materials required for the installation of the Redi-Rock retaining wall system.
 - The work includes all final restoration and cleanup. As the project progresses, the applicant/contractor shall schedule all necessary inspections with the local building officials and design engineer.
- MATERIALS:**
- The wall specified is Redi-Rock gravity wall types of units as specified on the design plans. The wall units shall have a minimum 28-day compressive strength of 4,000 p.s.i. Standard weight concrete shall have 4.5% to 7.5% air entrainment by volume. Density of concrete shall be 145 lb/cf.
 - Units shall be furnished and delivered free of stains, defects, cracks or chips. Units that contain visible defects such as, but not limited to cracks, seams, staining, form marks, color streaks or other defects shall be repaired to the satisfaction of the owner and/or design engineer or shall be removed and replaced at the contractor's and or supplier's expense.
 - The finish texture and color shall be specified by the owner prior to procuring any Redi-Rock wall materials.

FOUNDATION SOILS:

- The soil immediately beneath the retaining wall units and gravel base shall be suitable materials having soils bearing capacity capable of handling the bearing weight of the proposed wall. Unsuitable soils shall be removed and replaced with acceptable materials. Over-excavated areas shall be backfilled and brought to design grade with approved, compacted backfill materials.
- Backfill Soils: The soils used for retaining wall backfill beyond the limits of drainage aggregate shall be free of debris or organic matter and meet the characteristics of NYSDOT designation of "select fill".
- Aggregate Gravels: The gravels for leveling pad shall be a clean crushed stone or processed stone of gradation size 3/8" to 2" free of sands and/or fines. The contractor shall submit supplier material certifications to the owner for review and approval. River rock, broken shale, sands or pea gravel materials are not acceptable for use.

QUALITY CONTROL:

- The contractor shall confirm suitable compacted foundation soils for which a gravel leveling foundation pad of minimum 6" depth may be placed.
- Compaction of foundation soils, gravel leveling pad and backfill materials shall meet or exceed compactive effort of 95% standard proctor density.
- Compacted lifts of no greater than 8" depths are to be installed and tamped with a vibratory plate compactor, jumping jack or other suitable equipment.
- Each course of block wall shall be checked for level and proper alignment. The contractor shall remove and reset materials as necessary to meet manufacturer's design standards and tolerances. Units shall be installed level with a 5 degree batter on the face of wall.
- Should any unforeseen field condition arise to prevent proper installation of the wall, the contractor shall report such matter to the owner and design engineer.

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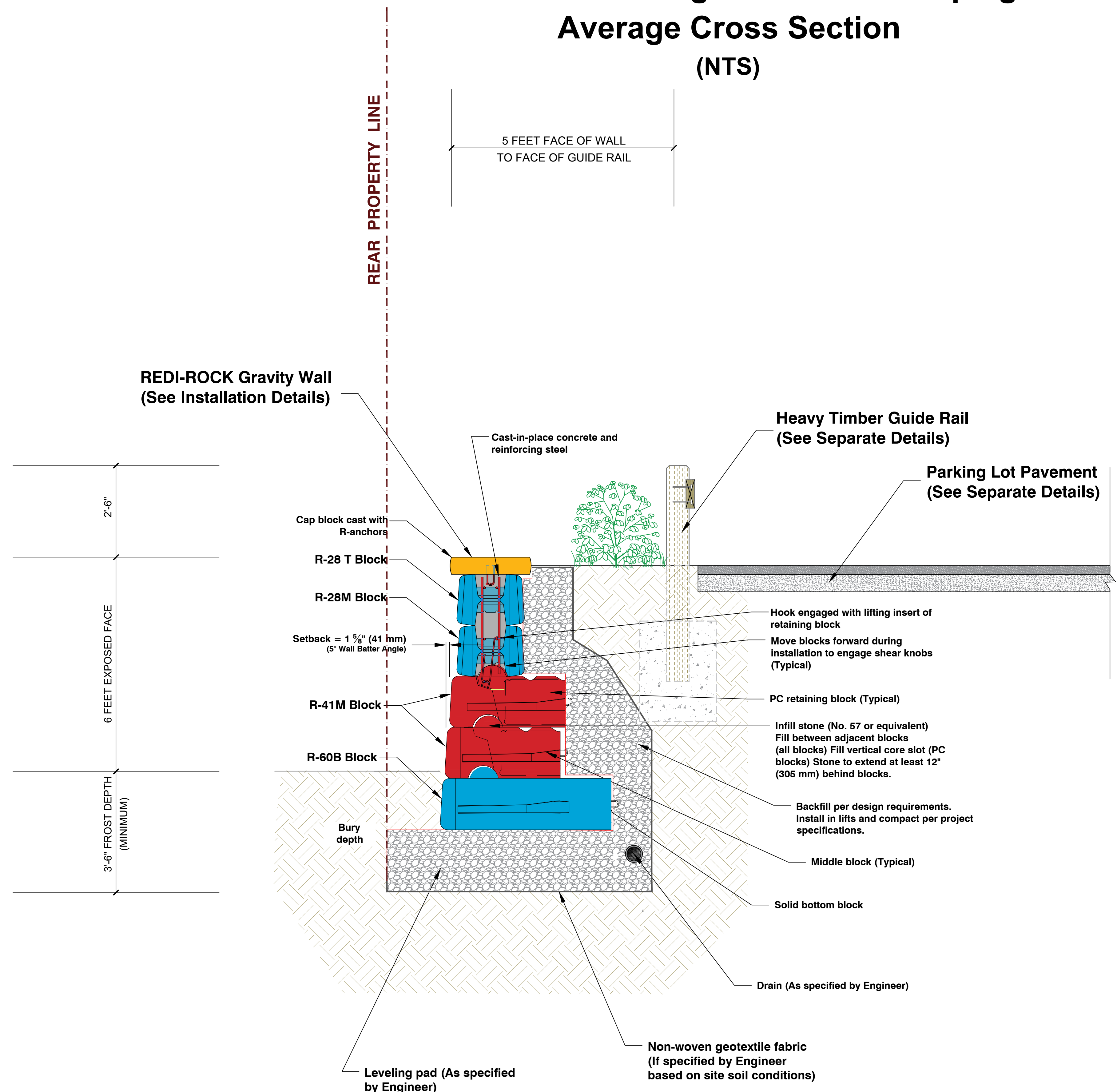
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| 2 | REVISED SW FOR TOWN REVIEW COMMENTS | August 19, 2023 |



Know what's below.
 Call before you dig.
 1-(800) 962-7962



Single Tier Redi-Rock Gravity Wall Section with Freestanding Hollow Core Coping Average Cross Section (NTS)



DESIGN PARAMETERS

All soils are considered as cohesionless for at rest pressure analysis.

Soil parameters

Sandy Silt
 Unit weight : $\gamma = 118.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 30.00^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 125.0$ pcf

Well graded gravel (GW), medium dense
 Unit weight : $\gamma = 133.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 38.50^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 133.0$ pcf

Silty sand (SM)
 Unit weight : $\gamma = 115.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 29.00^\circ$
 Cohesion of soil : $c_{ef} = 100.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 115.0$ pcf

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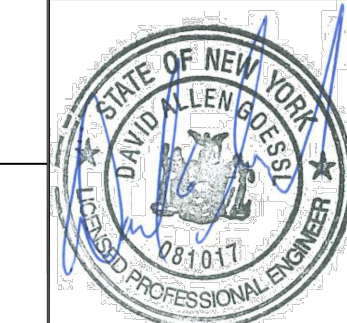
811
 Know what's below.
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DAVID A. GOESSL, PE
CIVIL ENGINEER
 622 SPROUT BROOK ROAD
 PUTNAM VALLEY, NY 10579 (914) 227-0258

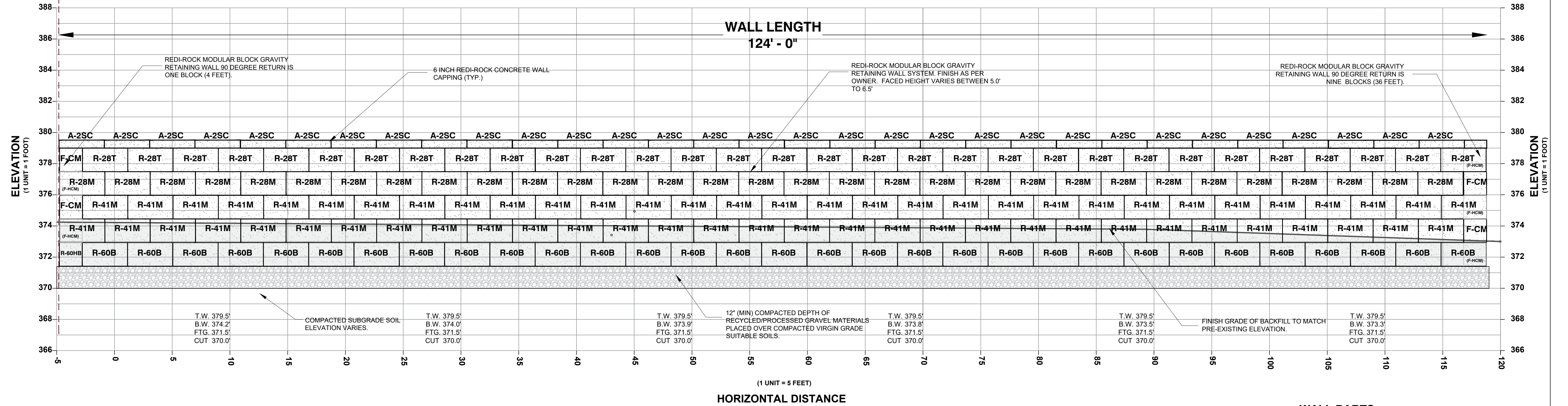
PROPOSED SITE IMPROVEMENTS TO
 GAVI RESTAURANT
 15 OLD ROUTE 22, ARMONK, NY 10504

PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO
 DATE: APRIL 26, 2023 SCALE: NONE SHEET: 10 OF 11

| NO. | REVISION | DATE |
|-----|---|--------------------|
| 1 | ADDED PROPOSED TWO STORY ADDITION AND RAISED DECK FOR GAVI RESTAURANT | July 18, 2023 |
| 2 | REVISED AS PER TOWN REVIEW COMMENTS | August 19, 2023 |
| 3 | ADDED RETAINING WALL DESIGN | September 20, 2023 |
| | | |
| | | |



REDI-ROCK RETAINING WALL PROFILE - BLOCK LIBRARY SCHEMATIC DIAGRAM



WALL PARTS

| | |
|--------------|--------------|
| A-2SC | (39) |
| F-CM | (4) |
| F-HCM | (5) |
| R-28T | (39) |
| R-28M | (39) |
| R-28HM | (2) |
| R-41M | (78) |
| R-41B | (2) |
| R-41HM | (2) |
| R-60B | (39) |
| R-60HM | (2) |
| TOTAL | (251) |

RETAINING Series

28" Series

41" Series

41" Series

60" Series

ACCESSORIES Series

CAPS & STEPS

COLUMNS

Block Library

R-28T 28" (710mm) HALF TOP

R-28M 28" (710mm) MIDDLE

R-28B 28" (710mm) BOTTOM

Block Library

R-41T 41" (1030mm) HALF TOP

R-41M 41" (1030mm) MIDDLE

R-41B 41" (1030mm) BOTTOM

Block Library

R-60B 60" (1520mm) MIDDLE

R-60HM 60" (1520mm) HALF MIDDLE

Block Library

A-2SC 28" (710mm) CORE

A-2SC 41" (1030mm) CORE

A-2SC 60" (1520mm) CORE

Block Library

A-2SC FOUR SIDED

A-2SC THREE SIDED

A-2SC THREE SIDED STEP TOP

Block Library

A-COL4 COLUMN - 4" (100mm) CORE

A-COL4 COLUMN - 6" (150mm) CORE

A-COL4 COLUMN - SOLID CORE

A-COL4 COLUMN CAP

ANY UNAUTHORIZED ALTERATION OR ADDITION TO A PLAN BEARING A SEAL OF A LICENSED LAND SURVEYOR OR PROFESSIONAL ENGINEER IS A VIOLATION OF SECTION 7209 OF THE NYS EDUCATION LAW.

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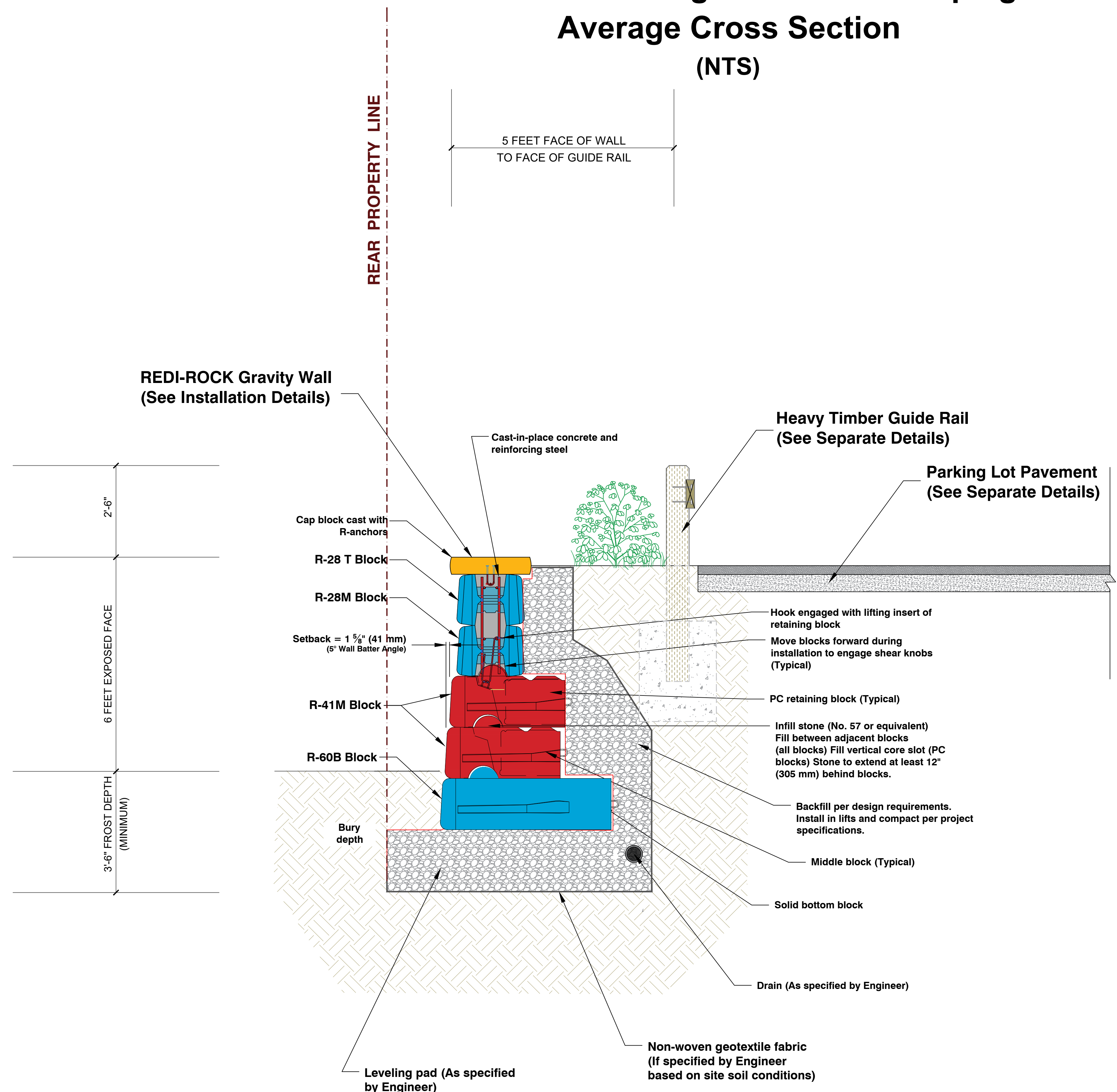
PROPOSED SITE IMPROVEMENTS TO
GAVI RESTAURANT
15 OLD ROUTE 22, ARMONK, NY 10504

PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO

DATE: APRIL 26, 2023 SCALE: NONE SHEET: 11 OF 11

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| 3 | ADDED RETAINING WALL DESIGN | September 20, 2023 |

Single Tier Redi-Rock Gravity Wall Section with Freestanding Hollow Core Coping Average Cross Section (NTS)



DESIGN PARAMETERS

All soils are considered as cohesionless for at rest pressure analysis.

Soil parameters

Sandy Silt
 Unit weight : $\gamma = 118.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 30.00^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 125.0$ pcf

Well graded gravel (GW), medium dense
 Unit weight : $\gamma = 133.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 38.50^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 133.0$ pcf

Silty sand (SM)
 Unit weight : $\gamma = 115.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 29.00^\circ$
 Cohesion of soil : $c_{ef} = 100.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 115.0$ pcf

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PROPOSED SITE IMPROVEMENTS TO
 GAVI RESTAURANT
 15 OLD ROUTE 22, ARMONK, NY 10504

PREPARED BY: DAVID GOESSL, P.E. PREPARED FOR: FRANCO DECARLO

DATE: APRIL 26, 2023 SCALE: NONE SHEET: 9A OF 9

| NO. | REVISION | DATE |
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| | | |
| | | |



Analysis of Redi Rock wall

Input data

Task : Redi Rock Gravity Wall Engineering Analysis
 Part : Proposed Wall with placed backfill including surcharge loads for vehicle, soils and groundwater
 Description : 15 Old Route 22, Armonk NY
 Customer : Gavi Restaurant
 Author : David A. Goessl, PE
 Date : 7/22/2023

Settings

USA - Safety factor

Wall analysis

Verification methodology : Safety factors (ASD)
 Active earth pressure calculation : Coulomb
 Passive earth pressure calculation : Mazindrani (Rankine)
 Earthquake analysis : Mononobe-Okabe
 Shape of earth wedge : Calculate as skew
 Allowable eccentricity : 0.333
 Internal stability : Standard - straight slip surface
 Reduction coeff. of contact first block - base : 1.00

| Safety factors | | | |
|---|--------------|------|-----|
| Seismic design situation | | | |
| Safety factor for overturning : | $SF_o =$ | 1.00 | [-] |
| Safety factor for sliding resistance : | $SF_s =$ | 1.00 | [-] |
| Safety factor for bearing capacity : | $SF_b =$ | 1.00 | [-] |
| Safety factor for sliding along geo-reinforcement : | $SF_{sr} =$ | 1.00 | [-] |
| Safety factor for geo-reinforcement strength : | $SF_{st} =$ | 1.00 | [-] |
| Safety factor for pull out resistance of geo-reinf. : | $SF_{po} =$ | 1.00 | [-] |
| Safety factor for connection strength : | $SF_{con} =$ | 1.00 | [-] |

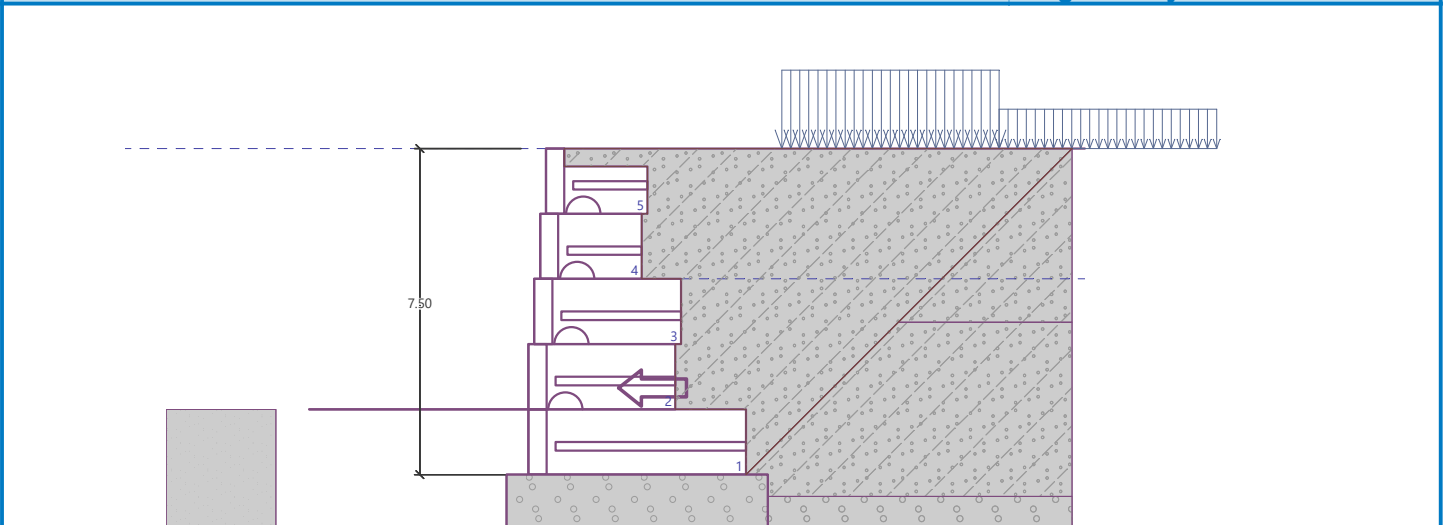
Blocks

| No. | Description | Height h [in] | Width w [in] | Unit weight γ [pcf] |
|-----|------------------------------|------------------|-----------------|-------------------------------|
| 1 | Block 28 | 18.00 | 28.00 | 120.00 |
| 2 | Block 41 | 18.00 | 40.50 | 120.00 |
| 3 | Block 60 | 18.00 | 60.00 | 130.00 |
| 4 | Top block 24 straight | 18.00 | 24.00 | 108.00 |
| 5 | Planter 41 | 18.00 | 40.50 | 120.00 |
| 6 | Planter 60 | 18.00 | 60.00 | 112.00 |
| 7 | Top block 28 | 18.00 | 28.00 | 120.00 |
| 8 | Top block 41 | 18.00 | 40.50 | 120.00 |
| 9 | Top block 24 straight garden | 18.00 | 24.00 | 80.00 |
| 10 | Block R-5236 HC | 36.00 | 52.00 | 110.00 |
| 11 | Block R-7236 HC | 36.00 | 72.00 | 110.00 |
| 12 | Block R-9636 HC | 36.00 | 96.00 | 110.00 |
| 13 | Block R-41 HC | 18.00 | 40.50 | 110.00 |

| No. | Description | Min. shear strength | Max. shear strength | Friction |
|-----|------------------------------|---------------------|---------------------|----------|
| | | F_{min} [lbf/ft] | F_{max} [lbf/ft] | f [°] |
| 1 | Block 28 | 6061.00 | 11276.00 | 44.00 |
| 2 | Block 41 | 6061.00 | 11276.00 | 44.00 |
| 3 | Block 60 | 6061.00 | 11276.00 | 44.00 |
| 4 | Top block 24 straight | 6061.00 | 11276.00 | 44.00 |
| 5 | Planter 41 | 6061.00 | 11276.00 | 44.00 |
| 6 | Planter 60 | 6061.00 | 11276.00 | 44.00 |
| 7 | Top block 28 | 6061.00 | 11276.00 | 44.00 |
| 8 | Top block 41 | 6061.00 | 11276.00 | 44.00 |
| 9 | Top block 24 straight garden | 6061.00 | 11276.00 | 44.00 |
| 10 | Block R-5236 HC | 4550.00 | 12000.00 | 44.00 |
| 11 | Block R-7236 HC | 4550.00 | 12000.00 | 44.00 |
| 12 | Block R-9636 HC | 4550.00 | 12000.00 | 44.00 |
| 13 | Block R-41 HC | 5358.00 | 12906.00 | 37.00 |

Name : Blocks

Stage - analysis : 1 - 0



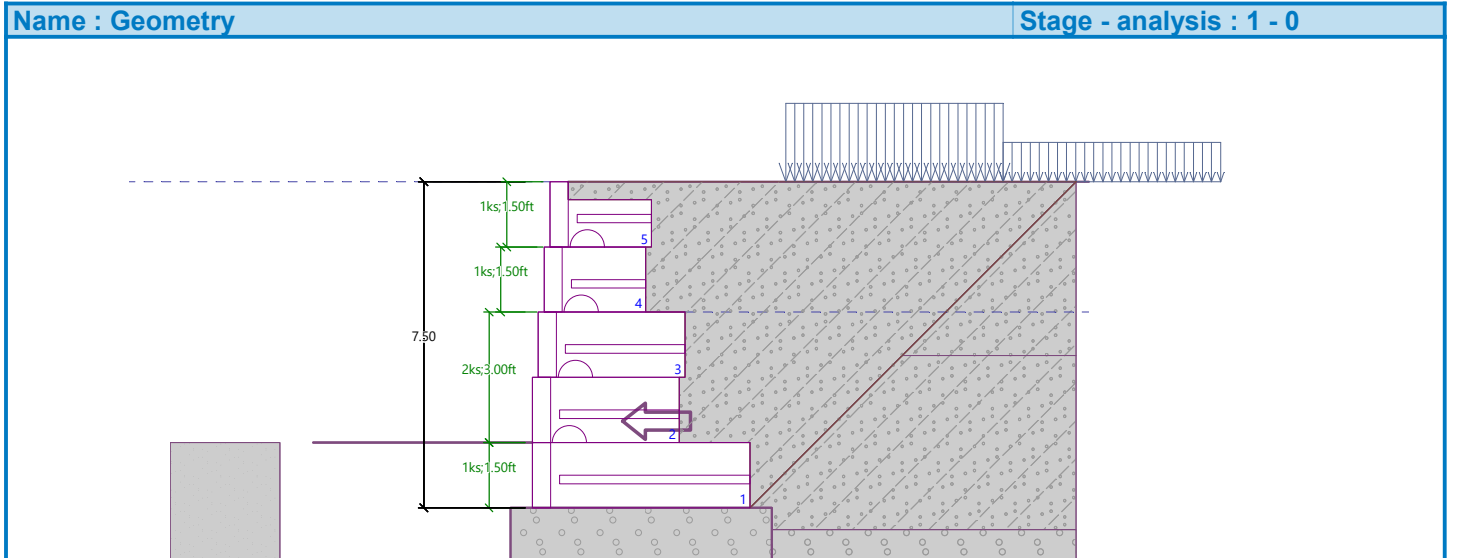
Setbacks

| No. | Setback s [in] |
|-----|----------------|
| 1 | 0.010 |
| 2 | 0.375 |
| 3 | 1.625 |
| 4 | 9.375 |
| 5 | 16.625 |

Geometry

| No. group | Description | Count | Setback s [in] |
|-----------|-------------|-------|----------------|
| 1 | Block 60 | 1 | 0.01 |
| 2 | Block 41 | 2 | 1.62 |

| No. group | Description | Count | Setback s [in] |
|-----------|--------------|-------|----------------|
| 3 | Block 28 | 1 | 1.62 |
| 4 | Top block 28 | 1 | - |



Base

Geometry

Upper setback $a_1 = 0.50$ ft
 Lower setback $a_2 = 0.50$ ft
 Height $h = 1.50$ ft
 Width $b = 6.00$ ft

Material

Soil creating foundation - Well graded gravel (GW), medium dense

Basic soil parameters

| No. | Name | Pattern | Φ_{ef} [°] | C_{ef} [psf] | γ [pcf] | γ_{su} [pcf] | δ [°] |
|-----|---------------------------------------|---------|-----------------|----------------|----------------|---------------------|--------------|
| 1 | Sandy Silt | | 30.00 | 0.0 | 118.00 | 62.50 | 25.00 |
| 2 | Well graded gravel (GW), medium dense | | 38.50 | 0.0 | 133.00 | 70.50 | 25.00 |
| 3 | Silty sand (SM) | | 29.00 | 100.0 | 115.00 | 52.50 | 25.00 |

All soils are considered as cohesionless for at rest pressure analysis.

Soil parameters

Sandy Silt

Unit weight : $\gamma = 118.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\Phi_{ef} = 30.00$ °
 Cohesion of soil : $C_{ef} = 0.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00$ °
 Saturated unit weight : $\gamma_{sat} = 125.0$ pcf

Well graded gravel (GW), medium dense

Unit weight : $\gamma = 133.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 38.50^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 133.0$ pcf

Silty sand (SM)

Unit weight : $\gamma = 115.0$ pcf
 Stress-state : effective
 Angle of internal friction : $\phi_{ef} = 29.00^\circ$
 Cohesion of soil : $c_{ef} = 100.0$ psf
 Angle of friction struc.-soil : $\delta = 25.00^\circ$
 Saturated unit weight : $\gamma_{sat} = 115.0$ pcf

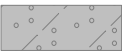



Backfill

Assigned soil : Silty sand (SM)

Slope = 45.00° **Geological profile and assigned soils****Position information**

Terrain elevation = 6.00 ft

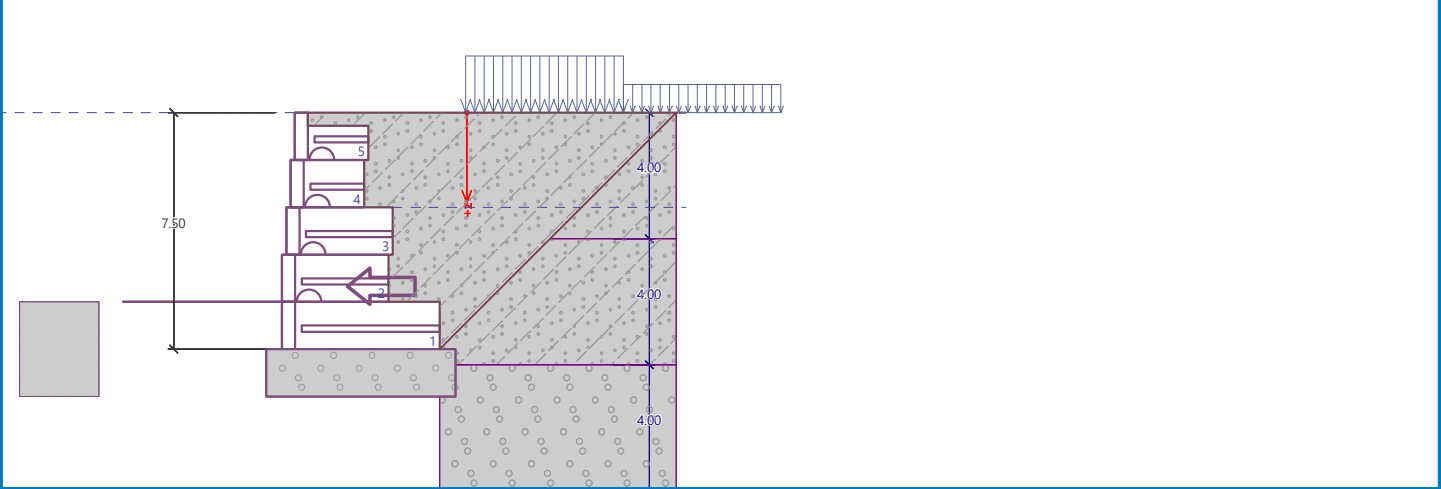
Geological profile and assigned soils

| No. | Thickness of layer t [ft] | Depth z [ft] | Elevation [ft] | Assigned soil | Pattern |
|-----|------------------------------|-----------------|-------------------|---------------------------------------|---|
| 1 | 4.00 | 0.00 .. 4.00 | 6.00 .. 2.00 | Silty sand (SM) |  |
| 2 | 4.00 | 4.00 .. 8.00 | 2.00 .. -2.00 | Silty sand (SM) |  |
| 3 | 4.00 | 8.00 .. 12.00 | -2.00 .. -6.00 | Well graded gravel (GW), medium dense |  |
| 4 | - | 12.00 .. ∞ | -6.00 .. - | Sandy Silt |  |

Name : 25 Rosehill Avenue, Tarrytown, NY

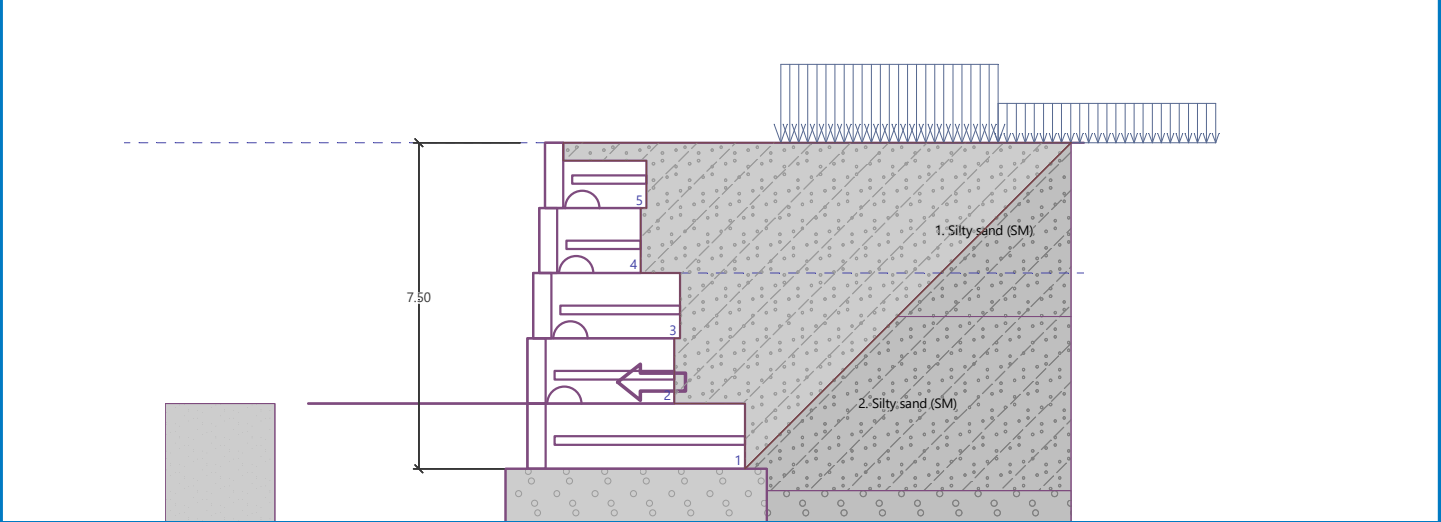
Stage - analysis : 1 - 0

Description : Redi Rock Engineering Analysis - Lower Tier Wall with Applied Surcharge Loads



Name : Profile and assignment

Stage - analysis : 1 - 0



Terrain profile

Terrain behind the structure is flat.

Water influence

GWT behind the structure lies at a depth of 3.00 ft

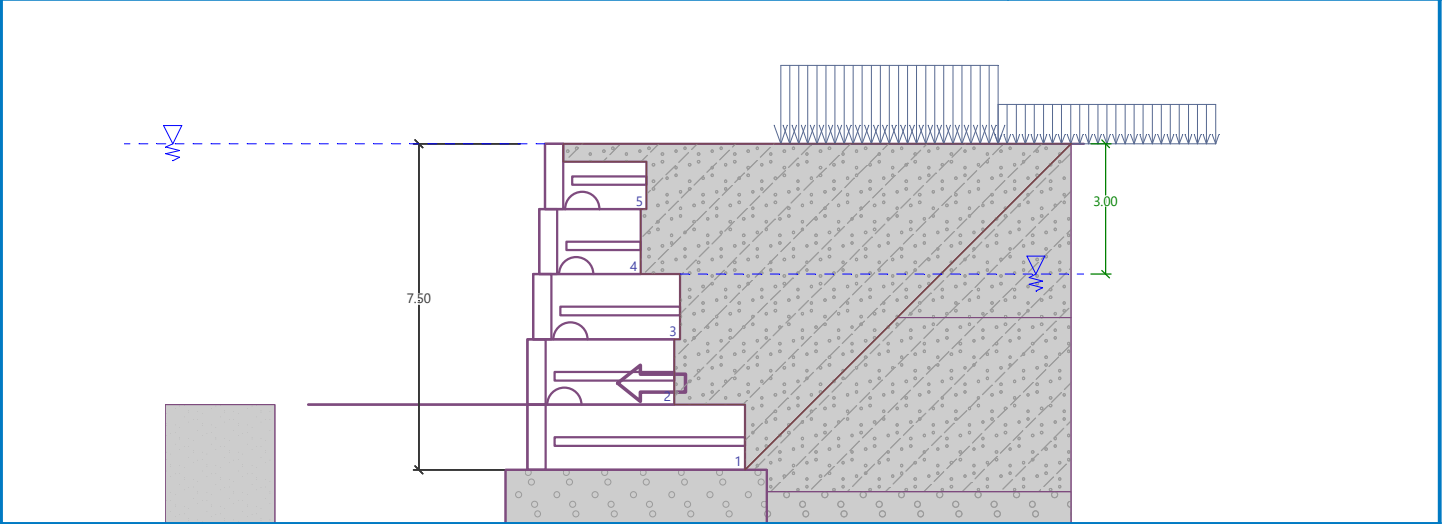
GWT in front of the structure lies at a depth of 0.00 ft

Subgrade at the heel is not permeable.

Uplift in foot. bottom due to different pressures is not considered.

Name : Water

Stage - analysis : 1 - 0



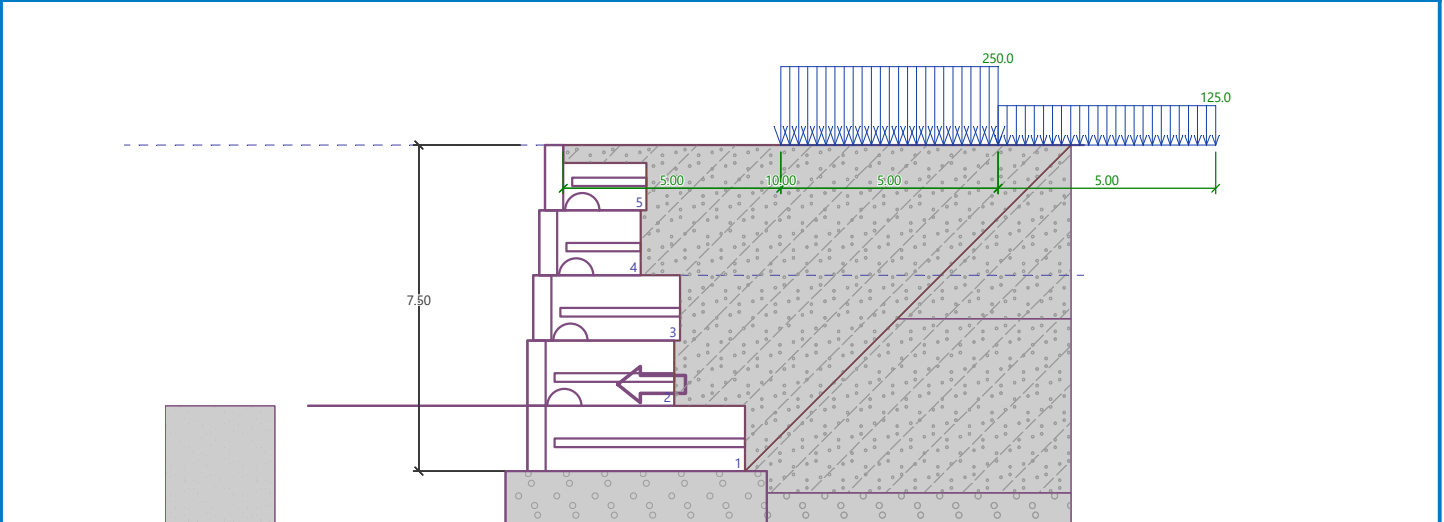
Input surface surcharges

| No. | Surcharge new | Surcharge change | Action | Mag.1 [lbf/ft ²] | Mag.2 [lbf/ft ²] | Ord.x x [ft] | Length l [ft] | Depth z [ft] |
|-----|---------------|------------------|-----------|------------------------------|------------------------------|--------------|---------------|--------------|
| 1 | Yes | | permanent | 250.00 | | 5.00 | 5.00 | on terrain |
| 2 | Yes | | permanent | 125.00 | | 10.00 | 5.00 | on terrain |

| No. | Name |
|-----|-----------------|
| 1 | Vehicle Loading |
| 2 | Overburden |

Name : Surcharge

Stage - analysis : 1 - 0



Resistance on front face of the structure

Resistance on front face of the structure: not considered

Soil on front face of the structure - Sandy Silt

Soil thickness in front of structure $h = 3.00$ ft

Terrain in front of structure is flat.

EarthquakeFactor of horizontal acceleration $K_h = 0.1500$ Factor of vertical acceleration $K_v = 0.0000$

Water below the GWT is restricted.

Settings of the stage of construction

Design situation : seismic

Reduction of soil/soil friction angle : do not reduce

Verification No. 1**Forces acting on construction**

| Name | F_{hor} [lb/ft] | App.Pt. z [ft] | F_{vert} [lb/ft] | App.Pt. x [ft] | Design coefficient |
|----------------------------------|----------------------|-------------------|-----------------------|-------------------|-----------------------|
| Weight - wall | 0.0 | -3.96 | 2471.1 | 2.52 | 1.000 |
| Earthq.- constr. | 620.9 | -3.50 | 0.0 | 2.58 | 1.000 |
| Weight - earth wedge | 0.0 | -1.78 | 11.1 | 5.67 | 1.000 |
| Earthquake - soil wedge | 3.7 | -1.78 | 0.0 | 5.67 | 1.000 |
| Weight - earth wedge | 0.0 | -3.85 | 109.2 | 4.46 | 1.000 |
| Earthquake - soil wedge | 35.9 | -3.85 | 0.0 | 4.46 | 1.000 |
| Weight - earth wedge | 0.0 | -6.44 | 69.5 | 3.45 | 1.000 |
| Earthquake - soil wedge | 10.4 | -6.44 | 0.0 | 3.45 | 1.000 |
| Weight - earth wedge | 0.0 | -8.79 | 86.0 | 2.22 | 1.000 |
| Earthquake - soil wedge | 12.9 | -8.79 | 0.0 | 2.22 | 1.000 |
| Active pressure | 666.5 | -3.05 | 883.2 | 5.01 | 1.000 |
| Water pressure | -1406.2 | -3.80 | 0.0 | 1.67 | 1.000 |
| Uplift pressure | 0.0 | -9.00 | 0.0 | 1.32 | 1.000 |
| Earthq.- act.pressure | 598.7 | -5.05 | 802.2 | 4.48 | 1.000 |
| Dyn. water pressure at the front | 443.0 | -3.60 | 0.0 | 2.99 | 1.000 |
| Vehicle Loading | 253.5 | -3.53 | 279.2 | 4.79 | 1.000 |
| Overburden | 68.4 | -2.11 | 65.0 | 5.47 | 1.000 |

Verification of complete wall**Check for overturning stability**Resisting moment $M_{res} = 16919.2$ lbfft/ftOverturning moment $M_{ovr} = 4844.0$ lbfft/ft

Safety factor = 3.49 > 1.00

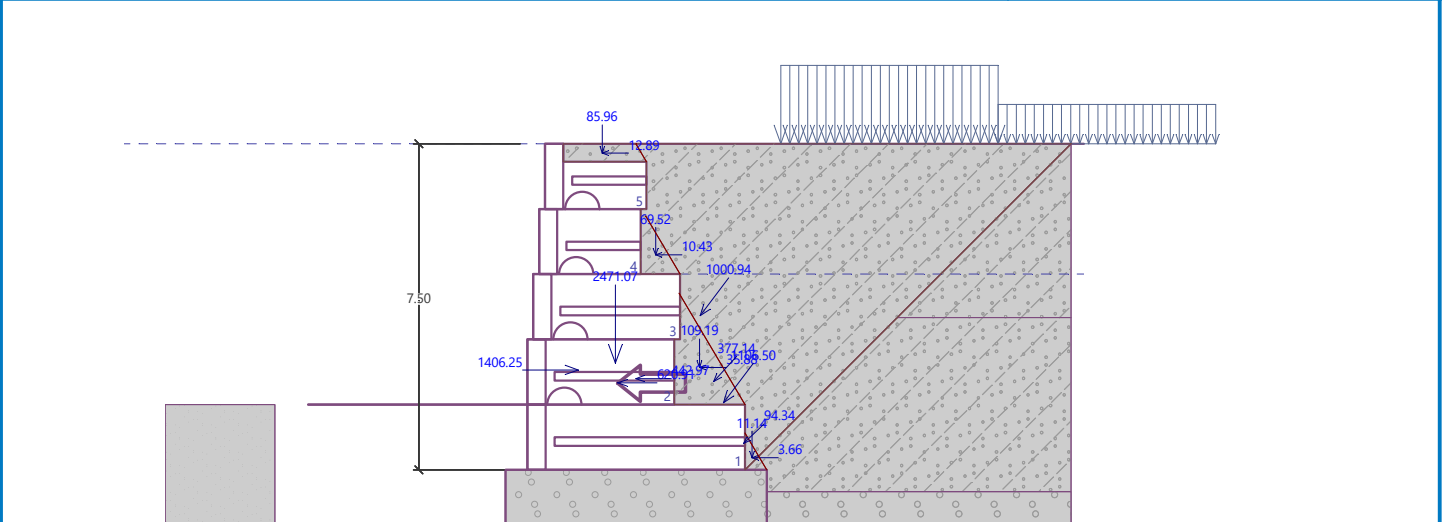
Wall for overturning is SATISFACTORY**Check for slip**Resisting horizontal force $H_{res} = 3799.44$ lbf/ftActive horizontal force $H_{act} = 1307.50$ lbf/ft

Safety factor = 2.91 > 1.00

Wall for slip is SATISFACTORY**Overall check - WALL is SATISFACTORY**

Name : Verification

Stage - analysis : 1 - 1



Dimensioning No. 1

Forces acting on construction

| Name | F _{hor} [lbf/ft] | App.Pt. z [ft] | F _{vert} [lbf/ft] | App.Pt. x [ft] | Design coefficient |
|----------------------------------|------------------------------|-------------------|-------------------------------|-------------------|-----------------------|
| Weight - wall | 0.0 | -3.56 | 1836.6 | 1.86 | 1.000 |
| Earthq.- constr. | 451.2 | -3.04 | 0.0 | 1.92 | 1.000 |
| Weight - earth wedge | 0.0 | -2.35 | 109.2 | 3.96 | 1.000 |
| Earthquake - soil wedge | 35.9 | -2.35 | 0.0 | 3.96 | 1.000 |
| Weight - earth wedge | 0.0 | -4.94 | 69.5 | 2.95 | 1.000 |
| Earthquake - soil wedge | 10.4 | -4.94 | 0.0 | 2.95 | 1.000 |
| Weight - earth wedge | 0.0 | -7.29 | 86.0 | 1.72 | 1.000 |
| Earthquake - soil wedge | 12.9 | -7.29 | 0.0 | 1.72 | 1.000 |
| Active pressure | 434.7 | -2.61 | 618.8 | 4.15 | 1.000 |
| Water pressure | -1125.0 | -3.06 | 0.0 | 1.67 | 1.000 |
| Uplift pressure | 0.0 | -7.50 | 0.0 | 0.82 | 1.000 |
| Earthq.- act.pressure | 359.4 | -4.24 | 470.8 | 3.71 | 1.000 |
| Dyn. water pressure at the front | 307.6 | -3.00 | 0.0 | 2.49 | 1.000 |
| Vehicle Loading | 216.3 | -2.61 | 234.3 | 4.05 | 1.000 |
| Overburden | 51.7 | -1.23 | 45.2 | 4.74 | 1.000 |

Verification of block No. 1

Check for overturning stability

Resisting moment $M_{res} = 9670.3$ lbfft/ftOverturning moment $M_{ovr} = 2365.4$ lbfft/ft

Safety factor = 4.09 > 1.00

Joint for overturning stability is SATISFACTORY

Check for slip

Resisting horizontal force $H_{res} = 2760.46$ lbf/ftActive horizontal force $H_{act} = 755.13$ lbf/ft

Safety factor = 3.66 > 1.00

Joint for verification is **SATISFACTORY**

Bearing capacity of foundation soil

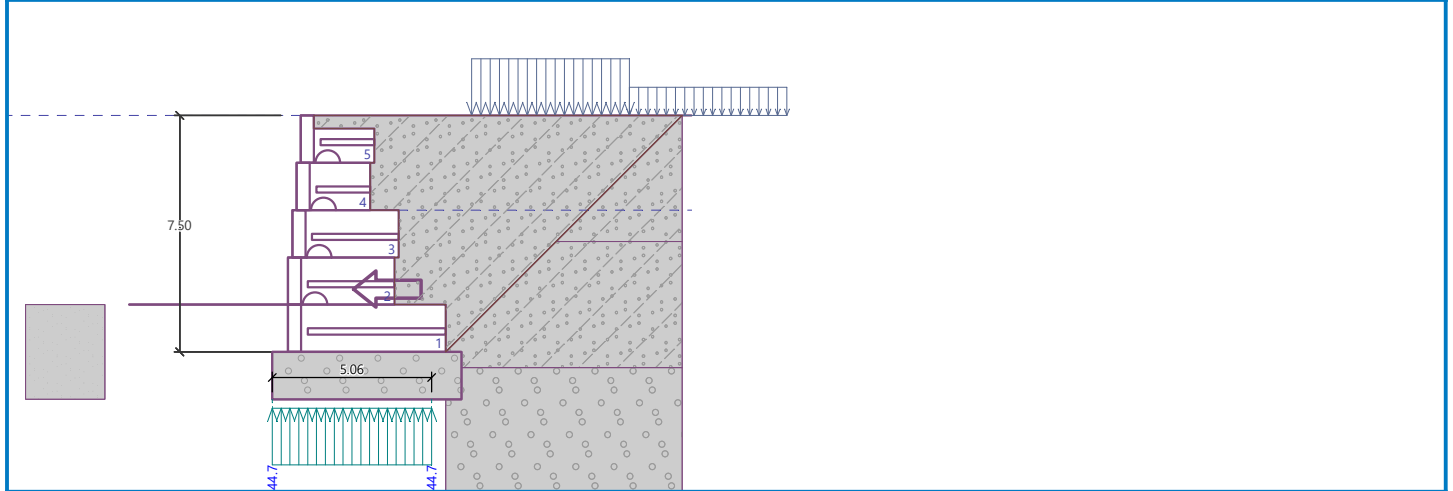
Design load acting at the center of footing bottom

| No. | Moment [lbfft/ft] | Norm. force [lbf/ft] | Shear Force [lbf/ft] | Eccentricity [-] | Stress [psf] |
|-----|-------------------|----------------------|----------------------|------------------|--------------|
| 1 | 2254.4 | 4776.55 | 1307.50 | 0.079 | 944.7 |

Service load acting at the center of footing bottom

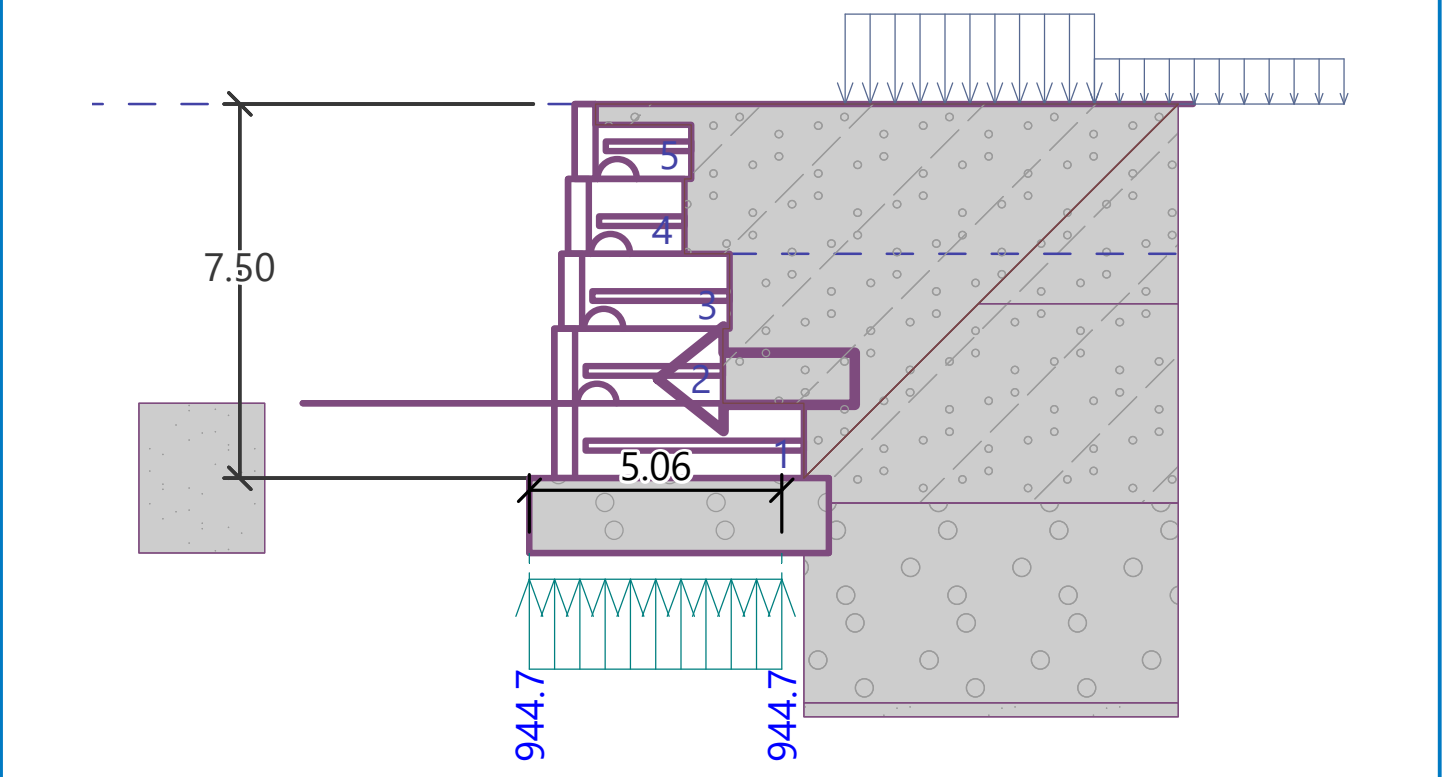
| No. | Moment [lbfft/ft] | Norm. force [lbf/ft] | Shear Force [lbf/ft] |
|-----|-------------------|----------------------|----------------------|
| 1 | 2254.4 | 4776.55 | 1307.50 |

| | |
|--|---------------------------|
| Name : Bearing cap. | Stage - analysis : 1 - -1 |
| Description : Lower Tier Wall Profile with Surcharge Loads | |



Name : Bearing cap.

Stage - analysis : 1 - -1



Slope stability analysis

Input data (Construction stage 1)

Project

Settings

USA - Safety factor

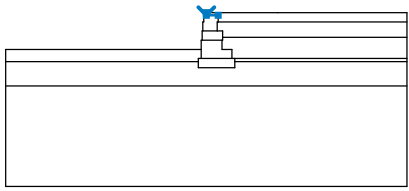
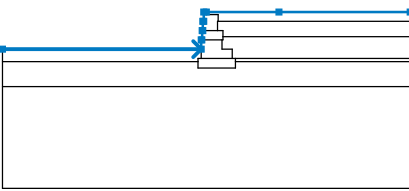
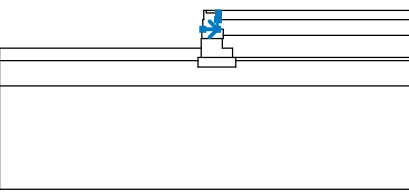
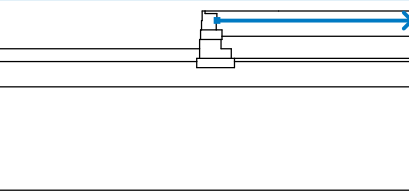
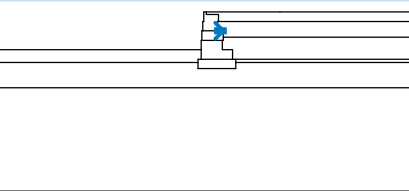
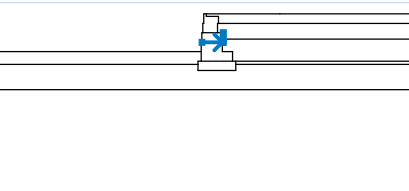
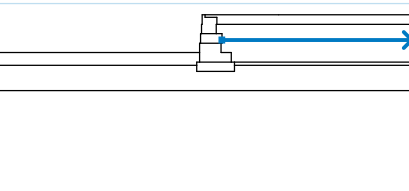
Stability analysis

Verification methodology : Safety factors (ASD)

Earthquake analysis : Standard

| Safety factors | | |
|--------------------------|-------------------|----------|
| Seismic design situation | | |
| Safety factor : | SF _s = | 1.00 [-] |

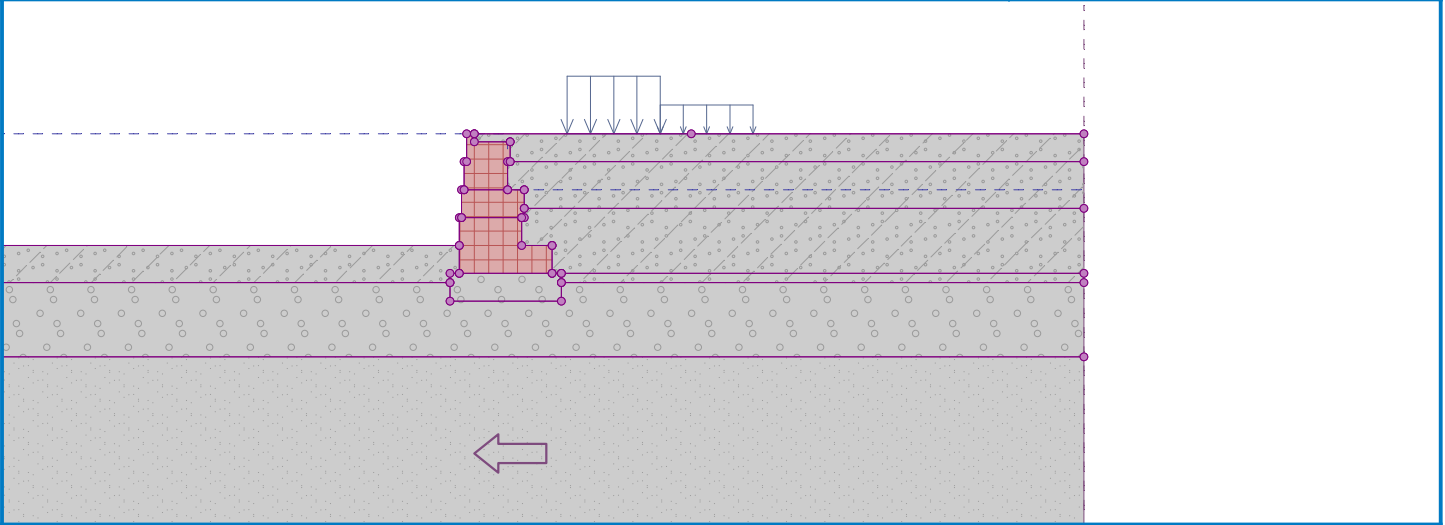
Interface

| No. | Interface location | Coordinates of interface points [ft] | | | | | |
|-----|---|--------------------------------------|------|-------|------|-------|------|
| | | x | z | x | z | x | z |
| 1 |  | 0.00 | 6.00 | 0.00 | 5.58 | 1.92 | 5.58 |
| 2 |  | -32.80 | 0.00 | -0.82 | 0.00 | -0.82 | 1.50 |
| | | -0.69 | 1.50 | -0.69 | 3.00 | -0.55 | 3.00 |
| | | -0.55 | 4.50 | -0.42 | 4.50 | -0.42 | 6.00 |
| | | 0.00 | 6.00 | 11.68 | 6.00 | 32.80 | 6.00 |
| 3 |  | -0.55 | 3.00 | 1.78 | 3.00 | 1.78 | 4.50 |
| | | 1.92 | 4.50 | 1.92 | 5.58 | | |
| 4 |  | 1.92 | 4.50 | 32.80 | 4.50 | | |
| 5 |  | 1.78 | 3.00 | 2.69 | 3.00 | | |
| 6 |  | -0.69 | 1.50 | 2.55 | 1.50 | 2.69 | 1.50 |
| | | 2.69 | 2.00 | 2.69 | 3.00 | | |
| 7 |  | 2.69 | 2.00 | 32.80 | 2.00 | | |

| No. | Interface location | Coordinates of interface points [ft] | | | | | |
|-----|--------------------|--------------------------------------|-------|-------|-------|-------|-------|
| | | x | z | x | z | x | z |
| 8 | | 2.55 | 1.50 | 2.55 | 0.00 | 4.18 | 0.00 |
| | | | | | | | |
| 9 | | -0.82 | -1.50 | 4.18 | -1.50 | 4.18 | 0.00 |
| | | | | | | | |
| 10 | | -32.80 | -2.00 | -1.32 | -2.00 | -1.32 | -1.50 |
| | | -0.82 | -1.50 | -0.82 | 0.00 | | |
| 11 | | 4.18 | -1.50 | 4.68 | -1.50 | | |
| | | | | | | | |
| 12 | | -1.32 | -2.00 | -1.32 | -3.00 | 4.68 | -3.00 |
| | | 4.68 | -2.00 | 4.68 | -1.50 | 32.80 | -1.50 |
| 13 | | 4.68 | -2.00 | 32.80 | -2.00 | | |
| | | | | | | | |
| 14 | | -32.80 | -6.00 | 32.80 | -6.00 | | |
| | | | | | | | |

Name : Interfaces

Stage : 1



Soil parameters - effective stress state

| No. | Name | Pattern | ϕ_{ef} [°] | c_{ef} [psf] | γ [pcf] |
|-----|---------------------------------------|---------|--------------------|-------------------|-------------------|
| 1 | Sandy Silt | | 30.00 | 0.0 | 118.0 |
| 2 | Well graded gravel (GW), medium dense | | 38.50 | 0.0 | 133.0 |
| 3 | Silty sand (SM) | | 29.00 | 100.0 | 115.0 |

Soil parameters - uplift

| No. | Name | Pattern | γ_{sat} [pcf] | γ_s [pcf] | n [-] |
|-----|---------------------------------------|---------|-------------------------|---------------------|------------|
| 1 | Sandy Silt | | 125.0 | | |
| 2 | Well graded gravel (GW), medium dense | | 133.0 | | |
| 3 | Silty sand (SM) | | 115.0 | | |

Soil parameters

Sandy Silt

Unit weight :

$$\gamma = 118.0 \text{ pcf}$$

Stress-state : effective
 Shear strength : Mohr-Coulomb
 Angle of internal friction : $\phi_{ef} = 30.00^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Saturated unit weight : $\gamma_{sat} = 125.0$ pcf

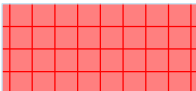
Well graded gravel (GW), medium dense

Unit weight : $\gamma = 133.0$ pcf
 Stress-state : effective
 Shear strength : Mohr-Coulomb
 Angle of internal friction : $\phi_{ef} = 38.50^\circ$
 Cohesion of soil : $c_{ef} = 0.0$ psf
 Saturated unit weight : $\gamma_{sat} = 133.0$ pcf

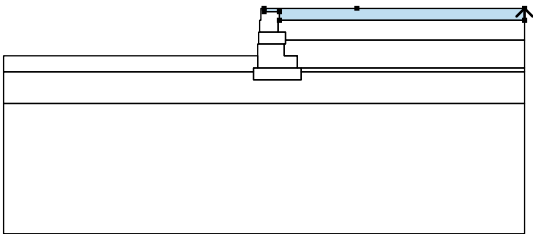
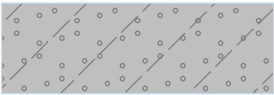
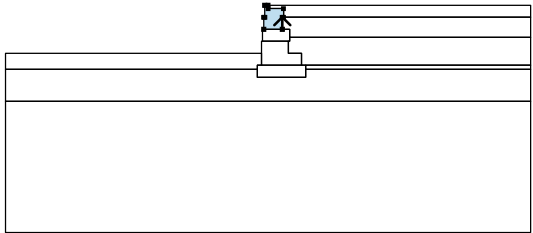

Silty sand (SM)

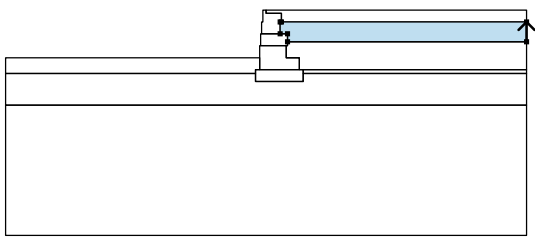
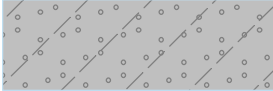
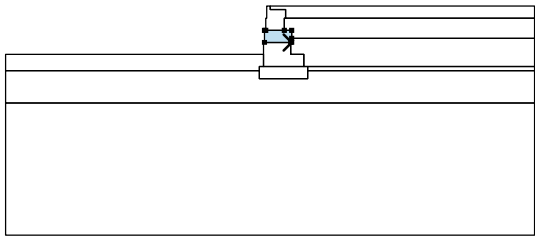
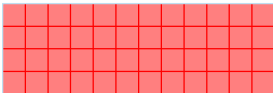
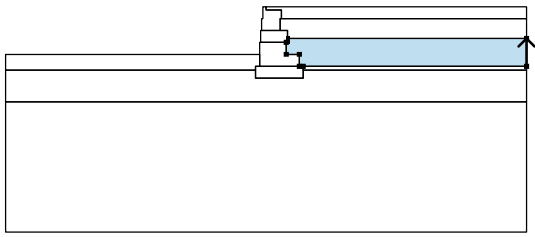
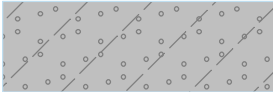
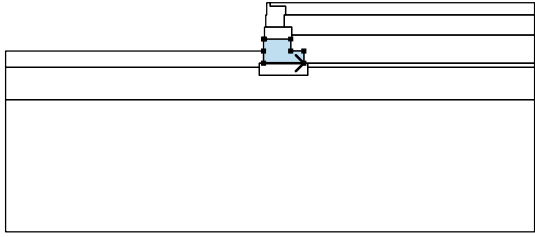

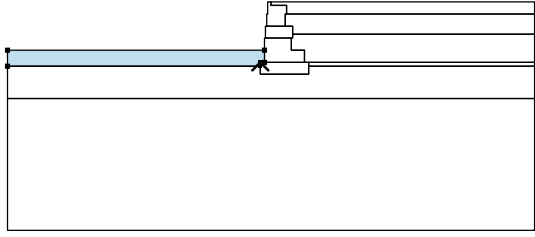
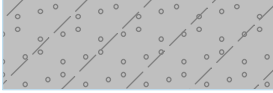
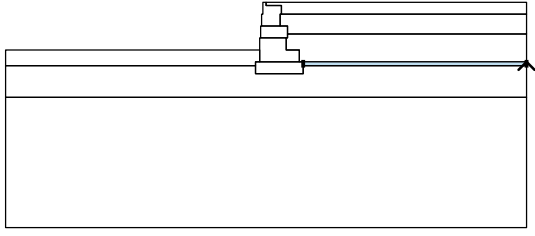
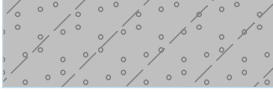
Unit weight : $\gamma = 115.0$ pcf
 Stress-state : effective
 Shear strength : Mohr-Coulomb
 Angle of internal friction : $\phi_{ef} = 29.00^\circ$
 Cohesion of soil : $c_{ef} = 100.0$ psf
 Saturated unit weight : $\gamma_{sat} = 115.0$ pcf

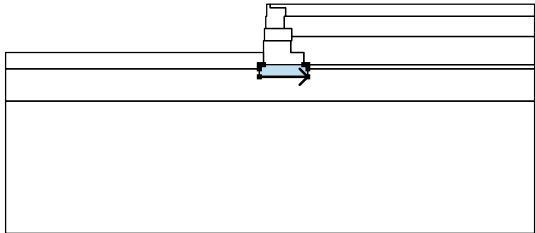
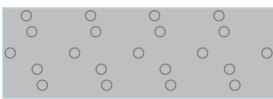
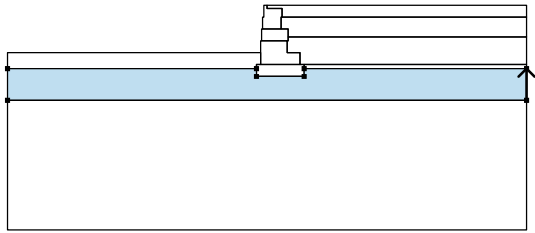
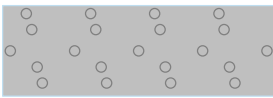
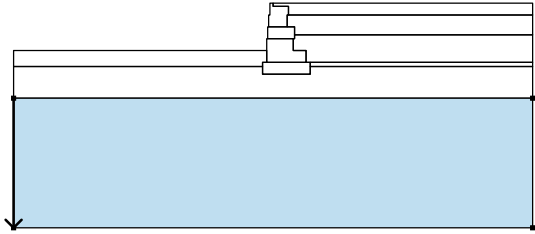

Rigid Bodies

| No. | Name | Sample | γ [pcf] |
|-----|-----------------------|---|----------------|
| 1 | Material of structure |  | 120.0 |

Assigning and surfaces

| No. | Surface position | Coordinates of surface points [ft] | | | | Assigned soil |
|-----|---|------------------------------------|------|-------|------|--|
| | | x | z | x | z | |
| 1 |  | 32.80 | 4.50 | 32.80 | 6.00 | Silty sand (SM)  |
| | | 11.68 | 6.00 | 0.00 | 6.00 | |
| | | 0.00 | 5.58 | 1.92 | 5.58 | |
| | | 1.92 | 4.50 | | | |
| 2 |  | 1.78 | 3.00 | 1.78 | 4.50 | Material of structure  |
| | | 1.92 | 4.50 | 1.92 | 5.58 | |
| | | 0.00 | 5.58 | 0.00 | 6.00 | |
| | | -0.42 | 6.00 | -0.42 | 4.50 | |
| | | -0.55 | 4.50 | -0.55 | 3.00 | |

| No. | Surface position | Coordinates of surface points [ft] | | | | Assigned soil |
|-----|---|------------------------------------|-------|--------|-------|--|
| | | x | z | x | z | |
| 3 |  | 32.80 | 2.00 | 32.80 | 4.50 | Silty sand (SM)  |
| | | 1.92 | 4.50 | 1.78 | 4.50 | |
| | | 1.78 | 3.00 | 2.69 | 3.00 | |
| | | 2.69 | 2.00 | | | |
| 4 |  | 2.55 | 1.50 | 2.69 | 1.50 | Material of structure  |
| | | 2.69 | 2.00 | 2.69 | 3.00 | |
| | | 1.78 | 3.00 | -0.55 | 3.00 | |
| | | -0.69 | 3.00 | -0.69 | 1.50 | |
| 5 |  | 32.80 | -1.50 | 32.80 | 2.00 | Silty sand (SM)  |
| | | 2.69 | 2.00 | 2.69 | 1.50 | |
| | | 2.55 | 1.50 | 2.55 | 0.00 | |
| | | 4.18 | 0.00 | 4.18 | -1.50 | |
| | | 4.68 | -1.50 | | | |
| 6 |  | -0.82 | -1.50 | 4.18 | -1.50 | Material of structure  |
| | | 4.18 | 0.00 | 2.55 | 0.00 | |
| | | 2.55 | 1.50 | -0.69 | 1.50 | |
| | | -0.82 | 1.50 | -0.82 | 0.00 | |
| 7 |  | -1.32 | -2.00 | -1.32 | -1.50 | Silty sand (SM)  |
| | | -0.82 | -1.50 | -0.82 | 0.00 | |
| | | -32.80 | 0.00 | -32.80 | -2.00 | |
| 8 |  | 32.80 | -2.00 | 32.80 | -1.50 | Silty sand (SM)  |
| | | 4.68 | -1.50 | 4.68 | -2.00 | |

| No. | Surface position | Coordinates of surface points [ft] | | | | Assigned soil |
|-----|--|------------------------------------|--------|--------|--------|--|
| | | x | z | x | z | |
| 9 |  | -1.32 | -3.00 | 4.68 | -3.00 | Well graded gravel (GW), medium dense  |
| | | 4.68 | -2.00 | 4.68 | -1.50 | |
| | | 4.18 | -1.50 | -0.82 | -1.50 | |
| | | -1.32 | -1.50 | -1.32 | -2.00 | |
| 10 |  | 32.80 | -6.00 | 32.80 | -2.00 | Well graded gravel (GW), medium dense  |
| | | 4.68 | -2.00 | 4.68 | -3.00 | |
| | | -1.32 | -3.00 | -1.32 | -2.00 | |
| | | -32.80 | -2.00 | -32.80 | -6.00 | |
| 11 |  | -32.80 | -6.00 | -32.80 | -22.40 | Sandy Silt  |
| | | 32.80 | -22.40 | 32.80 | -6.00 | |

Surcharge

| No. | Type | Type of action | Location z [ft] | Origin x [ft] | Length l [ft] | Width b [ft] | Slope α [°] | Magnitude | | |
|-----|-------|----------------|--------------------|------------------|------------------|-----------------|-----------------------|-----------------------------|--------------------|--------------------|
| | | | | | | | | q, q ₁ , f, F, x | q ₂ , z | unit |
| 1 | strip | permanent | on terrain | x = 5.00 | l = 5.00 | | 0.00 | 250.0 | | lb/ft ² |
| 2 | strip | permanent | on terrain | x = 10.00 | l = 5.00 | | 0.00 | 125.0 | | lb/ft ² |

Surcharges

| No. | Name |
|-----|-----------------|
| 1 | Vehicle Loading |
| 2 | soil overburden |

Water

Water type : GWT

| No. | GWT location | Coordinates of GWT points [ft] | | | | | |
|-----|--------------|--------------------------------|------|------|------|------|------|
| | | x | z | x | z | x | z |
| 1 | | -32.80 | 6.00 | 1.78 | 6.00 | 1.78 | 3.00 |
| | | 32.80 | 3.00 | | | | |

Tensile crack

Tensile crack not input.

Earthquake

Horizontal seismic coefficient : $K_h = 0.1500$

Vertical seismic coefficient : $K_v = 0.0000$

Settings of the stage of construction

Design situation : seismic

Results (Construction stage 1)

Analysis 1

Circular slip surface

| Slip surface parameters | | | | | | | |
|--------------------------------------|-----|-------|------|----------|--------------|--------|-----|
| Center : | x = | -5.15 | [ft] | Angles : | $\alpha_1 =$ | -35.87 | [°] |
| | z = | 16.24 | [ft] | | $\alpha_2 =$ | 59.27 | [°] |
| Radius : | R = | 20.04 | [ft] | | | | |
| The slip surface after optimization. | | | | | | | |

Total weight of soil above the slip surface: 14568.9 lbf/ft

Slope stability verification (Bishop)

Sum of active forces : $F_a = 4537.2$ lbf/ft

Sum of passive forces : $F_p = 8490.9$ lbf/ft

Sliding moment : $M_a = 90925.2$ lbfft/ft

Resisting moment : $M_p = 170158.2$ lbfft/ft

Factor of safety = 1.87 > 1.00

Slope stability ACCEPTABLE